

# Synthesis of dense bulk MgB<sub>2</sub> by an infiltration and growth process

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**Abstract:** We report the processing of dense, superconducting MgB<sub>2</sub> ( $\rho \approx 2.4 \text{ g/cm}^3$ ) by an infiltration and growth technique. The process, which involves infiltration of liquid magnesium at 750 °C into a pre-defined boron precursor pellet, is relatively simple, results in the formation of a hard, dense structure and has the potential to fabricate large bulk samples of complex geometries. X-ray diffraction has been used to confirm the presence of the MgB<sub>2</sub> primary phase with only residual magnesium content in the fully processed samples. The samples exhibit sharp superconducting transitions at 38.4 K and have critical current densities of up to 260 kA/cm<sup>2</sup> in self-field at 5 K. Modest measured values of H<sub>c2</sub>(0) of 17 T suggest that superconductivity in bulk MgB<sub>2</sub> fabricated by this technique is in the clean pairing limit.

## Introduction

Superconductivity in magnesium diboride ( $\text{MgB}_2$ ) was discovered in 2001 [1]. The relatively high  $T_c$  (39 K), high critical current density, long coherence length ( $\sim 6$  nm) [2], low raw material cost, lower density and relative ease of fabrication make this material an exciting choice for practical applications. Furthermore, lower anisotropy and strongly linked current flow in untextured polycrystalline samples of bulk  $\text{MgB}_2$  has enabled the development of different processing routes to fabricate  $\text{MgB}_2$  in the form of wires, tapes, thin films and bulks [3,4].

All the superconductors discovered over the past thirty years, despite having higher transition temperatures and critical current densities, have been unable to replace Nb based superconductors in commercial applications due primarily to difficulties associated with processing. In HTS materials, for example, strong crystallographic texture is necessary since grain boundaries inhibit strongly the flow of inter-granular current [5]. This also limits the thickness of the tape or bulk form of material to which they can be made [6]. Given these limitations,  $\text{MgB}_2$  could be a good choice of material for applications that operate around temperatures of around 20 K that are achievable using compact, cryo-coolers without the need for liquid helium. Unfortunately, the volatility of Mg during processing has hindered greatly its prospects for practical applications in the short term.

Conventionally,  $\text{MgB}_2$  processed in the form of wires and tapes can be synthesized either by an *ex situ* or *in situ* sintering technique. Grasso *et al* have reported high  $J_c$  using the *ex situ* route without any thermal treatment [7], although the relatively poor self-sintering nature of  $\text{MgB}_2$  grains results in weaker inter-grain coupling. As a result, overall connectivity is often poor in these samples, even for long sintering times [8]. Moreover, a higher reaction

temperature results in the decomposition of  $\text{MgB}_2$  to form Mg and  $\text{MgB}_4$  [9], which can further deteriorate the properties of the fully processed material. *In situ* synthesis from elemental (Mg+B) powder, on the other hand, is relatively simple and yields the  $\text{MgB}_2$  phase after a sintering time as little as 2 hours [10]. However, this processing route often results in the formation of a highly porous structure (up to 50%) due primarily to the high vapour pressure of magnesium and 28% volume shrinkage associated with  $\text{MgB}_2$  phase formation [11]. Precursor powders for the fabrication of bulk  $\text{MgB}_2$  are therefore often enriched with Mg to compensate for lost Mg vapour during processing. Although this leads to improved grain connectivity, porosity is still unavoidable in the fully processed bulk [12], and weak links are created frequently by the formation of oxides such as  $\text{BO}_x$  and MgO, which reduce the effective current carrying cross sectional area of the sample [13, 14]. There have been numerous reports of the synthesis of bulk  $\text{MgB}_2$  via sintering, and a number of studies have shown that high pressure and elevated temperature [15,16] are effective in promoting  $\text{MgB}_2$  phase formation and subsequent sintering. The use of high-pressure leads typically to the introduction of defects in the  $\text{MgB}_2$  structure that form effective pinning centres [17]. Although this approach results in a high critical current density, the need to use large pressure vessels represents a significant practical limitation for the development of a practical process and of the achievable dimensions in the final  $\text{MgB}_2$  sample.

