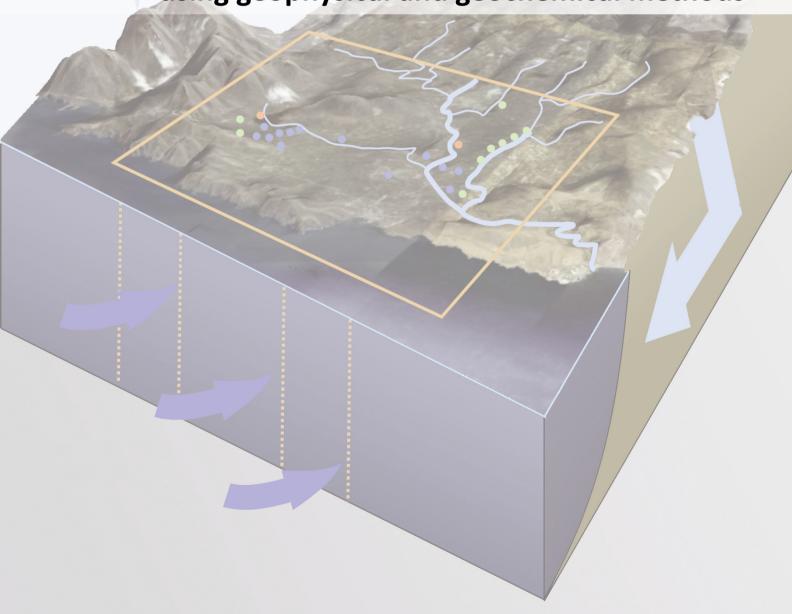
Assessment of groundwater resources in the north-central coast of Crete, Greece using geophysical and geochemical methods



Brunel University - UK December 2009

## [ABSTRACT]

The Geropotamos aquifer on the north-central coast of Crete, Greece, is invaded in some places by salt water from the Aegean Sea, with impact on freshwater supplies for domestic and business uses, including agriculture. The geological setting of the study area is considered complex, as Miocene biogenic limestones, marls, clays and conglomerates crop out in the central and the western part and clastic limestones and dolomites of the Tripolis and Plattenkalk nappe (the bedrock) in the eastern part of the study area. The phyllitequartzite nappe (which forms the oldest rock of the study area) lays on the northern part of Geropotamos basin. The local tectonic regime of the study area is characterized by faults of NW-SE and NE-SW directions. Investigation of the aquifer using Transient ElectroMagnetic method (TEM) and Vertical Electrical Resistivity (VES) measurement technique has resulted in 1D models and 2D/3D imaging of geoelectric structures, depicting the zones of salination of groundwater in the aquifer. 1179 TEM soundings in 372 sites have been carried out in a detailed survey grid (about 200m in X and Y dimension) and 3 VES soundings were acquired in three different sites (different geological conditions). For the 2 of them, multidirectional measurements were also acquired since the structure is more complex than a 1D model that VES technique is able to model. Moreover, 3 water samplings carried out. At each sampling, samples from 22 boreholes and 2 springs were analysed and 16 chemical parameters were determined. Detailed geochemical analysis, including Piper, Durov, Ternary, Stiff, Wilcox, Dispersion diagrams and Factors controlling the groundwater quality, was accomplished showing very good results and the relationship with the geophysical methods. All data were inserted in GIS environment and Groundwater Quality Maps were produced. Furthermore, Remote Sensing application, geological mapping and hydro-lithological data showed that the physical characteristics of geomorphology and geology are in great relationship with the chemical and geophysical properties as well. Suggestions that Miocene evaporites led to groundwater salination are unconfirmed, and seawater intrusion is the most probable cause, supported by the results of this research. It is indicated that saline intrusion is likely to occur along fractures in a fault zone through otherwise low-permeability phyllite-quartzite bedrock, and it is emphasized the critical role of fracture pathways in salination problems of coastal aquifers.

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This thesis is dedicated to the memory of my sister and my father.

## [INTRODUCTION]

### **Chapter Contents**

- ► Preface: the background of this thesis
- ► Aim and objectives of this study
- Choice of study area
- ► General information about the study area
- ▶ Geomorphological, Geological and Hydrological setting of the study area
- ▶ Geographic Information System (GIS) as data-base management system
- ► Previous geochemical data from local authorities
- **▶** Thesis outline
- **▶** Summary

#### 1.1 Preface: the background of this thesis

The recent changes in climate patterns, caused naturally and by human activities, highlight the need to secure reliable water supplies especially in areas where water is scarce. The Mediterranean and particularly its islands are mostly affected due to their geographical isolation and climate. A particular problem is seawater intrusion into near-shore aquifers (Donta, 2005).

A place where this issue is of great importance is the island of Crete, Greece. Crete has undergone a rapid and substantial economic development over the last 35 years. This is due not only to the long-established tourist industry but also to changes in the pattern of agriculture. This research combines geophysical and geochemical analyses to investigate the extent of seawater intrusion in the Geropotamos aquifer, on the coast of north-central Crete where water demand has increased notably the last decades. The main source of water in the Geropotamos area (and in the whole island) is from groundwater, which is ultimately derived from the (predominantly winter) rainfall; the economy of the region depends to a large extent on the availability of water of sufficient quality.

#### 1.2 Aim and objectives of this study

**Overall purpose of thesis** - apply geophysical and geochemical methods to a poorly understood area of limited groundwater resources, in order to determine the status of those resources used by an increasing local population.

The primary questions of this study are:

- What is the relationship between the geomorphology, rock types and structure?
- What is the relationship between the water quality and the physical characteristics of geomorphology and geology?
- What is the relationship between the physical and geochemical characters of the area, and the results of geophysical surveys?

#### 1.3 Choice of study area

This work is a development from a European Project, INTERREG III B ARCHIMED, subproject A1.020 entitled "Methodology integration of EO techniques as operative tool for land degradation management and planning in Mediterranean areas - MILDMAP", accomplished partly by the group of the Seismology and Geophysics laboratory of the Technological Educational Institute of Crete (branch of Chania). One of the objectives of that project was to investigate the salt-water problem in the Bali area (Fig.1.1), a very touristic and developing area, in Rethymnon Prefecture, lying a few kilometers east of the Geropotamos basin (AMRA, 2007).

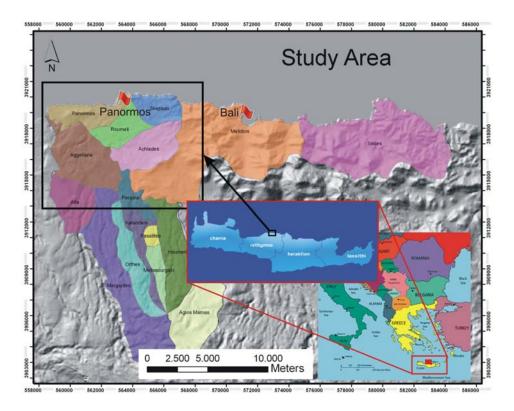
The Geropotamos River catchment and its underlying aquifer system is an important component of the water resources of the general area; the relationship between the Geropotamos catchment and the Bali area is not clearly known, so in order to enhance and inform the Bali project, as well as increase understanding of water resource management in this zone of increasing economic and touristic development, this research was designed to carry out a detailed geophysical and geochemical study of Geropotamos area. The expected outcome is that this work will provide some key answers to the hydrogeologic problems of this region.

In the poorly-understood Geropotamos catchment, two main factors affecting water resources were believed to be prevalent: salt water from the sea intruding into the aquifer and/or Miocene evaporates leading to groundwater salination. Increasing withdrawal of water from aquifers due to tourism (particularly new-build accommodation along coast), and agriculture (primarily olive crops) and sheep/goat farming puts considerable stress on water resources and a detailed scientific investigation was essential.

#### 1.4 General information about the study area

#### 1.4.1 Geographical information and population

The municipality of Geropotamos is located on the north-central coastline of Crete. The study area is in the northern part of the municipality, about 30 km eastern of Rethymnon city, after Geropotamos River to some km before Bali village, covering about 40 km<sup>2</sup> (**Fig. 1.1**).



**Fig. 1.1:** The black box specifies the study area which is situated on the north-central coast of Crete Island covering about 40 km<sup>2</sup>.

The study area covers 7 municipal districts (Perama, Aggeliana, Achlades, Melidoni, Panormos, Roumeli, Skepasti) including 14 villages: Perama, Dafni, Aggeliana, Alexandrou Hani, Hanothiana, Achlades, Siripidiana, Solochiana, Melidoni, Exadis, Panormos, Lavris, Roumeli, and Skepasti (**Table 1.1**) (Prefecture of Rethymnon, 2008). The most recent census in Greece came about in 2001 by the General Secretariat of National Statistical Service of Greece (General Secretariat of National Statistical Service of Greece, 2008) and the population data for each village are displayed in **Table 1.1**. This showed that 4,665 people live in the study area. Perama village is the most highly populated (1,650 inhabitants) as it is the capital of the Municipality of Geropotamos.

#### 1.4.2 Local economy

Occupations of the local population are mainly agriculture, stock farming, light industry and tourism.

**Table 1.1:** Population of study area (General Secretariat of National Statistical Service of Greece, 2008).

| Municipal District | Village         | Population | Sum   |  |
|--------------------|-----------------|------------|-------|--|
| Perama             | Perama          | 1,598      | 1 650 |  |
| Perama             | Dafni           | 52         | 1,650 |  |
|                    | Aggeliana       | 604        |       |  |
| Aggeliana          | Alexandrou Hani | 76         | 691   |  |
|                    | Hanothiana      | 11         |       |  |
|                    | Achlades        | 113        |       |  |
| Achlades           | Siripidiana     | 66         | 193   |  |
|                    | Solochiana      | 14         |       |  |
| Malidani           | Melidoni        | 391        | 470   |  |
| Melidoni           | Exadis          | 79         | 470   |  |
| D                  | Panormos        | 887        | 002   |  |
| Panormos           | Lavris          | 105        | 992   |  |
| Roumeli            | Roumeli         | 427        | 427   |  |
| Skepasti           | Skepasti        | 242        | 242   |  |
| Total SUM          |                 |            | 4,665 |  |

Olive trees are the most usual plants that someone sees throughout the whole municipality of Geropotamos. In fact, data from the General Secretariat of National Statistical Service of Greece, concerning the whole municipality of Geropotamos (16 municipal districts, 8,323 inhabitants), show that 70% of the agriculture (24 km²) belongs to olive crops and the 30% to other crops (vegetables, vines, and fruits). The farming consists mainly of sheep and goats (about 65,000 animals). It is estimated that the water demand for both agriculture and sheep/goat farming for the municipality of Geropotamos for the year 2005 is 18,000,000 m³ per year (General Secretariat of National Statistical Service of Greece, 2008).

The study area has a small industry concern, comprising 9 small olive oil factories, 2 small cement plants and 1 small local factory producing prepared feed and feed ingredients for animals.

Tourism is an important part of the local economy. A popular place is Panormos village (the northern part of the study area lying near the sea) where a lot of Greek and foreign people choose to holiday during summer season (**Fig. 1.1**). More than five deluxe hotels (4 or 5-star

hotels) have been built next to the seaside (beyond Panormos village) and several apartments and villas are located in the village.

Another place, where a lot of tourists visit, is the Melidoni Cave at the south-eastern part of the area. The cave is about 2 km NW of Melidoni village and is of big significance because of the archaeological findings which are displayed in the Archaeological Museum of Rethymnon. The cave is also considered to be the mythical home of Talos - the giant bronze protector of Crete (Psilakis, 1996).

#### 1.4.3 Water Demand

There is not a lot of information about the needs for water of the local people. The most recent reliable data from the Municipality of Geropotamos concern the years 1999 and 2000 (Tables 1.2 & 1.3). So, the water demand was calculated about 2,000,000 m<sup>3</sup> per year. Of course those data do not depict the true situation i.e. the real water consumption. In actual fact, the volume of water that was consumed for irrigation and water supply, according to employees of the Municipality, was much more than the cubic meter values that are displayed at the tables below. This is due to damage to the pipes or other kind of leaks, or even because of malfunctioning water-meters and illegal use of the water from the public wells. Hence, the values should be considered to be much higher according to the General Secretariat of National Statistical Service of Greece estimates (section 1.4.2 of this chapter).

**Table 1.2:** Water Consumption of the study area for **1999**.

| Municipal<br>District | Water Supply           |                                     | Irrigation             |                                     |  |
|-----------------------|------------------------|-------------------------------------|------------------------|-------------------------------------|--|
|                       | Number of Water-meters | Water consumption (m <sup>3</sup> ) | Number of Water-meters | Water consumption (m <sup>3</sup> ) |  |
| Aggeliana             | 445                    | 76,000                              | 391                    | 280,000                             |  |
| Achlades              | 152                    | 35,000                              | 479                    | 310,000                             |  |
| Melidoni              | 508                    | 250,000                             | 349                    | 320,000                             |  |
| Panormos              | 367                    | 90,000                              | 148                    | 90,000                              |  |
| Perama                | 896                    | 125,000                             | 135                    | 35,000                              |  |
| Roumeli               | 250                    | 37,000                              | 191                    | 110,000                             |  |
| Skepasti              | 165                    | 30,000                              | 217                    | 155,000                             |  |
| SUM                   |                        | 643,000                             |                        | 1,300,000                           |  |
| TOTAL SUM 1,943,000   |                        |                                     |                        |                                     |  |

**Table 1.3:** Water Consumption of the study area for **2000**.

| Municipal<br>District | Water Supply           |                        | Irrigation             |                                     |  |
|-----------------------|------------------------|------------------------|------------------------|-------------------------------------|--|
|                       | Number of Water-meters | Water consumption (m³) | Number of Water-meters | Water consumption (m <sup>3</sup> ) |  |
| Aggeliana             | 445                    | 70,500                 | 391                    | 284,500                             |  |
| Achlades              | 152                    | 27,500                 | 479                    | 352,500                             |  |
| Melidoni              | 508                    | 175,000                | 349                    | 355,000                             |  |
| Panormos              | 367                    | 81,000                 | 148                    | 89,000                              |  |
| Perama                | 896                    | 124,500                | 135                    | 45,500                              |  |
| Roumeli               | 250                    | 35,000                 | 191                    | 105,000                             |  |
| Skepasti              | 165                    | 32,000                 | 217                    | 163,000                             |  |
| SUM                   |                        | 545,500                |                        | 1,393,500                           |  |
| TOTAL SUM 1,939,000   |                        |                        |                        |                                     |  |

#### 1.5 Geomorphological, Geological and Hydrological setting of the study area

#### 1.5.1 Geomorphology

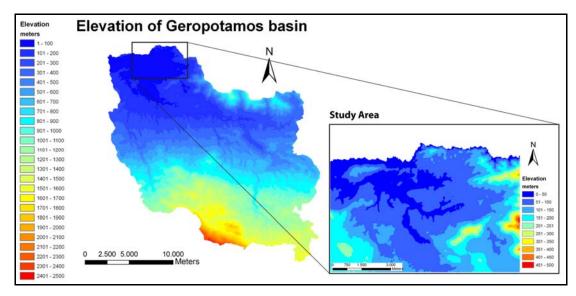
The Geropotamos basin has an estimated area of 375 km<sup>2</sup> and an elevation range of 0-2,456 m, with average elevation of 664.8 m (**Fig. 1.2**).

The study area lies in the northern part of the basin and covers 66.4 km<sup>2</sup>. The overall study area is characterized as lowland and semi-mountainous, as the elevation range is 0-502m, with an average elevation 106.4 m (**Figs. 1.2** & **1.3**).

#### 1.5.2 Hydro-meteorological and Hydrological data

Crete's climate is influenced by the Mediterranean weather systems. Dry, hot summers, and humid, mild winters are typical characteristics of weather in Crete. The rainfall, which mainly takes place in winter, ranges from 300 to 700 mm annually in the coastal zone, and from 700 to 1,000 mm in the plains of the mainland, whereas in the mountains it reaches up to 2,000 mm. July and August are the hottest months and rainfall is at its lowest during this time. Apart from the differences due to the elevation, there are significant differences between the western and eastern part too. The eastern part of Crete is drier and warmer than the western part, which is obvious in the vegetation. In addition, the temperature of

Crete shows a big variation. The annual temperature generally ranges between 17-20°C and during the summer period temperatures higher than 40°C may occur in the coastal zone (Chartzoulakis et al., 2001).



**Fig. 1.2:** Elevation of Geropotamos basin and study area classified into equal elevation zones (100 m and 50 m respectively).



**Fig. 1.3:** Google Earth image defining the area of interest with a red line. The 9 large villages are located with yellow pins (satellite image date: March 7<sup>th</sup>, 2003) (from Google Earth©2009).

Although a number of different local authorities installed meteorological stations in Crete (Water Management Authority of Crete (WMAC), Hellenic National Meteorological Service (HNMS), Institute of Geology and Mineral Exploration (IGME), Hellenic Ministry for the Environment (HME) the study area is not well covered. There are 6 stations whose data can be used for hydrological investigation (3 in the basin and 3 nearby the basin to the west) (Table 1.4). Due to limit of availability of meteorological data, it is very hard to find data from different stations for the same periods, especially for the recent past (Zarris, 2008).

**Table 1.4:** Meteorological stations at the broad area of Geropotamos basin (Zarris, 2008).

|   | Station Name      | Authority | Elevation (m) | Data Period           |
|---|-------------------|-----------|---------------|-----------------------|
| 1 | Garazo station    | WMAC      | 260           | 1996-2005             |
| 2 | Anogia station    | HME       | 740           | 1967-2000             |
| 3 | Perama station    | HME       | 90            | 1963-2006             |
| 4 | Vizari station    | WMAC      | 310           | 1969-2004             |
| 5 | Kavousi station   | WMAC      | 580           | 1969-1996 & 2006-2007 |
| 6 | Rethymnon station | MNMS      | 5.1           | 1967-1996             |

Geropotamos basin consists of 3 sub-basins: Peramatianos, Anogianos and Zonianos. The study area is situated at the northern part of the Peramatianos sub-basin (Fig. 1.4). More details about the hydrology of the study area are given in section 4.3 of *Chapter 4*.

#### **1.5.3** Geology: lithology (rock types) and Structure (nappes, thrusts and normal faults)

The surficial geology of the area is composed of Pliocene/Pleistocene marine deposits laid down on the older bedrock. Miocene biogenic limestones, marls, clays and conglomerates crop out in the central and the western part of the study area and clastic limestones and dolomites of the Tripolis and Plattenkalk nappe (the bedrock) in the eastern part of the study area. The phyllite-quartzite nappe (which forms the oldest rock of the study area) lays on the northern part of Geropotamos basin (Kalisperi et al., 2008).

The local tectonic regime of the study area is characterized by faults of NW-SE and NE-SW directions, which cut across geological formations as well as the groundwater flow direction and possible contamination from seawater intrusion. In some cases, these tectonic

structures may act as underground barriers to groundwater movement. Worth noting that tectonic features will not start at the coast, they will continue below the seabed for many kilometers into the Cretan Sea. However, geological mapping shows that major faults run from the coastline and continue inland for about 5 Km; later in this thesis it is shown how these faults may facilitate water flow inland into the aquifers from the sea.

More details about the geological status of the broad area are given in **section 2.2** of the next chapter.

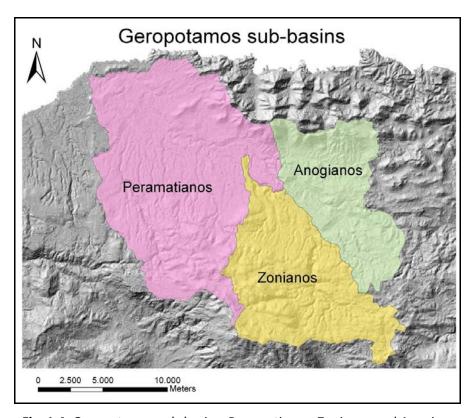


Fig. 1.4: Geropotamos sub-basins: Peramatianos, Zonianos and Anogianos.

#### 1.5.4 Hydrogeology

The northern part of the study area (along the coastline) consists of apparently impermeable formations, expecting to act as groundwater barriers for any possible seawater intrusion or groundwater discharge into the sea. The recharge of the study aquifer is expected to come from a) the eastern and southern part of the area

(mountainous area) which consists of highly permeable formations - primary recharge, and b) leakages from the dense river banks (network) - secondary recharge.

A priori hydro-geological data from water wells are available from the local authorities and data from 23 public drills (9 drills for potable water, and 14 used only for irrigation; as they were classified by the local authorities) and 2 springs were used.

The two local springs, Sweet (fresh) and Salty (brackish), are explicitly investigated as well, as they represent an unusual hydrological occurrence. Sweet and Salty springs are less than 200 m from each other but the water quality differs greatly, demonstrating the complex nature of local subterranean plumbing.

More details about the hydro-geological status of the broad area are given at **section 2.3** of the next chapter, while more information about the salty-sweet spring phenomenon is given at **section 4.5** of *Chapter 4*.

#### 1.6 Geographic Information System (GIS) as data-base management system

All the data that were collected or acquired (geological, hydrogeological, geochemical, geophysical, etc) within the frame of this thesis were inserted in GIS environment, and maps with different thematic layers were produced. GIS theory and techniques are described in full at **section 3.4** of *Chapter 3*. Maps, and generally GIS derivatives, are used throughout the thesis in appropriate places.

#### 1.7 Previous geochemical data from local authorities

There are chemical data from previous years which were made available from the local authorities. In particular, Mr. Vassilis Simitzis, geologist from the Organisation for the Development of Western Crete (OADYK), branch of Rethymnon, Mrs. Eleni Vedergiotaki, chemical engineer from the Municipality of Geropotamos, Mr. Marinos Kritsotakis,

geologist from Regional Governor of Crete, Mrs. Saia Pavlidou, geologist from Institute of Geology and Mineral Exploration - branch of Rethymnon (IGME), and Mrs. Eva Vrodaki, geologist from Prefecture of Rethymnon, were kindly provided all the existing chemical data prior to this research.

Unfortunately, these existing data are very scarce (and some of them very old) and could not be used for detailed analysis. They were useful, however, for comparison with the results from the samplings, which were took place by the author just for this study, for confirmation purposes.

#### 1.8 Thesis outline

This introduction has presented an overview of Geropotamos study area. It was actually an "overture" of the research and provided some background information concerning the known data of the region. The rest of this thesis is structured as follows:

Chapter 2 is divided into three parts including the key aspects of the thesis. It starts by describing the geology and hydrogeology of the broad study area as previous researchers has studied it by referring series of published works. Then the theory of the salination problem is explored, giving emphasis to sea-water intrusion and evaporites, as possible sources of fresh water contaminants. Finally this chapter provides a short review of each method that has been used to recognize salt-water intrusion and especially those methodologies that are used in this thesis.

The basic theory, the equipment and the procedures of all the methods used are given in **Chapter 3**. This includes a brief description of geophysical, geochemical and GIS/RS methods and techniques.

The results, the processing of the data and their analysis and modelling are presented in *Chapter 4*. This chapter details also the fieldwork carried out in Geropotamos area in order to identify the salination problem.

The relationship between the results and the methodologies are presented in *Chapter 5*. Actually it is a detailed discussion of the implementation of this research.

**Chapter 6** summarizes the major outcomes of this research and explains to what extent the aims, referred at this chapter, have been achieved. To conclude, recommendations for further research are discussed.