Several authors have adopted a low temperature, solid-solid reaction approach for the fabrication of  $\text{MgB}_2$  to avoid vaporization of Mg during processing. Rogado *et al* first reported the *in situ* synthesis of  $\text{MgB}_2$  at a temperature as low as 500 °C [18]. Kumakura *et al* subsequently proposed a technique based on “internal Mg diffusion”, which involved placing Mg rod along the axis of a B powder compact in a sealed tube, followed by cold working and then annealing at 600 °C [19]. Similarly, Goldacker *et al* obtained high transport  $J_c$  in fine

grain  $\text{MgB}_2$  fabricated *in situ* at low temperature (640 °C) [20], which resulted in the formation of a highly dense  $\text{MgB}_2$  phase. Yamamoto *et al* have proposed a “powder in closed tube” method that involves packing Mg and B powders densely in the form of tapes in a sealed tube by applying a high uniaxial pressure prior to sintering [21]. This method was found to be effective in confining the Mg vapour in the reaction chamber, which led to a high  $\text{MgB}_2$  bulk density. The same process at lower reaction temperature (600 °C) yielded a finer grain and a reduced crystalline  $\text{MgB}_2$  phase content, both of which contributed to an increase in flux pinning force and  $J_c$  [22]. Alternatively, Togano proposed an “interface diffusion” method using layers of Fe-Mg alloy as source of Mg with a layer of B powder sandwiched between the layers and then annealed. Mg atoms were observed to diffuse into the B grains during this process to yield a dense  $\text{MgB}_2$  tape containing relatively little porosity [23]. Finally, Fujii *et al* and Matsumoto *et al* used  $\text{MgH}_2$  as a source of Mg. The  $\text{H}_2$  produced following the decomposition of  $\text{MgH}_2$  forms a reducing atmosphere, which results in reduced oxidation of Mg and the formation of a well-connected  $\text{MgB}_2$  phase [24,25]. These improvised methods largely avoid the problem of Mg vaporization, resulting in the formation of a dense microstructure with high critical current densities. However, these techniques tend to be difficult to scale up to form bulk  $\text{MgB}_2$  components for practical applications due to limited diffusion of Mg into B at low temperatures [26] and long reaction times associated with the process. As a result, the fabrication of high density, bulk  $\text{MgB}_2$  remains a challenging processing problem.

Here, we report the synthesis of bulk  $\text{MgB}_2$  by the infiltration of liquid Mg into porous B precursor. This process has been adapted from the “infiltration and growth” technique used to synthesize bulk Y-Ba-Cu-O (YBCO) superconductor, which involves infiltrating Ba-Cu-O liquid into solid  $\text{Y}_2\text{BaCuO}_5$  (Y-211) followed by a controlled peritectic reaction to yield the

target superconducting  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$  (Y-123) phase [27,28]. The infiltration and growth process offers potentially significant advantages for the Mg-B system due to its lower reaction temperature and the inherent capability of  $\text{MgB}_2$  fabricated in polycrystalline form to carry large current. This relatively simple method not only results in the formation of hard, dense structures but also has the potential to fabricate complex geometries, which are not achieved easily using conventional sintering techniques.

The infiltration route for processing  $\text{MgB}_2$  fibers (of diameter 160  $\mu\text{m}$ ) was first reported by Canfield *et al* [10] and involves exposing B fibers to Mg vapour at 950 °C. Later, Dunand *et al* [29] reported the synthesis of Mg- $\text{MgB}_2$  composites by infiltrating liquid Mg under pressure at 800 °C into a B preform. Improved versions of this process were reported subsequently by Giunchi *et al* [30] for the fabrication of bulk  $\text{MgB}_2$  artefacts, in which Mg bulk and B powder are placed in a metallic container. The container was then welded closed and heat-treated at 950 °C to obtain dense, bulk  $\text{MgB}_2$ , with the initial arrangement of B and Mg bulk in the container being used to define the geometry of the final product [31].