#### 1.9 Summary

In this introductory chapter, the overall aim and objective questions of the thesis were presented first. Then the study area was located and general information like local economy, land use and water demand was given. The geomorphological, geological and hydrological setting of the study area was described next. At the end, the thesis outline was given. The literature review of the study follows at next chapter.

## [LITERATURE REVIEW]

### **Chapter Contents**

- **▶** Introduction
- ► Geological Setting
  - Geodynamic Evolution of Aegean
  - o The Cretan Nappe Pile and the Sediments of Crete
  - Tectonics of Crete
  - o The geology of Geropotamos study area
- ► Hydro-geological Setting
- **▶** Origin of Saltwater Intrusion
  - Seawater Intrusion Problem
  - Evaporites
- ► Methods recognizing saltwater Intrusion
  - By Geophysical Methods
  - o By Geochemical Approach
  - o By GIS and RS Techniques
- Summary

#### 2.1 Introduction

This thesis deals with the geophysical and geochemical study of northern Geropotamos basin, in order to understand the origin of the saline groundwater that exists in the area. Initially, this requires understanding of the geology and hydrogeology of the area. A brief description of those matters is presented next, while the chapter ends up with some case studies of geophysical and geochemical applications.

#### 2.2 Geological Setting

The geology of Crete considered to be very interesting due to the position of the island (in the central fore arc of the Hellenic Subduction Zone (HSZ)), and the complexity of the tectonic structure. The geological history has therefore been object of intensive research. From 1848, when V. Raulin published the first papers (1848, 1856, 1860, 1867, 1869a, 1869b) about the geological status of the island, up to present, more than 1000 scientific studies have been published about the same topic internationally.

#### 2.2.1 Geodynamic Evolution of Aegean

Crete lies in the southern Aegean Sea among the islands of Kithira, Kassos, Karpathos and Rhodes, which those five islands consist the Hellenic Arc (Angelier, 1976) (Figs. 2.1 & 2.2).

The upper Cenozoic evolution of Crete is characterized by the Subduction of the African plate which it is subducted northwards under the Aegean lithosphere (Makris, 1977; McKenzie 1978; Papazachos and Comninakis, 1978, Le Pichon & Angelier, 1979). Due to the fact that the African plate moves to the north, compression between the Arabian and Eurasian plate is caused (Molnar & Tapponier, 1975). The rate of convergence consists of a 3-4 cm/year SSW-ward movement of Crete relative to stable Eurasia (Jackson, 1994; Le Pichon et al., 1995; Cocard et al., 1999; Noomen et al., 1999; Bohnhoff et al., 2001) and an 1 cm/year northward movement of Africa towards Eurasia (McKenzie, 1970; Le Pichon et

al., 1995; Taymaz et al., 1990; Bohnhoff et al., 2001), resulting in a net convergence rate of 4 to 5 cm/year at the plate boundary (**Fig. 2.2**). The Benioff zone seismicity reaches down to ca. 180 km (Makris & Röwer, 1986), being situated at a depth of ca. 140 km underneath the magmatic arc, with volcanic activity on the islands of Aegina, Milos, Santorini and Nisyros in the Aegean Sea (**Fig 2.2**).

This procedure results in the movement of the Aegean and Anatolia lithospheric plates to the west, and then the gravitational spreading of the Aegean to the east Mediterranean (McKenzie, 1972; McKenzie, 1978; Le Pichon & Angelier, 1979; Angelier et al; 1981). This gravitational spreading of the Aegean is proved by the large amount of normal faults (Upper Miocene) (Aubouin & Dercourt, 1965; Aubouin, 1971; McKenzie, 1972; McKenzie, 1978; Le Pichon & Angelier, 1979; Angelier et al., 1981; Angelier et al., 1982; Peters, 1985; Mercier et al., 1987; Mascle & Martin, 1990).

Due to this tectonic regime of extension that takes place in the Aegean area, Aegean subducts. Whereas, the Hellenic Arc (and Crete) appears to be uplifted to the north, in comparison with the Cretan Sea. Angelier & Le Pichon (1980), Angelier (1981), Le Pichon & Angelier (1981), Angelier et al. (1982) believe that this uplift of the Hellenic arc is due to a mechanism where sediments move from the Subductive plate (African) to create the new bedrock of the Hellenic arc (Barton et al., 1983). On the other hand, geological data support the option that probably compression tectonic movements were dominant in Crete, in comparison to the rest of the Aegean area (Angelier et al., 1982; Kopp & Richter, 1983; Fortuin & Peters, 1984; Meulenkamp et al., 1988, Postma et al., 1993). The aforementioned authors correlated the origin of the compression mechanism with the general extension regime of the Aegean lithosphere (Cretan Sea area), and not with the Subduction procedures. Meulenkamp et al. (1988) refer that extension begun 12-11 Ma ago.

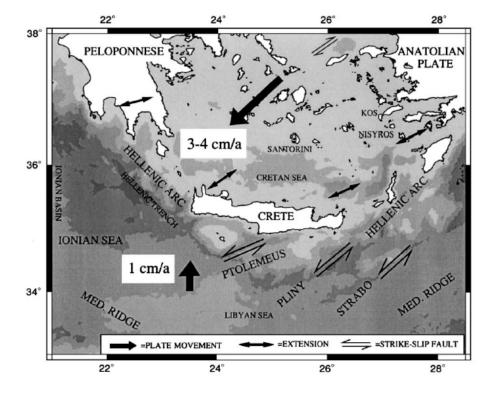
### 2.2.2 The Cretan nappe pile (Alpine and Pre-Alpine Rocks) and the sediments of Crete (Post-Alpine Rocks)

As aforementioned, the geological setting of the island of Crete is very complex and it is characterized by **pre-Alpine and Alpine rocks** (composing a pile of nappes) and **post-Alpine** 

**rocks** (Neogene and Quaternary sediments) (**Table 2.1**), i.e. rocks which formed prior, during or after the Alpine orogenesis.



**Fig. 2.1:** the Hellenic Arc consisting of five islands: Kithira, Crete, Kassos, Karpathos and Rhodes.



**Fig. 2.2:** Generalized map of the main tectonic elements of the south Aegean region (Bohnhoff et al., 2001)

#### pre-Alpine and Alpine rocks

The Cretan nappe pile has been studied extensively and numerous studies have been published by many authors. This has led to a variety of interpretations, which in many cases result in diverging views. Detailed description of the tectono-stratigraphic sequence of the rock units is not within the scope of this thesis. The stratigraphy and tectonic interpretation of the Alpine orogenesis in Crete are part of the studies of the following authors: Creutzburg (1958), Aubouin & Dercourt (1965), Fytrolakis (1967, 1972), Creutzburg & Papastamatiou (1969), Bonneau (1970, 1972, 1973, 1982, 1984, ), Epting et al. (1972), Creutzburg & Seidel (1975), Sannemann & Seidel (1976), Bijon et al. (1976), Baumann et al. (1977), Aubouin et al. (1979), Karakitsios (1979, 1987, 1989), Bonneau & Karakitsios (1979), Richter & Kopp (1983), Hall & Audley-Charles (1983), Hall et al. (1984), Robertson & Dixon (1984), Mercier et al. (1989), De Boer (1989), Alexopoulos (1990), Fassoulas et al. (1994); Jolivet et al. (1996); Kilias et al. (1994); Ring et al. (2001), Fassoulas (2004). Among others, the metamorphic conditions and ages have been studied by Seidel et al (1982), Feldhoff et al. (1991), Theye et al (1992), Koepke et al. (2002). A short description of the stratigraphic sequence, lithologies, protolith ages, and metamorphic ages of the rock units in Crete is given next.

The Cretan nappe pile can be divided into two main nappe groups: the upper nappes and the lower nappes, separated by a major thrust fault (**Table 2.1**). The lower nappes consist of: i) the Plattenkalk (called Ida nappe or Cretan-Mani sequence or Ionion nappe), ii) the Trypali (only in western Crete), and iii) the Phyllite/Quartzite nappes which reveal High Pressure-Low Temperature (HP-LT) metamorphism (during Late Oligocene-Early Miocene). The upper nappes consist of (in rising order): the Tripolis (or Tripolitza), the Pindos, and the Uppermost nappe. The second nappe group lacks of the HP-LT metamorphism. The lithology, protolith ages and metamorphic conditions are given in **Table 2.1**, while **Table 2.2** is the geological time scale for protolith rock ages symbols understanding.

#### post-Alpine rocks

Sedimentation (basin fills) has occurred in Crete approximately 13,000,000 years ago, since Miocene, beginning in the Serravallian-Tortonian, and comprises Neogene and Quaternary sediments (**Table 2.2**), covering the 1/3 of the island (Meulenkamp et al. 1979). More than 60 Neogene lithological units have been recognised the last years (e.g. Meulenkamp, 1969; Dermitzakis & Papanikolaou, 1981; Peters 1985). Meulenkamp et al. (1979) divided the sediments of Crete into six groups that can been seen everywhere in the island: i) Prina group, ii) Tefeli group, iii) Vrysses group, iv) Hellenikon group, v) Finikia group, and vi) Agia Galini group.

**Table 2.1:** The nappe pile of Crete and sediments (modified from Chatzaras et al, 2006). The nappes and sediments that are present in the study area are highlighted and only their rock types are shown in the last column (see **Table 2.2** for the protolith ages symbols understanding).

| Post-                       |                        | Quaternary sediments  |   | Alluvial deposits (Q2)  |  |
|-----------------------------|------------------------|-----------------------|---|---|--|
| Alpine<br>Rocks             | Neogene sediments      |                       | iments                                      | Marine deposits (N2-Q1)<br>Limestones, Marls, Clays, Conglomerates (N1-N2)                          |  |
|                             |                        | LP-HT<br>metamorhosed | Uppermost nappe                             |   |  |
|                             | es                     |                       | - thrus                                     | t fault -   |  |
|                             | Upper nappes           | unmetamorphosed       | Pindos nappe                                |   |  |
| sks                         | ŋ                      | - thrust fault -      |   | t fault -   |  |
| pine Roc                    |                        | LP-LT<br>metamorhosed | Tripolis nappe                              |   |  |
| e-Al                        | - major thrust fault - |                       |   |   |  |
| Alpine and Pre-Alpine Rocks |                        | ν I                   | Phyllite-Quartzite nappe                    | - Phyllites, quartzites and orthorocks (C3-T3)  |  |
| ۱۱pin                       | Ş.                     |                       |   | - thrust fault -  |  |
| 4                           | Lower nappes           | HP-LT metamorphosed   | Trypali nappe<br>(only in western<br>Crete) |   |  |
|                             |                        |                       |   | - thrust fault -  |  |
|                             |                        |                       | Plattenkalk<br>nappe                        | - Dolomites and dolomitic limestones (T3-J1) - Banded recrystallized olomitic stromatolites (C3-T3) |  |

#### 2.2.3 Tectonics of Crete

Mainly two different dominant opinions exist concerning the structural evolution of Crete, concerning the post-alpine tectonics.

a. Among others Kilias et al. (1994), Fassoulas et al. (1994), Jolivet et al. (1996), Ring & Reischmann (2002), etc suggest that the contact between the high pressure rocks and overlying thrust sheets (**Table 2.1**) is a shallow-dipping extensional detachment, which formed in the Lower Miocene.

As it is described in Fassoulas' field-guide: "North-south crustal extension in the Early Miocene (Low N1) was associated with northward- or southward-directed detachment faulting, collapse of the nappe pile, and syntectonic basin formation. The detachment faulting accelerated the removal of at least 10Km of crust now missing between the Upper, unmetamorphosed and the Lower HP metamorphosed nappes. Miocene extension consequently led to the reemplacement of the whole nappe pile and to boudinage of almost all the tectonic units lying above the Plattenkalk series" (Fassoulas, 2000).