## **Experimental**

Disc shaped precursor bodies (20 mm diameter and 4 mm thickness) were prepared from 99.99% (44  $\mu\text{m}$ ) purity amorphous boron powder (Alfa Aesar) under an applied uniaxial load of 5 MPa. The green density of the precursor pellet was engineered to be around 40% of the theoretical value, so that any residual pores in the bulk microstructure could be infiltrated by liquid Mg during processing to satisfy the overall compositional stoichiometry. A boron pellet was sandwiched initially between Mg blocks of commercial purity, as shown in Fig. 1(a). The magnesium was then melted at 750 °C in a graphite crucible for 2 hours. Excess liquid Mg was used in this process in view of its high vapour pressure and to maintain a

positive fluid pressure aid to infiltration. A  $N_2 + SF_6$  (95:5) cover gas mixture was maintained to minimize the oxidation of Mg during the process. The excess Mg was removed from the sample by machining after cooling to room temperature and the  $MgB_2$  disc recovered, as shown in Fig 1(b). Several small specimens of size 3 mm\*3 mm\*1 mm were cut from the  $MgB_2$  bulk for further characterization. The density was determined from simple mass and volume measurements to be 90% of the theoretical density. The microstructure and fracture surface of the infiltrated sample was examined by scanning electron microscopy (SEM), and X-ray diffraction (XRD) was performed to analyse the phase content of the sample. The magnetic moment of sample was measured using a superconducting quantum interference device (SQUID) magnetometer. Critical current density was calculated from the measured magnetic moment loop using the extended Bean model for a rectangular cross section in a perpendicular magnetic field [32]. Finally, a four-probe resistance technique was used to measure the resistivity of the sample under an applied external field of up to 9 T (applied perpendicular to the direction of transport current).

## **Results and Discussion**

Figure 2 shows an X-ray diffraction powder pattern for the  $MgB_2$  sample fabricated by infiltration and growth, which confirms that the specimen consists of a majority  $MgB_2$  phase with residual MgO and Mg. The presence of Mg is commonly observed in infiltration studies [29, 30] and associated with the dense packing of the  $MgB_2$  unit cell, which creates voids that become occupied by surrounding liquid Mg during processing. Detailed analysis suggests that material has about 5% MgO and 13% Mg. MgO has likely formed as a result of reaction between excess Mg and O during milling process that was used to powder the bulk. Giunchi *et al* reported the presence of boron rich phases such as  $Mg_2B_{25}$ ,  $MgB_4$  or  $MgB_7$  in the reactive liquid infiltration process [31,33], although no such phases were detected in the

samples prepared in this study. This may be explained by the Mg-rich atmosphere generated intrinsically as part of the fabrication process, which facilitates the formation of Mg-rich borides in the  $MgB_x$  family, and  $MgB_2$  in particular.

Figure 3(a) shows a secondary electron image of the fracture surface of the  $MgB_2$  bulk sample, which reveals a dense microstructure and clean grain boundaries. Significantly, no impurities or porosity are observed in this image. A higher magnification micrograph of the same fracture surface is shown in Fig 3(b), from which the presence of hexagonal plate-like crystals can be observed. This is due primarily to the rapid crystal growth parallel to the  $a$ - $b$  plane; such geometry is typical of hcp borides that exhibit faceted growth. The grain size can be estimated from this micrograph to be around 500 nm. A similar morphology has been reported previously for  $MgB_2$  [34]. Giunchi *et al* also observed the presence of several grains of size 100  $\mu m$  after processing at 950  $^{\circ}C$  in a similar experiment [30], suggesting that such fine grain size is due potentially to the use of a lower reaction temperature (750  $^{\circ}C$ ), which limits grain growth. Such homogeneous microstructure is attributed presence of excess Mg during reaction, which is known for improving grain connectivity, elimination of micro-cracks, facilitating recrystallization and avoiding B-rich impurities [35].

The normalised field cooled (FC) and zero field cooled (ZFC) magnetic moment for the bulk  $MgB_2$  fabricated by infiltration and growth are shown in Fig. 4 for an applied field of 1 mT. A sharp superconducting transition at 38.4 K and transition width of 0.7 K is observed in both sets of data, which suggest that bulk sample prepared in this study is homogeneous.