At the same booklet it is referred that from Middle Miocene to present (Middle N1-present), the tectonic development of Crete was mainly the result of successive extensional periods that created three fault groups (three generations): A) EW trending faults, B) NS trending faults, and C) NE-SW and NW-SE large scale normal faults.

**b.** To the contrary, models for the Peloponnese suggest that exhumation of the high-pressure rocks was achieved by a compressional mechanism (e.g. Xypolias & Doutsos, 2000). A very recent work in central Crete by Chatzaras et al (2006) proposes an orogenic model for the Hellenides in Crete, resembling that proposed for the Peloponnese. Three major deformation phases (D<sub>1</sub>-D<sub>3</sub>) are distinguished at that study and their prominent structural features are presented below: D<sub>1</sub>) Early constructional phase - low angle thrusting, D<sub>2</sub>) Late constructional phase - thrust

faults and folds, and,  $D_3$ ) Extensional phase - moderate to steep normal faults, which strike WNW-ESE and NNE-NNW.

Table 2.2: Geological Time scale

| ERA       | PERIOD        | EPOCH       |              | SYMBOL     |
|-----------|---------------|-------------|--------------|------------|
|           |               |             | Holocene     | Q2         |
|           | Quaternary    | Pleistocene |              | Q1         |
|           |               |             | Pliocene     | N2         |
|           |               |             | Messinian    |            |
|           | Neogene       | ne          | Tortonian    |            |
| CENOZOIC  | reagene       | Miocene     | Serravallian | N1         |
|           |               | Σ           | Langhian     |            |
|           |               |             | Burdigalian  |            |
|           |               | (           | Oligocene    | P3         |
|           | Paleogene     |             | Eocene       | P2         |
|           |               | ı           | Paleocene    | <i>P</i> 1 |
|           |               | Upper       |              | К2         |
|           | Cretaceous    | Lower       |              | К1         |
|           | Jurassic      | Upper       |              | J3         |
|           |               | Middle      |              | J2         |
| MESOZOIC  |               | Lower       |              | J1         |
|           |               | Upper       |              | Т3         |
|           | Triassic      | Middle      |              | T2         |
|           |               | Lower       |              | T1         |
|           | Permian       | Upper       |              | P2         |
|           | Carboniferous | Lower       |              | P1         |
| PALEOZOIC |               | Upper       |              | C3         |
|           |               | Middle      |              | C2         |
|           |               | Lower       |              | C1         |

#### 2.2.4 The geology of Geropotamos study area

The geological setting of the Geropotamos study area has been examined poorly in the past and mainly by local authorities. The investigations were based on the available literature and some exploratory boreholes from the local geologists. IGME (branch of Rethymnon)

has published some geological studies for the area, but in the most cases were included as a section in hydro-geological studies. Of course, there is a detailed geological map (Perama sheet) 1:50,000 from IGME that includes the study area at the north-eastern part of the map.

IGME, branch of Rethymnon, and, specifically, the geologist M. Knithakis published some geological/ hydrogeological studies about the area of Rethymnon prefecture, where the study area was included. At the report of 1995 ("geological & hydrogeological setting of Rethymnon" issue), Knithakis gives a detailed description of the geology (lithology and tectonics) of Retyhmnon, but the study was based on old hat ideas about the nappe pile of Crete (Knithakis, 1995).

The information used for that section, in order to state the geology of the area, is acquired mainly by the IGME geological map (Perama Sheet) (IGME, 1991). The geological mapping was carried out by I. Mylonakis, geologist of IGME, from 1982 to 1987.

The geology of the Geropotamos study area (Northern part of Geropotamos basin) is composed mainly by some of the oldest rocks in Crete (Phyllite/ Quartzite and Plattenkalk nappes) covered by Neogene and Quaternary deposits. At the western part of the broad study area lays the Tripolis nappe, but it is out of the range of this thesis and there has been no geophysical or geochemical research on Tripolis unit (Fig. 2.3 & Table 2.1).

At the northern part near the coastline lays the Phyllite/ Quartzite nappe (C3-T3). This unit is comprised by low-permeable rocks (Phyllites and Quartzites) and it is considered to be a "block" for the seawater by the locals. According to Fassoulas' N-S geological cross-section in the North-central part of Crete, nearby the study area (Fig. 2.4) the thickness of this nappe is approximately 500m. At the eastern part of the target area the roots of the Talea Ori Mountain are situated. That part of the mountain consists of dolomitic limestones and dolomites at the southern part, and stromatolites of marbles and dolomitic limestones at the northern (Plattenkalk nappe). The Phyllite/Quartzite nappe overlies the Plattenkalk nappe in thrust contact. Pliocene/ Pleistocene marine deposits and Miocene biogenic limestones, marls, clays and conglomerates crop out in the central and the southern part

covering the largest piece of the study area. The Neogene sediments (N1) are overlain by the youngest sediments, the Marine (N2-Q1), following a presumed sequence. At the top of the stromatographic commun the Alluvial deposits (Q2) are present (Fig. 2.5).

The local tectonic regime of the study area is characterized by normal faults of NW-SE and NE-SW directions, as it is expected (section 2.2.3 of this chapter) (Fig. 2.3). These faults define the groundwater flow direction and possible contamination from seawater intrusion. In some cases, these tectonic structures may act as underground barriers bounding the groundwater movement. The only worry, concerning the "contribution" of tectonic in the aforementioned water contamination, comes from the fact that the tectonic features start from the coastline and seems to continue for about 5 Km (section 2.3 of this chapter).

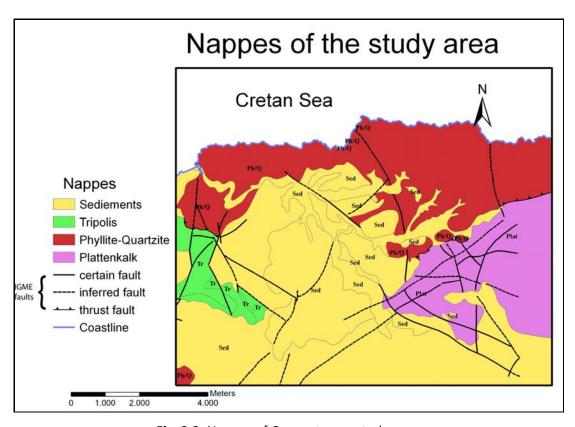
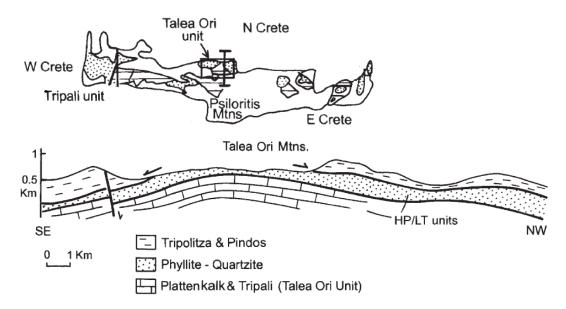


Fig. 2.3: Nappes of Geropotamos study area

#### 2.3 Hydro-geological setting

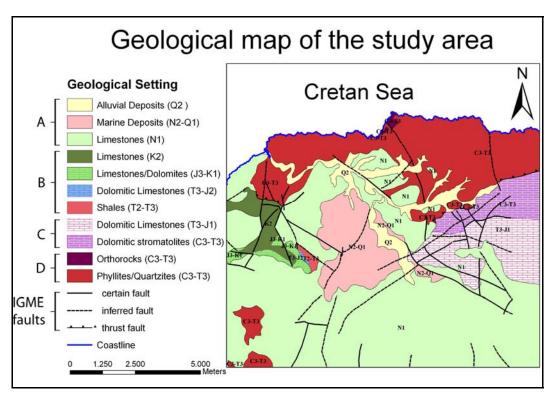
A large number of hydrological studies have been written about Crete, and some of them exclusively about Rethymnon region. These investigations attest one more time the immense value of freshwater and the increased demand. Some public reports were written about the hydrological setting of Rethymnon, mainly by accomplishing exploratory boreholes and chemical analyses. IGME (branch of Rethymnon), OADYK (Organisation for the Development of Western Crete), Regional Governor of Crete, municipality of Geropotamos, and many others tried to acquire and interpret hydrogeological and hydrogeochemical data from all over the Rethymnon prefecture. Nevertheless, Geropotamos, the study area of this thesis, has been poorly investigated and some assumptions (especially about the contamination of the groundwater) are still unconfirmed.



**Fig. 2.4:** Simplified cross-section of central-northern Crete showing the main thrust sheets and nappes. (Robertson, 2006 - modified from Fassoulas, 2000)

The first integrated study concerning the hydrogeology of the prefecture of Rethymnon is that of 1995 by IGME (branch of Rethymnon) (Knithakis, 1995) which was assigned from 1983 by the Greek ministry of the Environment. That study comprises six volumes: geological/hydrogeological description, exploratory boreholes, hydro-meteorological data, geochemical analyses, maps, and conclusions. The northern part of Geropotamos basin is referred at this study and the contamination problem of the area is investigated for the first

time. After some chemical analyses (mainly from analysing samples from the Salty spring), they have assumed that there are evaporites (halite) in the Neogene. The reason why they reached that conclusion is because of the phyllite/quartzite nappe that lies near the coast and generally it works like a boundary to the seawater intrusion. Another reason is the gypsum that has been found in Pigi-Adele region western to the study area (section **2.4.2** of this chapter). There is no further study about this problem up to the present and never evaporite evidence was found in Geropotamos basin, either from exploratory boreholes or hydrowells.

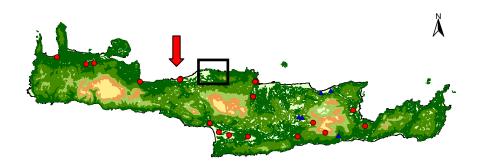


**Fig. 2.5:** Geological status of the study area (modified from IGME map). Note the prominent approximately North-South-orientated faults intersecting the coastline, that may permit pathways of saltwater intrusion. A: Sediments, B:Tripolis nappe, C: Plattenkalk nappe, D: Phyllite/Quartzite nappe

The study of Crete by the Regional Governor of Crete in 1999 (by the leadership of the geologist Marinos Kritsotakis) (Regional Governor of Crete, 1999) is a full and detailed study about the hydrogeological setting of Crete and the water resources (data collected from IGME, OADYK (Organisation for the Development of Western Crete), OANAK (Organisation for the Development of Eastern Crete), Regional Governor of Crete, Ministry of Agriculture

and Ministry of the Environment, local Prefectures, local Municipalities, etc.). It is divided into three phases. The first one includes data collection, data processing and analyses, and data base construction; and the other two phases consist mainly of management and development plans. Concerning the Geropotamos study area and the contamination problem, this project does not make any further research (except some more chemical analyses) but reviews the IGME study of 1995 (see above). So, they reach the same conclusion: halite existence as the contamination source.

From 2000 the Regional Governor of Crete has began the installation of an on-line telemetric hydrologic network and up to now 21 telemetric hydrologic stations have been installed all over Crete (**Fig. 2.6**). The parameters that are monitored in real time from those 21 stations (boreholes and wells) are: depth, electrical conductivity (EC), and temperature. The closest station to the study area has been installed from 2004, but it is out of the range of the targeted region, and no data, coming from this borehole, have been used.



**Fig. 2.6:** The hydrogeologic telemetric network of Crete (Regional Governor of Crete, 2008). The red arrow indicates the closest station (Platanias station) western to the study area (indicated by the black box).

Another project that the Regional Governor of Crete was involved is the EU-funded project called MEDIS. The overall goal of MEDIS is to contribute towards the sustainable use of water on islands of the Mediterranean where conflicting demand for water is combined with a wide range of hydrological, social and economic conditions. The study is carried out at a catchment-scale on major islands of the Mediterranean extending from the west to the

east: Corsica, Crete, Cyprus, Mallorca and Sicily. Except of the Regional Governor of Crete, the MEDIS consortium consists of many Institutions including universities, research centres and organizations from Germany, Cyprus, Greece, Italy, France, and Spain.

The project was mainly concerning the water management of the islands. However, in the frames of MEDIS some geophysical research was performed in Crete studying the seawater intrusion in two areas. More information about this work is given at section **2.5.1** of this chapter.

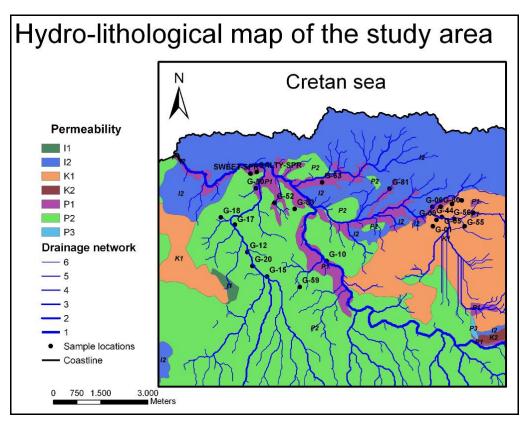
The geologist Vassilis Simitzis from OADYK, has investigated the Geropotamos basin for more than 25 years and has constructed more than fifteen boreholes at the broad region. Data from the organisation (OADYK), which include logs and the chemical analyses (whenever they were available) have been provided to the author, contributing to the completeness of this thesis. After personal collaboration with him, he is the first one that introduces the option of seawater intrusion as a contaminator, contrarily to the previous studies, however without any evidence, except some observations of the fieldwork.

**Figure 2.7** and **Table 2.3** give some information about the hydrogeological situation of the study area. As already mentioned at the introduction, the northern part of Geropotamos basin (along the coastline) consists of impermeable formations (I2) (phyllites/quartzites), expecting to act as groundwater barrier for any possible seawater intrusion. The recharge of the study aquifer is expected to come from Talea Ori, the eastern and southern part of the area, which consists of high permeable formations (K1) (dolomitic limestones and stromatolites), and from leakages from the dense river banks (network).

Two different types of aquifer are expected based on rock types: a) a phreatic aquifer, into porous media (Quaternary and Neogene sediments), and b) deep aquifer into fracture zone (phyllite/quartzite nappe)/ karstic rocks (plattenkalk) - secondary porosity (Kallergis, 2001).

A priori hydro-geological data from hydrowells, which were available from the local authorities, were collected. In the study area data from 23 public drills exist (9 drills for potable water, and 14 used only for irrigation; as they were classified by the local

authorities (**Fig. 2.8**)). The groundwater of the drills, which are used only for irrigation, is characterized by high salinity and conductivity. Note that at the study area many exploratory drills have been constructed, especially at the central part (where no drills are situated), but then they were abandoned not due to the small amount of water but due to their bad water quality.

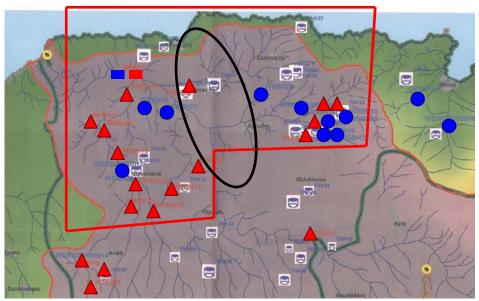


**Fig. 2.7:** Hydrolithological status of the study area. See **Table 2.3** for explanation of key colours.

**Table 2.3:** The hydrolithological classification of the geological units based on permeability is presented (Regional Governor of Crete, 1999).

| l1 | impermeable, low-very low permeability             |
|----|--|
| 12 | impermeable or selective low-very low permeability |
| P1 | Granural deposits, fluctuating permeablility       |
| P2 | Deposits, medium-low permeability                  |
| P3 | Granural, low-very low permeability                |
| K1 | Karstic, high-medium permeability                  |
| К2 | Karstic, medium-low permeability                   |

The increasing density of those drills (mostly the private ones) influence adversely the environment (the quantitative and qualitative characteristics of the coastal aquifers) is also investigated. Finally, the logs from available boreholes are the only reliable geological information, so they are used for calibration and confirmation of the geophysical modelling.



**Fig. 2.8:** Quality classification of the waters of the study area as it is used by the municipality of Geropotamos (modified from Zarris, 2008) <u>Red triangles</u>: irrigation wells, <u>blue circles</u>: wells for drinking purpose, <u>red and blue rectangulars</u>: Salty and Sweet spring respectively, <u>cylinders</u>: water tanks. The black ellipse indicates the lack of wells at the center part of the study area.

The two local springs, Sweet and Salty, lying at the north-western part of the study area, are explicitly investigated as well, as they consist an unusual hydrological occurrence. The distance between them is less than 200m from each other but the water quality differs significantly. Actually, the groundwater from the Sweet spring is considered to have the best quality and the sample from the Salty spring, the worst (based on 16 chemical parameters according to WHO (World Health Organization) regulations). The names of the springs, that local people have gave, are apparently due to this difference in water quality.

#### 2.4 Origin of Saltwater Intrusion

Saline groundwater can lead to serious problems for water supply, especially under arid climate conditions. To define saline groundwater, we will consider the concentration of chloride exceeding 250 mg/L and electrical conductivity exceeding 2500  $\mu$ S/cm (WHO; 2004).

In addition to anthropogenic effects (e.g. fertilizer, waste deposits) the main origins of saline groundwater are (Kirsch, 2006):

- Seawater intrusions in coastal areas
- Salt domes
- Enhanced mineral concentration in groundwater under arid conditions

In this section, a brief description of two main salination problems, that it is assumed to influence Geropotamos basin, is following: **seawater intrusion** and **evaporites**. As already mentioned, up to present the contamination of Geropotamos is still a debate problem, and no well-documented answer exists.

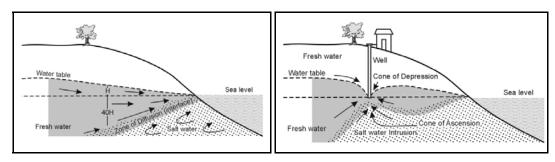
#### 2.4.1 Seawater Intrusion Problem

Where aquifers form a coastline, groundwater discharges into the sea. In addition, seawater intrusions occur due to higher density (slightly heavier) of saltwater than freshwater. As a result, in coastal areas the seawater forms a saline wedge below the fresh water, i.e. freshwater is underlain by saltwater, and the boundary (or salt/freshwater interface) between them (in a state of dynamic equilibrium) is moving with the seasonal variations of the water table (transition zone of mixed salinity).

Ghyben (Drabbe and Badon Ghyben, 1888-1889) and Herzberg (1901) were two European scientists who independently recognized the known Ghyben-Herzberg relationship. This principle empirically relates the depth of the interface to the elevation of the land surface

under a set of simplifying assumptions: the theoretical interface occurs at a depth below sea-level that is 40 times the height of fresh water above sea-level. Of course, geological variability makes the formula more complex.

The equilibrium between freshwater and seawater can be disturbed by high pumping rates from a coastal aquifer. So, the fresh-water level gets lower and the seawater intrudes further into the aquifer (Fig. 2.9b), making the water of the pumping boreholes saline.



**Fig. 2.9: (a)** Balanced and **(b)** disturbed salt/freshwater interface in a coastal area (Kirsch, 2006; after Keller, 1988)

There is a scientific meeting that it is important for hydrogeologists whose subject is the seawater intrusion problems. The Saltwater Intrusion Meeting (SWIM) has been held in different European countries on a biennial basis since 1968 with an increasing number and diversity of participants. The scope of SWIM in the beginning was a pure exploitation of coastal and continental aquifers that may be affected by salt water to all aspects of a sustainable development of the groundwater resources. Today, the categories in which the published papers were grouped in the proceedings shifted constantly. Geological, geophysical, hydrogeological, hydro-geochemical and isotopic research were described as providing the data for the modelling work. In every meeting people who are interested in saline groundwater issues are brought together, many new methodologies and new ideas are exchanged, and discussed results on saline groundwater problems (SWIM, 2009). On the "Methods recognizing saltwater intrusion" section (section 2.5), some case studies of different methods (geophysics and geochemistry) that have been presented on some of the SWIM meetings are discussed.

#### 2.4.2 Evaporites

Evaporites are sediments deposited from natural waters that have been concentrated as a result of evaporation. The source waters can be either marine or continental in origin. Evaporite deposits are important sources of gypsum, halite, sylvite, and other minerals. Substantial thicknesses of evaporites are buried in some sedimentary basins. There, they act as important barriers to groundwater flow, but they are also susceptible to dissolution by groundwater. Buried evaporites can migrate slowly though overlying sediments in the form of salt domes (Ingebritsen and Sanford, 1998).

In Greece, and especially in Crete, evaporites have been formed mainly due to the Mediterranean Salinity crisis that took place in the upper Neogene period. That event caused the creation of gypsum that is lying in the Neogene formations and in phyllite/quartzite nappe in some places all over Crete. In the vicinity of the study area, south-eastern to Rethymnon city and western to Geropotamos basin, at the Pigi-Adele Neogene basin (Fig. 2.10), gypsum has been found during drillings and it is the reason for the groundwater contamination of that region (Regional Governor of Crete, 1999).

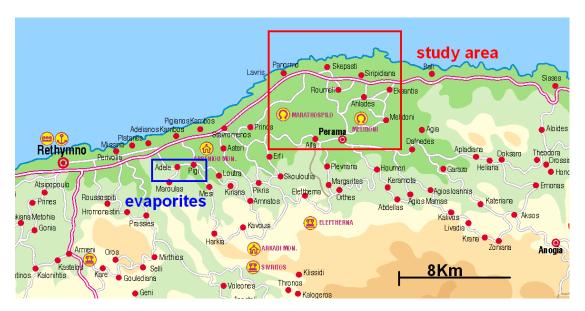


Fig. 2.10: Map showing the study area (red box) and the closest evaporite evidence in boreloles at Pigi-Adele region (blue box).

#### 2.5 Methods recognizing saltwater intrusion

Generally the salination problem all over the world has been studied by several methodologies, including geophysics, geochemistry and remote sensing analysis. This section reviews briefly some of the most important works, where mainly seawater intrusion issues have been studied with success, using the same tools as the ones used for this thesis.

#### 2.5.1 By geophysical methods

Among all geophysical methods, resistivity and electromagnetic methods considered to be the leading ones in the exploration of groundwater. Many successful applications of these methods reported in the literature have to do with seawater intrusion detection and fresh-saline groundwater interface configuration.

Much has been published on the Transient ElectroMagnetic (TEM) technique, including applications in hydrogeological research (e.g. Fitterman and Stewart, 1986; Eddy-Dilek, 1997; Richards et al, 1998; Meju et al, 2000; Guérin et al, 2001; Danielsen et al, 2003; Young et al., 2004; Lepper and Elmore, 2005; Metwaly et al, 2006, Barrett et al, 2006; MacNeil et al, 2007), and for studying the specific problem of salt water intrusion (Mills et al. 1988; Yuhr and Benson, 1995; Hoekstra et al. 1996; Richards et al. 1995; Young et al., 1998; Chen, 1999; Land et al, 2004; Papadopoulos et al., 2004; Nielsen et al, 2006; Kontar and Ozorovich, 2006).

Vertical Electrical Sounding (VES) technique is used fulsomely for groundwater investigations (e.g. Yadav and Abolfazli, 1998; Salem, 2001; Dhakate and Singh, 2005; Soupios, 2007) and seawater intrusion mapping (e.g. Shaaban, 2001; Frohlich and Urish, 2002). Many successful applications combine VES and TEM surveys as well (e.g. Al-Sayed and El-Qady, 2007), while joint inversion of DC and TEM soundings has been attempted (e.g. Albouy et al, 2001, Barsukov et al., 2007).