Fig. 5 shows the variation of critical current density,  $J_c$ , as a function of applied field at 5 K, 20 K and 30 K.  $J_c$  at 5 K and 20 K under self-field is as high as 260  $kA/cm^2$  and 200  $kA/cm^2$ ,

respectively, suggesting that the sample is well connected with a relatively large current carrying cross sectional area.  $J_c$  decreases appreciably in higher applied field, which is indicative of weak flux pinning in this field regime. Giunchi *et al* obtained slightly high  $J_c$  of  $80 \text{ kA/cm}^2$  (20K, 2 T) with RLI process [36]. Similarly Maeda *et al* ( $10^3 \text{ A/cm}^2$ , 20 K, 4T) [37], Yamamoto *et al* ( $600 \text{ kA/cm}^2$ , self-field 20 K) [11] reported high  $J_c$  in ambient pressure in-situ sintering route. Prikhna *et al* recently reported very high  $J_c$  of  $900 \text{ kA/cm}^2$  (Self field, 20 K) using high pressure [38]. Obtained  $J_c$  here, although modest when compared to these data, is relatively high taking into account residual Mg content.

Figure 6 shows the variation of resistivity with temperature for the  $\text{MgB}_2$  bulk sample between 300 K and 5 K in an applied external field up to 9 T. For a comparison, normalised ZFC magnetic transition is also plotted (Figure 6 inset). Although  $T_c$  offset is slightly reduced (difference of .4 K) in inductive mode,  $T_c$  onset is quite close (difference is  $\approx .02 \text{ K}$ ). Such behaviour has previously been observed and is attributed to the transport current path in resistive measurement that chooses good quality grains (least resistance) [39]. This is in contrast to the inductive measurement where current loop passes through surface of material which includes good and poor quality grains. The observed low difference in measured  $T_c$  by two separate techniques suggests that the material is indeed homogeneous.

The sample exhibits a very low residual resistivity of  $2.64 \mu\Omega\text{cm}$  and a residual resistivity ratio (RRR) of 5.63, which is comparable to values observed for single crystal  $\text{MgB}_2$  samples (typically  $1\text{-}2 \mu\Omega\text{cm}$  measured in-plane), as reported previously [2,40,41]. In addition, the observed increase in resistivity with external field at a given temperature indicates that the bulk  $\text{MgB}_2$  sample exhibits significant magneto resistive effects. The normal state electrical connectivity (K) (or effective cross sectional area), which is defined by Rowell [9] as the

ratio of difference of resistivity between a single crystal to that of a polycrystal, is calculated for the MgB<sub>2</sub> bulk sample from the following expression:

$$K = \frac{\rho_{sc}(300\text{ K}) - \rho_{sc}(40\text{ K})}{\rho(300\text{ K}) - \rho(40\text{ K})} = 51.8\% \quad \begin{array}{l} \rho_{sc}(300\text{ K}) - \rho_{sc}(40\text{ K}) = 6.32\ \mu\Omega\text{cm} \\ \rho(300\text{ K}) - \rho(40\text{ K}) = 12.2\ \mu\Omega\text{cm} \end{array}$$

where  $\rho_{sc}$  is the resistivity of an MgB<sub>2</sub> single crystal averaged over random orientations and  $\rho$  is the resistivity of MgB<sub>2</sub> fabricated by infiltration and growth. Difference of resistivity of single crystal between 300 K and 40 K ( $\rho(300\text{ K}) - \rho(40\text{ K})$ ) is taken as 6.32  $\mu\Omega\text{cm}$  based on predictions of mean field theory in [11]. The connectivity obtained here is significantly higher than that observed in bulk MgB<sub>2</sub> samples synthesized by both *ex situ* ( $\sim 10\%$ ) and *in situ* ( $\sim 30\%$ ) ambient pressure processing routes [8].

It is important to note that the transport properties of the present sample are altered by residual magnesium metal within the infiltrated grown sample.  $\rho$ -T plot for pure MgB<sub>2</sub> shows plateau near 80 K, whereas  $\rho$ -T curve for Mg exhibits linear decrease till 40 K [42]. Magneto-resistance is another evidence for the contribution of residual magnesium on current transport [43]. It is evident from figure 6 that  $\rho$ -T curve obtained here has characteristics of MgB<sub>2</sub> as well as Mg. Thus it is likely that  $\rho(300\text{ K})$  and  $\rho(40\text{ K})$  are underestimated whereas RRR and connectivity are overestimated in the present case. A prediction of connectivity in such case would require numerous samples with known amount of excess Mg. The intercept of extrapolated  $\rho(T)$  *versus* excess Mg curves would yield a fairly good value of  $\rho(300\text{ K})$  and  $\rho(40\text{ K})$  excluding any effects by Mg. These values can then be used to estimate corrected value of connectivity.