This section reviews briefly some applications of using TEM, and VES techniques (the same geophysical methodology that used for this thesis). Moreover, joint inversion or

combination of them with other geophysical techniques, in coastal regions for hydrogeological investigations. The point is to show the wide application that those methods have found globally and the good results that have been extracted for this kind of problems.

#### Medis program

Within the frame of MEDIS EU-project (described in **section 2.3** of this chapter) a catchment on Crete (Tybaki) was selected for field surveys, as the geophysical objective within MEDIS was to investigate possibilities and limitations for aquifer characterization and detection of saline intrusions on Mediterranean islands. Both areas are mainly used for agriculture, which takes place preferable in greenhouses or plantations.

Tymbaki catchment lies at the south coast of the island. It is located in the Messara plain, close to the sea and near to the town of Tymbaki. Two surveys using TEM, combined with VES and radio-magnetotellurics (RMT), were carried out in spring and summer 2003. A limited area in the north of Tymbaki was identified to be affected by a saline intrusion. This analysis is verified by water samples and corresponds with information from local farmers. In the south of Tymbaki a second area with low-resistivities above ground water level was found, whereas the decreased resistivites are assigned to other ground water contaminations. As a conclusion, the authors refer that TEM is the best suited method for surface geophysics in Mediterranean coastal area, since other methods often fail due to the small field sizes and the multitude of fences and greenhouses. Nevertheless other methods are recommended in some cases and a careful field reconnaissance is always essential (Pipatpan & Blindow, 2005).

#### **SWIM** meetings

As described in **section 2.4.1** of this chapter SWIM meetings every two years provide a great opportunity for hydrogeologists to gain knowledge of the new methodologies and applications concerning saline water intrusion globally. A few case studies from the two

more recent meetings of 2006 and 2008, where TEM and VES geophysical techniques have been used, have been selected and presented next.

At the 19<sup>th</sup> SWIM of 2006 in Italy the following two studies were presented using TEM technique as tool for saltwater intrusion characterisation in Southern Spain and Nabeul-Hammamet (Tunisia) regions respectively.

A TEM survey was carried out in Motril Salobrena coastal aquifer in order to define the characteristics of the fresh water-salt water contact in the aquifer, as boreholes existing in the area are not deep enough to directly locate the contact. Four profiles performed and the results of the first profile managed to detect zones of the aquifer that were affected by seawater more than 150m deep (Duque-Calvache et al., 2006).

At the second study selected, the TEM survey in Nabeul-Hammamet was able to map the interface between fresh and salt water as well. One dimensional interpretation of the TEM data was correlated to existing data from borehole logs (Gamma Ray, Spontaneous Potential, Resistivity) giving good results (Trabelsi et al., 2006).

The 20<sup>th</sup> SWIM of 2008 took place in Florida USA (out of Europe). Two studies follows that were presented using TEM and resistivity methods for saltwater intrusion mapping.

Another study from Duque et al. was presented, using two geophysical techniques (TEM and VES) in the Motril Salobrena coastal aquifer. The two methods carried out in different chronological periods (TEM data acquired 25 years after VES data) and the analysis of the water table trend showed a similar situation after 25 years (Duque et al., 2008).

The next application was in Los Angeles Country of California, where the TEM compared with High Resolution Electric Resistivity (ER) in order to determine which method is the most suitable for full-scale intrusion mapping of the basin. The conclusion is that TEM proved the most effective at measuring brackish and salty water with the smallest footprint and minimal noise. The results also compared favorably to nearby monitoring wells (Johnson et al, 2008).

#### Seawater intrusion mapping in Israel

More than 25 years Goldman M., Kafri U. and Melloul A. evaluate seawater intrusion and apply the TEM technique in order to delineate seawater intrusion into the multiple aquifer system of the Mediterranean coastal aquifer of Israel (Melloul and Aberbach, 1984; Goldman et al, 1988; Melloul and Bibas, 1991; Goldman et al, 1991; Kafri et al., 1997; Goldman and Gendler, 2002; Goldman and Kafri, 2002; Goldman et al, 2003; Goldman & Kafri, 2004; Kafri and Goldman, 2006; Kafri et al., 2007). All those years they have constructed a dense TEM grid, and combining other geophysical methods as well (e.g. reflection seismics), they have succeed a detailed study of the whole coast of Israel.

#### 2.5.2 By Geochemical Approach

Geochemical parameters and processing of them, using quality factors (e.g. Na:Cl, Mg:Cl, etc) and special diagrams (e.g. Piper, Durov, Stiff), are good tools for indicating the origin of the salination of the groundwaters. In some occasions, like Geropotamos basin, the demarcation between the contaminators is hard, but a lot of applications have shown that geochemistry can give reliable answers.

Tremendous number of hydro-geochemical researches has taken place in coastal regions by taking samples from boreholes nearby the sea with the aim to contributing to the understanding of the processes which effect groundwater quality (e.g. Jeen, 2001; Kim et al, 2003; Pulido-Leboeuf, 2004; Sivan, 2005; Subba Rao et al, 2005; Park et al., 2005; Petalas and Lambrakis, 2006; El Moujabber, 2006; Lee and Song, 2007; Psychoyou et al, 2007; Panagopoulos, 2008; de Montety, 2008; Petalas, 2009; Aris, 2009) or trying to understand the source of contamination (Petalas and Diamantis, 1999; Sanchez-Martos, 1999; Perry et al, 2002; Sanchez-Martos, 2002).

#### 2.5.3 By GIS and RS techniques

Geographic Information System (GIS) and Remote Sensing (RS) methods are considered the recent years as very effective tools in groundwater modelling and management. Specifically, GIS methods have been extensively used in groundwater vulnerability mapping (e.g. Loague et al., 1996; Rupert, 2001; Lake et al. 2003; Babiker, 2007; Kouli et al., 2008). Moreover, RS analysis, and specifically application of special filtering techniques on satellite images for major tectonic features, geomorphologic structures, etc detection, has shown great results in the past (e.g. Argialas et al, 1988; Rokos, 2000).

#### 2.6 Summary

This chapter was mainly a review in previous studies, where it described briefly the geological (rock types and tectonics) and hydrogeological status of Crete, focusing in the study area. Then, seawater intrusion and evaporites (the two hypotheses) problems were introduced. Finally, some case studies were referred, where the same methodologies (geophysical and geochemical) have been applied successfully in the past in different places.

## [METHODS]

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- **▶** Introduction
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    - Transient Electromagnetic Method (TEM) Fundamentals
    - The TEM-Fast 48 System
  - o Resistivity method VES technique
    - Basic principles
    - Vertical Electrical Soundings
    - Instrumentation for DC measurements
- **▶** Geochemical Analyses
  - Collection & Preservation of Samples
  - Physical and Aggregate Properties
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- ► GIS and Remote Sensing methods and techniques
- Summary

#### 3.1 Introduction

In order to reach the objectives that were given in *Chapter 1*, this thesis applies a combination of methodologies, of which geophysics, and geochemistry are the principal ones; and by attempting a preliminary remote sensing analysis. This chapter describes all the methods used in this research.

#### 3.2 Geophysical measurements

Two geophysical measuring tools were used for this project to observe the electrical conductivity changes with depth. This section reviews the theoretical background of Transient Electromagnetic and Vertical Electrical Soundings and the instrumentation of those techniques. Transient electromagnetic theory is described in more detail, as the EM survey is the main part of this thesis.

#### 3.2.1 Electromagnetic Method - Transient ElectroMagnetic (TEM) Technique

The TEM technique (known also as Time-Domain ElectroMagnetic technique, TDEM) is relatively a young method in comparison with other EM methods, as it has been developed and re-fined mainly in the mid-1980s. The reason is that the technology was not at the same level as it is today, because TEM data acquisition and interpretation require sophisticated electronics and modern computers, respectively (Kirsch, 2006). During the last few years TEM method has become increasingly popular for hydrogeological purposes with very good results (section 2.5.1 of *Chapter 2*).

In the first part of this section, some general idea of this technique is given and then follows a more detail description of this geophysical tool, based on the Fast TEM technology.

#### 3.2.1.1 Electromagnetic methods - Fundamentals

Most of Electromagnetic (EM) techniques (Transient-EM (TEM), Controlled source audiofrequency magnetotellurics (CSAMT), Frequency Domain EM (FDEM), Ground Penetrating Rarar (GPR), etc) use a controlled artificial electromagnetic source as a primary field that

induces a secondary electromagnetic field. On the other hand, other EM methods use the Earth's natural EM fields as well (e.g. Magnetotelluric method).

The EM methods have many advantages. They are sensitive to electrical resistivity and electrical permittivity over a volume of ground where induced electric currents are present. In comparison with other geophysical methods, EM provides deeper penetration depth capability and grater resolving power (Everett and Meju, 2005). However, the main concerns in all EM methods are cultural noise sources, such as power lines, pipelines, etc, that decrease the signal-to noise ratio. EM induction methods, like TEM, are not the most widely used in hydrogeological studies. However, TEM is the most promising and versatile geophysical method for this purpose.

General EM theory can be found in the literature (e.g. Edminister, 1994; Stratton, 2007, etc) and it is beyond the scope of this section. Next, just an introduction of electromagnetism is given, which is actually the backbone of the TEM technique. The principle behind Electromagnetic methods (EM) is governed by Maxwell's equations that describe the coupled set of electrical and magnetic fields change with time.

Electric and magnetic fields are connected by Maxwell's field equations (differential form):

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$
 (3.1)

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$$
 (3.2)

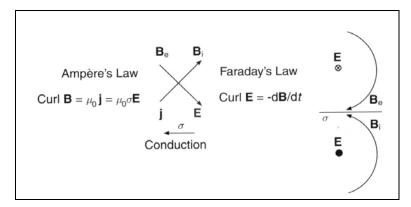
$$\nabla \cdot \mathbf{B} = 0 \tag{3.3}$$

$$\nabla \cdot \mathbf{D} = \rho \tag{3.4}$$

where  $\mathbf{E}$  is the electric field (in  $V m^{-1}$ ),  $\mathbf{B}$  is magnetic induction (in T),  $\mathbf{H}$  is the magnetic intensity (in  $A m^{-1}$ ),  $\mathbf{D}$  is electric displacement (in  $C m^{-2}$ ),  $\mathbf{J}$  is the electric current density

owing to free charges (in C m<sup>-3</sup>), and  $\rho$  is the charge density (C m<sup>-3</sup>). Curl ( $\nabla \times$ ) and div ( $\nabla \cdot$ ) are vector calculus expressions.

A time-varying external magnetic field,  $\mathbf{B}_{e}$ , in accord with Faraday's Law (**Equation 3.1**), induces an electric field  $\mathbf{E}$ , which then induces a secondary, internal magnetic field  $\mathbf{B}_{i}$ , in accord with Ampère's Law (**Equation 3.2**) (**Fig. 3.1**).



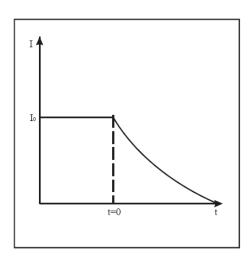
**Fig 3.1:** Diagram explaining graphically the Maxwell's Equations (Simpson & Bahr, 2005)

#### 3.2.1.2 Transient Electromagnetic Method (TEM) - Fundamentals

In this section a brief description of TEM method is provided. An analytical presentation of the method can be found by McNeill (1980), and Nabighian and Macnae (Nabighian & Macnae, 1991).