Figure 7 shows the variation of upper critical field,  $H_{c2}$ , and irreversibility field,  $H_{irr}$ , with temperature, both of which have been estimated using the 90%-10% definition of the resistive transition. It can be seen that both  $H_{c2}$  and  $H_{irr}$  vary linearly at temperatures below around 34

K (i.e. slightly below  $T_c$ ). A simple extrapolation of the curve yields a value of  $H_{c2}$  at 0 K of 17 T. This is rather lower than that obtained for polycrystalline  $MgB_2$  [16] and is close to the value of  $H_{c2}$  for a single crystal (15 T in the  $a$ - $b$  plane) [44]. This suggests that sample fabricated in the present study is transformed fully into highly crystalline  $MgB_2$ .

## **Conclusion**

We have demonstrated the fabrication of dense and highly connected bulk  $MgB_2$  by an infiltration and growth process. This relatively simple technique is performed at ambient pressure and is therefore potentially scalable to the fabrication of larger bulk  $MgB_2$  samples of more complex geometries. X-Ray diffraction has revealed that  $MgB_2$  is present in the bulk samples as the main phase with Mg and MgO present in minor quantities. Densification mechanism in this study differs significantly from conventional solid state sintering of  $MgB_2$ , in which the porosity is typically retained during processing resulting in poorly connected grains.  $J_c$  of the bulk  $MgB_2$  samples in self-field is  $200 \text{ kA/cm}^2$  (at 20 K) and is relatively high considering high residual Mg content. The good microstructural and superconducting properties of bulk  $MgB_2$  fabricated by the infiltration and growth process are attributed to the presence of dense, fine grains and a pore free  $MgB_2$  bulk microstructure. Finally, an upper critical field of 17 T has been observed for this sample, which is close to single crystal value and which indicates that bulk material is operating in the clean pairing limit for superconductivity.