TEM is a controlled source electromagnetic (EM) method (the energy source is a transient EM signal) that uses large loops laid on the ground as a transmitter/receiver. The method can be applied in many different configurations, no direct electrical contact with the ground is required, can be used to investigate the top few meters of ground till hundreds of meters in depth (depend on the size of the antenna), it is a fast and cost effective method, but it does not work properly in high resistive region and is susceptible to interference from nearby (buried or not) metal pipes, cables, fences, vehicles and induced noise from power lines.

In the Transient Electromagnetic method (TEM) a strong direct current (DC) is passed through an ungrounded loop. The flow of the current in the loop creates a primary electromagnetic field. The rapid termination of the current generates a system of induced currents in subsurface conductors, called eddy currents, which flow in such way as to preserve the magnetic field that existed before the current was switched off. The eddy currents and the secondary magnetic field, which they produce, decay with time, according to the "Zero Input Response" ( $i(t) = i(0)e^{-t/\tau}$ , (more details in **Fig. 3.2**), and induces a voltage in the receiver coil.

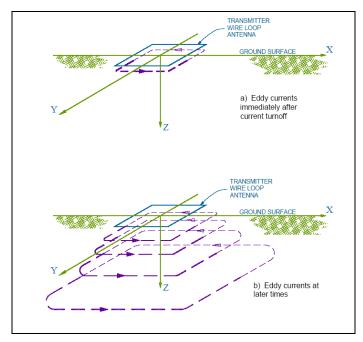


**Fig. 3.2** The Zero Input Response (ZIR), also called the natural response, of an RL (resistor-inductor) circuit describes the behavior of the circuit after it has reached constant voltages and currents and is disconnected from any power source. It is called the zero-input response because it requires no input.

It can be shown that on or above the surface of the earth at any given time after switch off, the combined effect of all induced currents in the ground can be approximated by the effect of a single current filament of the same shape as the transmitter loop, that moves outwards and downwards with time This is known as the "smoke ring" concept and it is useful for visualising the complex process occurring in the earth (**Fig. 3.3**). The amplitude of the current filament decreases with time as does its velocity in a homogeneous earth.

"Each TEM measurement is treated as a sounding; many measurements must be carried out to produce many soundings, which may then be interpreted as a collection of soundings. As for all electrical and electromagnetic methods, TEM measurements yield information about variations in the earth's **electrical resistivity**", Dept of Geography - University of British Columbia, 2009. The depth of investigation depend on the size of the antenna (the bigger the loop size, the deeper the investigation), and on the type of the rocks.

Three TEM measuring array configurations are used: central loop, offset loop and the coincident loop (or single-loop). For this project the coincident loop configuration was used. It is the most simple, and the perhaps the most usable. The same wire loop is used for both transmitter (**TR**) and receiver (**REC**), and major advantages of this loop configuration include good signal-to-noise ratios and a uniform response as a function of transmitter location. However, a homogeneous relief area is required.



**Fig. 3.3:** The secondary field immediately begins to decay, in the process generating additional eddy currents that propagate downward and outward into the subsurface like a series of smoke rings (French, 2002; after McNeil, 1990).

#### 3.2.1.3 The TEM-Fast 48 System

TEM-Fast 48 system, developed by AEMR Ltd (TEM-Fast 48 manual, 2007), is a new geophysical tool and it was used in this project, with coincident loop configuration. That new TEM instrument is intended for electromagnetic researches within the limits of first 350 m depth (depending on the ground resistivity). The main areas of application are: search of

mineral deposits; geological researches, research of rock samples; and of course hydrogeological researches.

TEM-FAST originally was developed within the framework of the international program MARS-94" and intended for installation on the Martian module with the purpose of TEM sounding of the surface of Mars. It follows that by its development increased requirements to reliability of the tool in extreme conditions were set.

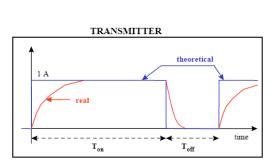
#### 3.2.1.3.1 TEM-Fast 48 Components

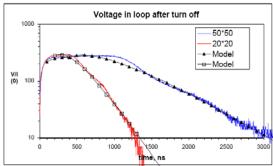
TEM-FAST includes: i) the **generator** of unipolar rectangular pulses (transmitter), ii) the measuring block providing registration of the signals (**receiver**), iii) the control block (**controller**), and iv) the **power supply** (battery). All devices are assembled in a single case.

#### i. Transmitter (generator)

The generator develops rectangular pulses of a current, which are passed through the transmitting antenna. The form of the pulses is shown in **Figure 3.4a**. The real antenna can be presented as inertial electrical system with distributed inductance, capacitance and resistance. At the moment of switching off (namely this moment represents the special interest at measurements of transients!), current in the antenna sharply differs from the ideal. Voltage profiles in the transmitter antenna of  $50 \times 50$  m and  $20 \times 20$  m size at the moment of the current off, measured by a digital oscilloscope are shown in **Figure 3.4b**. Graph of the voltage (Model) calculated for the line with distributed parameters is presented in the **Figure 3.4b** as well.

The parameter **Ton + Toff** of the current's pulses TEM-FAST 48 (**Fig. 3.4**) depending on a measurement mode (FILTR = 50/60 Hz) is given in **Table 3.1**.





**Fig. 3.4:** a) Pulses developed by the generator (real & theoretical), and b) Voltage profiles in the transmitter antenna of  $50 \times 50$  and  $20 \times 20$  m after turn off, and models (TEM-Fast 48 manual, 2007).

**Table 3.1:** The parameter **Ton + Toff** of the current's pulses TEM-FAST 48 (**Fig. 3.4**) depending on a measurement mode (FILTR = 50/60 Hz) (TEM-Fast 48 manual, 2007)

| Key | Max time (μs) | Active Time gates | Ton + Toff (50Hz)<br>(ms) | Ton + Toff<br>(60Hz) (ms) |  |
|-----|---------------|-------------------|---------------------------|---------------------------|--|
| 1   | 64            | 16                | 0.3125                    | 0.26                      |  |
| 2   | 128           | 20                | 0.625                     | 0.52                      |  |
| 3   | 256           | 24                | 1.25                      | 1.042                     |  |
| 4   | 512           | 28                | 2.5                       | 2.08                      |  |
| 5   | 1024          | 32                | 5                         | 4.17                      |  |
| 6   | 2048          | 36                | 10                        | 8.33                      |  |
| 7   | 4096          | 40                | 30                        | 25                        |  |
| 8   | 8192          | 44                | 50                        | 41.67                     |  |
| 9   | 16384         | 48                | 90                        | 75                        |  |

#### ii. Receiver (measuring block)

Measuring block consists of: a) devices of protection from a high input voltage **HVP**, b) multichannel strobe system, integration and storage of the analog information - **DAS**, c) the multiplexer of channels - **MX**, and d) the Analog-to-Digital Converter (**Fig. 3.5**). Some further description of the DAS is following.

The signal after passage of the protection device HVP gets in DAS. As it was mentioned above, this device is intended for stacking of a measured signal, integration of a signal in readouts (strobes) for suppression of noise and compressing of a dynamic range, and finally storing and stacking of the analog information.

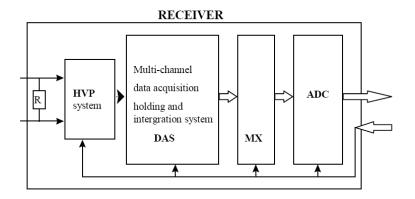


Fig. 3.5: Block diagram of the receiver of TEM Fast 48 (TEM-Fast 48 manual, 2007)

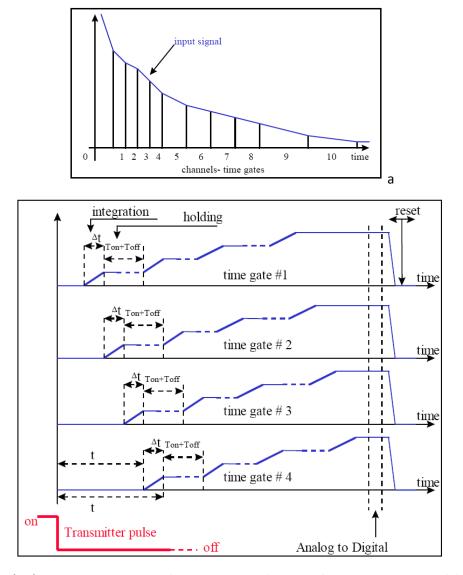


Fig 3.6: a), b) The main principles of DAS operation (see text for more explanation) (TEM-Fast 48 manual, 2007)

**Figures 3.6a** & **3.6b** show schematically measured transient  $\mathbf{E}(\mathbf{t})$  and arrangement of strobes in limits of which further integration is made. The moment "0" on an axis of time corresponds to the moment of turning off the current's pulse (**Fig. 3.4a**).

The algorithm of **DAS** works depend on time for first four strobes is shown in **Figure 3.7**. The intervals of time **t finish** - **t start** determine location of a strobe on time axes,  $\Delta t$  is the gate's width and time of integration, **Ton+Toff** is time of keeping determined by the period of recurrence of the generator's pulses. The parameters of strobe pulses of TEM-FAST 48 are given in **Table 3.2**.

Table 3.2: Parameters of strobe pulses of TEM-Fast 48 (TEM-Fast 48 manual, 2007)

| #Time | <b>t</b> start | <b>t</b> finish | T center | Δt | # Time | <b>t</b> start | <b>t</b> finish | <b>t</b> center | Δt   |
|-------|----------------|-----------------|----------|----|--------|----------------|-----------------|-----------------|------|
| Gates | μs             | иs              | μS       | μS | Gates  | μ <b>s</b>     | μs              | μs              | μs   |
| 1     | 3.6            | 4.6             | 4.06     | 1  | 25     | 255.6          | 319.6           | 285             | 64   |
| 2     | 4.6            | 5.6             | 5.07     | 1  | 26     | 319.6          | 383.6           | 350             | 64   |
| 3     | 5.6            | 6.6             | 6.07     | 1  | 27     | 383.6          | 447.6           | 414             | 64   |
| 4     | 6.6            | 7.6             | 7.08     | 1  | 28     | 447.6          | 511.6           | 478             | 64   |
| 5     | 7.6            | 9.6             | 8.52     | 2  | 29     | 511.6          | 639.6           | 570             | 128  |
| 6     | 9.6            | 11.6            | 10.53    | 2  | 30     | 639.6          | 767.6           | 699             | 128  |
| 7     | 11.6           | 13.6            | 12.55    | 2  | 31     | 767.6          | 895.6           | 828             | 128  |
| 8     | 13.6           | 15.6            | 14.56    | 2  | 32     | 895.6          | 1023.6          | 956             | 128  |
| 9     | 15.6           | 19.6            | 17.44    | 4  | 33     | 1023.6         | 1279.6          | 1152            | 256  |
| 10    | 19.6           | 23.6            | 21.46    | 4  | 34     | 1279.6         | 1535.6          | 1408            | 256  |
| 11    | 23.6           | 27.6            | 25.49    | 4  | 35     | 1535.6         | 1791.6          | 1664            | 256  |
| 12    | 27.6           | 31.6            | 29.50    | 4  | 36     | 1791.6         | 2047.6          | 1920            | 256  |
| 13    | 31.6           | 39.6            | 35.28    | 8  | 37     | 2047.6         | 2559.6          | 2304            | 512  |
| 14    | 39.6           | 47.6            | 43.30    | 8  | 38     | 2559.6         | 3071.6          | 2816            | 512  |
| 15    | 47.6           | 55.6            | 51.40    | 8  | 39     | 3071.6         | 3583.6          | 3328            | 512  |
| 16    | 55.6           | 63.6            | 59.41    | 8  | 40     | 3583.6         | 4095.6          | 3840            | 512  |
| 17    | 63.6           | 79.6            | 71.60    | 16 | 41     | 4095.6         | 5119.6          | 4608            | 1024 |
| 18    | 79.6           | 95.6            | 87.60    | 16 | 42     | 5119.6         | 6143.6          | 5632            | 1024 |
| 19    | 95.6           | 111.6           | 103.6    | 16 | 43     | 6143.6         | 7167.6          | 6656            | 1024 |
| 20    | 111.6          | 127.6           | 119.6    | 16 | 44     | 7167.6         | 8191.6          | 7680            | 1024 |
| 21    | 127.6          | 159.6           | 143.6    | 32 | 45     | 8191.6         | 10239.6         | 9216            | 2048 |
| 22    | 159.6          | 191.6           | 175.6    | 32 | 46     | 10239.6        | 12287.6         | 11264           | 2048 |
| 23    | 191.6          | 223.6           | 207.6    | 32 | 47     | 12287.6        | 14335.6         | 13312           | 2048 |
| 24    | 223.6          | 255.6           | 239.6    | 32 | 48     | 14335.6        | 16383.6         | 15360           | 2048 |

#### iii. The control block (controller)

The controller is executed on the basis of a Programmable Logic Device and is intended to control of all process of measurements and transfer of the information to the computer.