## **Acknowledgements**

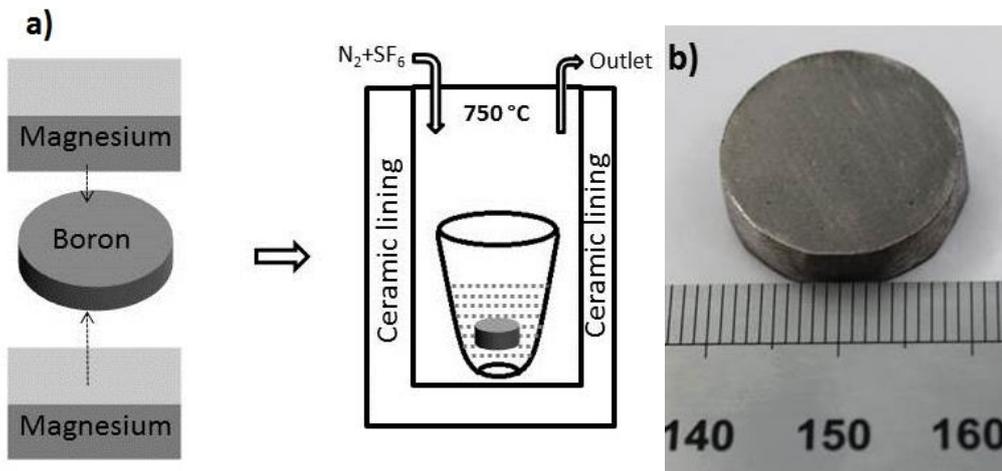
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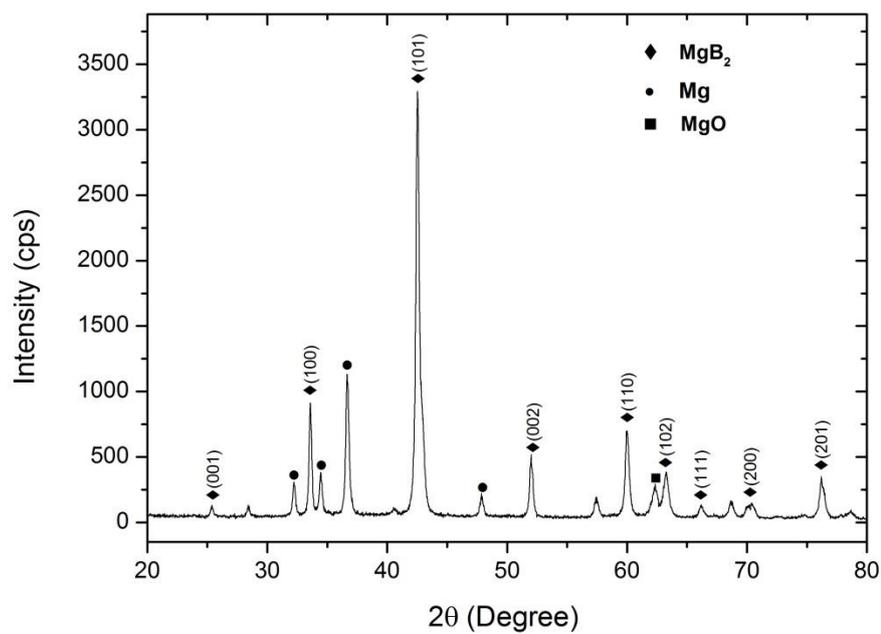
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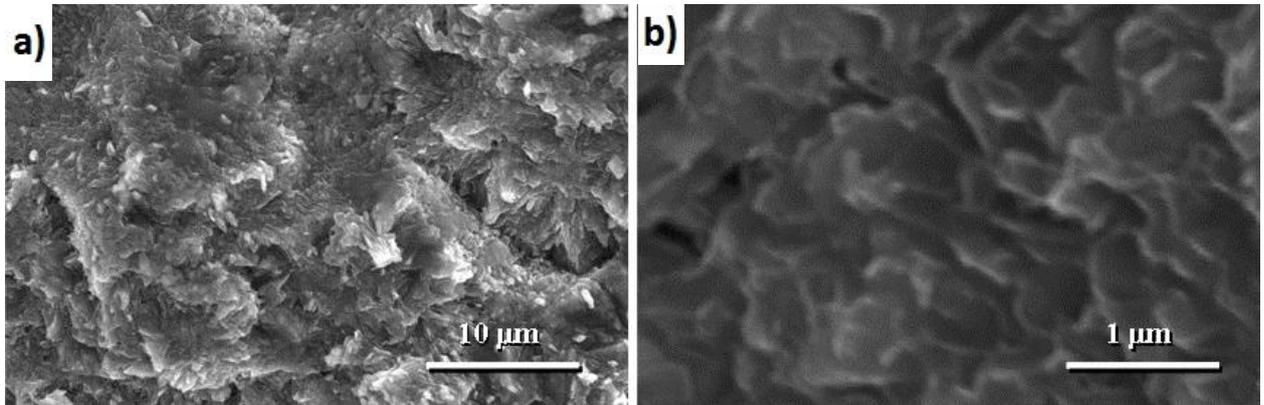
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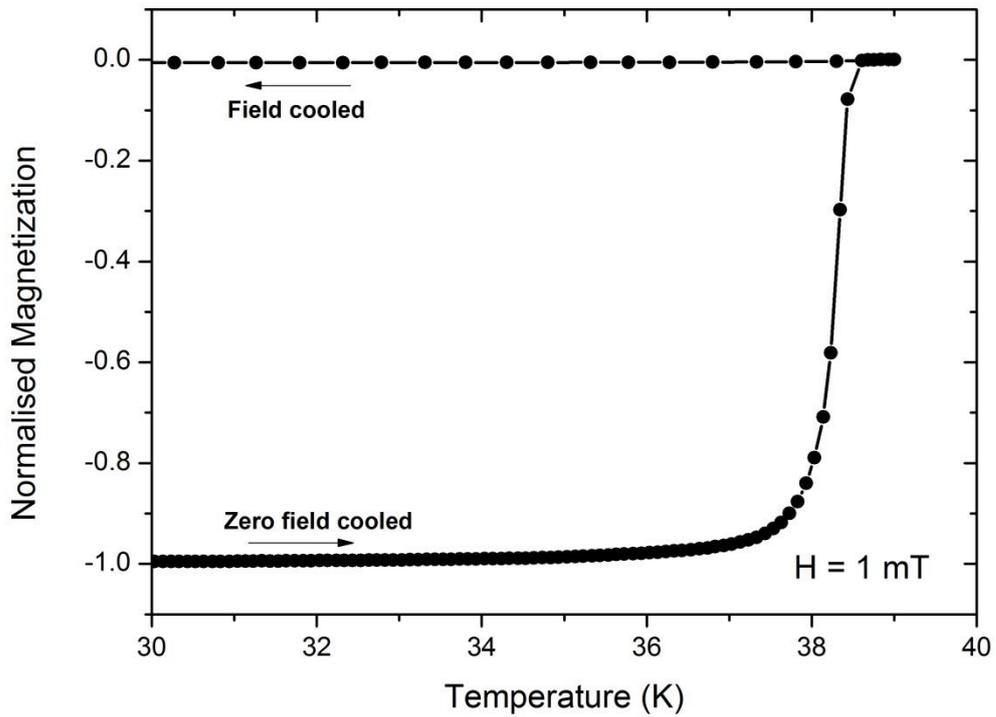
**Fig 1 (a) Schematic of the infiltration and growth process and (b) Photograph of a  $MgB_2$  disc fabricated by infiltrated and growth**



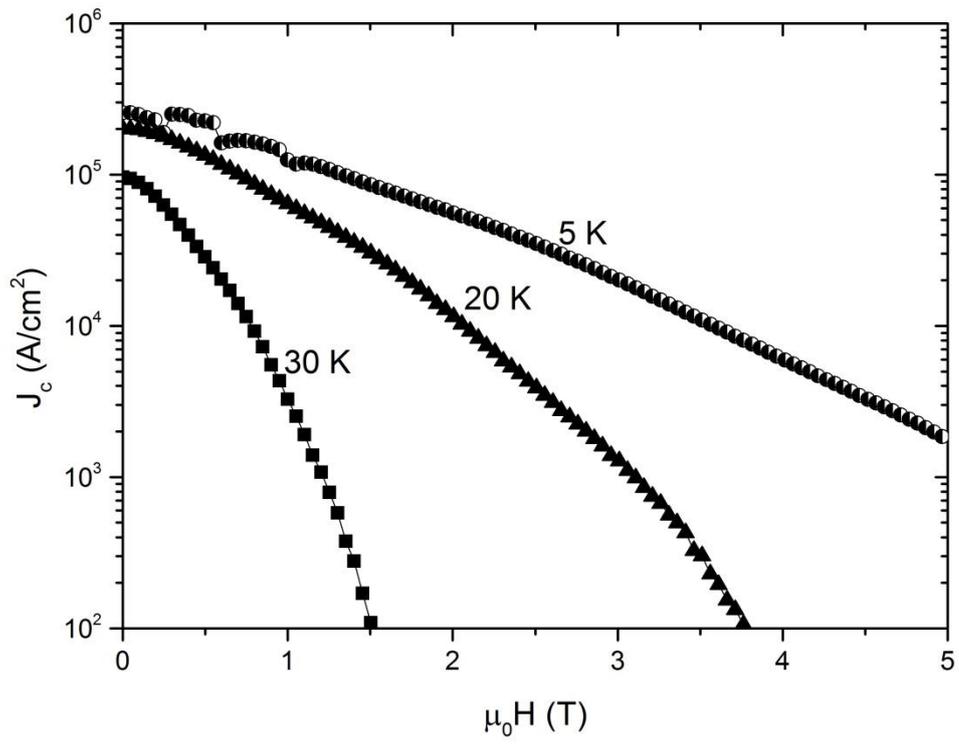
**Fig. 2. X ray diffraction pattern of a  $MgB_2$  powder specimen fabricated by infiltration and growth indicating the presence of Mg and MgO impurities. All  $MgB_2$  peak positions are indexed.**



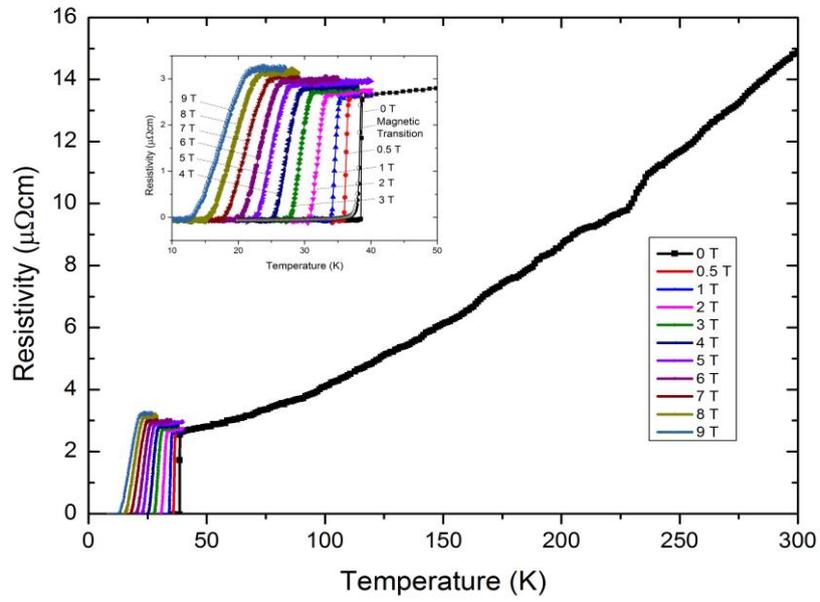
**Fig. 3(a)** SEM observation of the fractured bulk  $\text{MgB}_2$  surface (b) fine grain structure



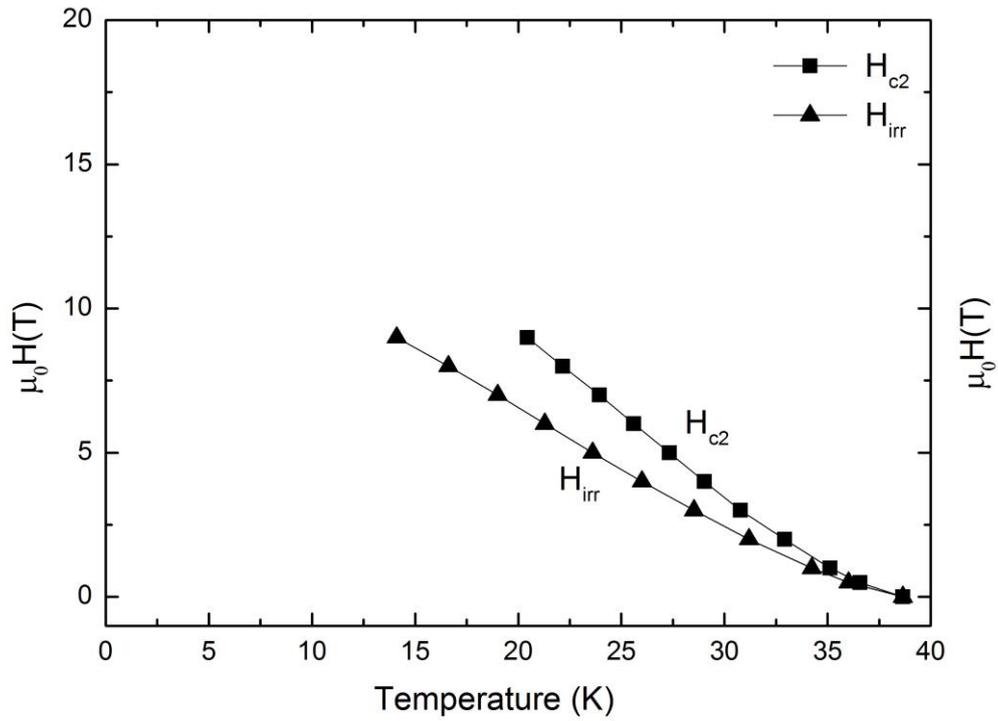
**Fig. 4.** Normalised magnetization of  $\text{MgB}_2$  as a function of temperature, measured under zero field and field cooled conditions at 1 mT.



**Fig. 5.** Critical current density of bulk MgB<sub>2</sub> as a function of applied magnetic field



**Fig. 6. Variation of the bulk MgB<sub>2</sub> resistivity with temperature at applied magnetic fields of up to 9 T**



**Fig. 7. Dependence of  $H_{c2}$  and  $H_{irr}$  of infiltrated bulk  $MgB_2$  with temperature. Values estimated using 90%-10% of the normal-state resistivity.**