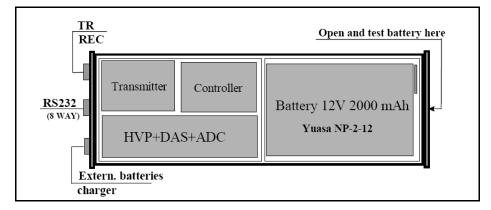
#### iv. Power supply

In TEM-FAST 48 the opportunity to use several power batteries is stipulated:

- Standard internal battery, 12V 2000 mAh
- External battery 12V for supply of the receiver and generator
- External battery 24V only for supply of the generator

#### v. The case and connectors of the device

All blocks of the device, including the internal battery, are assembled in the uniform duralumin case (Fig. 3.7).



**Fig. 3.7:** The arrangement of blocks of the device in the case (TEM-Fast 48 manual, 2007)

#### 3.2.1.3.2 More details in TEM Theory (based on Fast TEM technology)

A long description of physical and mathematical bases of TEM theory in general can be found in literature (e.g. Spies and Frischknecht, 1991), (Nabighian & Macnae, 1991)), and Kamenetsky, 1997) and it is not the scope of this section. A picture of the TEM theory which is based on Fast TEM technology, as it is referred at TEM-Fast 48 manual (2007) and Barsukov

et al (2007), is given next in this section, followed by representation about the instrumentation and its components.



**Fig. 3.8:** TEM instrumentation and peripheral units: a) palmtop PC, b) external power supply (12V+12V in series =24V), c) TEM Fast 48 system

A common practice in electric prospecting is to use, as the interpretation parameter, an apparent resistivity  $\rho_{\alpha}(t)$  of a homogeneous medium, the response of which at a given moment coincides with the signal measured in experiment. Traditionally,  $\rho_{\alpha}(t)$  is calculated by asymptotic formula for late times in near zone of transient field when the condition

$$t = \frac{t}{(\mu_0 R^2 / \rho)} >> 1$$
 is satisfied:

$$\rho_{\alpha}(t) = \left[ \frac{\sqrt{\pi}}{20} \frac{\mu^{5/2} R^4}{t^{5/2} E(t)/I} \right]^{2/3}$$

where  $\mu_0$  is the magnetic permeability of vacuum,  $\rho$  is the resistivity of the homogeneous half-space, E(t)/I is the measured value of normalized voltage at antenna terminals, and  $R=L/\pi^{1/2}$  the effective radius of a single-turn square antenna with a side L.

**Table 3.3:** Technical specifications of TEM Fast 48 (TEM-Fast 48 manual, 2007).

| The transmitter  |
|--|
| Time of turning off the current's pulse (TR=REC, I=1 A) (µs)                     |
| TR=25m   |
| TR=50m   |
|  |
|  |
| - The amplitude of current's pulses (A) is (selective)                           |
| - Ratio pulse/pause (time range = 1-6)   |
| - Active resistance of load (Ohm)  |
| - Inductance of a load (I=1A) (H)  |
| The receiver   |
| - Frequency band (MHz) > 4   |
| - Allowable constant voltage at input (mV)2 + 5                                  |
| - Number of automatically registered delays                                      |
| - Suppression of industrial noise 50/60 Hz (dB) > 60                             |
| - Internal noise ( RMS- root mean square, μV)                                    |
| (Stack = 20, TR=REC, I=1A, resistance at input $r = 2-8$ Ohm) 1                  |
| - Dynamic range (max /min) ( $\mu$ V)  |
| - Systematic errors (%)  |
| - Measured parameters:   |
| E.M.F./CURRENT V/A   |
| Errors of measurements   |
| - Allowable types of measuring antenna's configurations:                         |
| One-loop with the sizes of antennas (m) $0.01\times0.01$ up to $400\times400$    |
| "loop-in-loop" - size of a TR-loop (m)   |
| size of a REC-loop   |
| Optimum configuration - one loop by the size (m) $18 \times 18 - 100 \times 100$ |
| Time of measurements (Stack = 1) min/max (sec)                                   |
| Power consumption  |
| - Standard internal battery  |
| - Maximum number of soundings with standard battery:                             |
| (I = 1A, Stack = 10)   |
| - Consumption in a mode - "sleep" (µA)   |
| - Constitution in a mode - Steep ( $\mu$ A)                                      |
| Other characteristics  |
| Operation with IBM - compatible PC with standard port RS 232,                    |
| DOS or Windows 95/98 or Palmtop PC with OS Windows CE                            |
| Weight (kg)  |
|  |
|  |
| Operating temperature range -20° - + 65° C                                       |
| Change of temperature (°C / minute)  |
| Power of protection of the case of the device IP15 (65)                          |

Next follows some practical solutions and recommendations about TEM theory and practice from Dr. Pavel Barsukov et al (2007), as they referred at TEM-Fast 48 manual:

- "The increase of the size of antenna in TEM method results the increase of a level of registered signals. At late stages the ratio signal-to-noise is proportional to the area of the transmitting antenna (TR<sup>2</sup>)".
- "Maximal depth of researches is determined by the maximal time t, on which it is possible reliably to register a signal E(t)/I".
- "Maximal depth of researches with configuration loop-in-loop theoretically is identical to the coincident configuration".
- "Stratification of section with high levels of resistivity is extremely complicated. It is practically impossible to distinguish layers with  $\rho=1000$  and  $\rho=10000$  ohm.m. At these levels of resistivity it is necessary to use antennas of the large sizes (for  $\rho>1000$  ohm.m TR = 100m and more)".
- "The most favourable range of specific resistivity for stratification of rock lays within the limits of  $10 \text{ ohm.m} < \rho < 300 \text{ ohm.m}$ ".
- "Optimum range of the sizes of transmitting-receiving antennas for TEM-FAST 48 is TR=REC=18×18 - 100×100 m".
- "At a choice of the optimum size of antennas it is necessary to remember that large size antennas increase limiting depth of researches. However, estimations of a range of depths  $\mathbf{h}$ , for which reliable interpretation of the received results is possible, at use of coincide antennas with the side  $\mathbf{TR} = \mathbf{REC} = \mathbf{L}$  usually lay in limits:  $\mathbf{h}_{min} > \mathbf{L}/10$  and  $\mathbf{h}_{max} < 3\mathbf{L}$ ".

#### 3.2.1.3.3 Side Effects in TEM sounding

During TEM data acquisition with TEM-Fast instrumentation, three physical phenomena take place that cause difficulties to the process of field diffusion and may affect significantly the effectiveness of geological interpretation of the measured results. These are: SuperParaMagnetic (SPM) effect and Induced Polarization (IP) effect (Barsukov, 2007). Apart from those, man-made noise can distort a TEM sounding too.

i) When TEM measurements are acquired on SPM rocks (SPM material – superficial clay above parent rocks, glacier, etc), anomalous transient recordings are taken, leading to invalid apparent resistivity determinations with time.

- ii) The IP effect has as a result to increase the voltage on a TEM decay curve at early times and to decrease it at late times (in extreme cases becoming negative). This effect is minimal in the coincident antennas. Generally reduction of IP effect can be achieved by increasing the size of the antenna or by rising the antenna above ground surface (TEM-Fast 48 manual, 2007).
- iii) Man-made (known also as cultural noise) arises from the presence of pipelines, power and telephone lines, metal fences, etc. Currents induced in such metallic conductors, cause distortions in the TEM data. It is not possible to carry out TEM measurements in areas with high power-line noise, even though instrumentation has internal notch filters for reducing the effect.

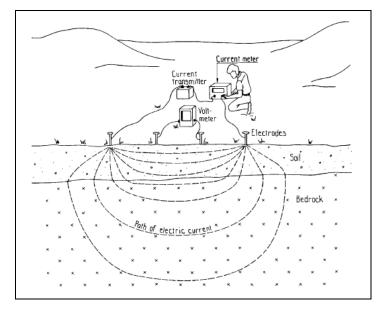
#### 3.2.2 Resistivity Method - VES technique

The resistivity method has a longer history than EM methods and it has a wide range of applications to environmental and engineering problems. The technique of resistivity surveying has its origin in 1912 and it was developed by Conrad Schlumberger, who conducted the first experiments in Normandy. This section describes in brief the theoretical principles of the resistivity method, and deals in greater detail with the Vertical Electrical Sounding (VES) field technique and Schlumberger electrode configuration.

#### 3.2.2.1 Basic principles

The underlying principle of geoelectrical methods is: "Electrical measurements of various types are made at the surface of the earth to investigate subsurface conditions in an area. An electric current is driven through the ground and the resulting potential differences are measured at the surface. Anomalous conditions or inhomogeneities within the ground, such

as electrically better or poorer conducting layers, are inferred from the fact that they deflect the current and distort the normal potentials" (Sharma, 1997).



**Fig. 3.9:** Sketch showing principle of DC resistivity measurement (Dahlin, 2001; modified from Robinson and Coruh, 1988).

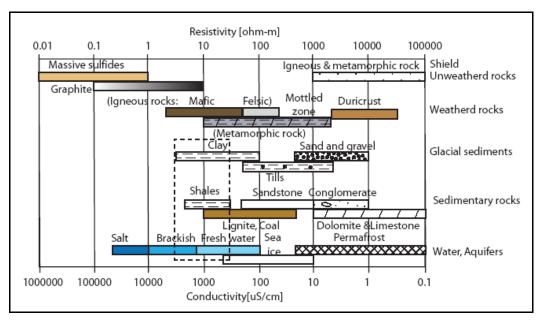
The property of the electrical resistance (R) of a material is expressed in terms of its resistivity ( $\rho$ ) [ $\Omega$  m or ohm.m]. Resistivity is a bulk property of a material and describes how well that material inhibits current flow and should not be confused with the term resistance. The inverse of resistivity is called conductivity,  $\sigma$  (=1/ $\rho$ ) [S/m]. The purpose of Vertical Electrical Soundings (VES) is to determine the variations in resistivity with depth. **Figure 3.10** shows the approximate resistivity ranges of earth materials.

For a homogeneous ground the resistivity  $\rho$  is calculated by:

$$\rho = K \cdot \frac{\Delta V}{I} \qquad (3.5)$$

where  $\Delta V$  the potential difference, I the flowing current, and K denotes the geometric factor of the electrodes configuration and calculated by:

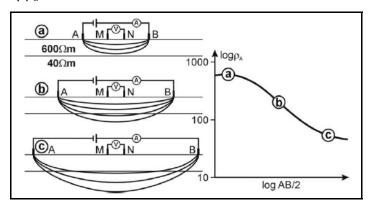
$$K = \frac{1}{2\pi} \left( \frac{1}{AM} - \frac{1}{BM} - \frac{1}{AN} + \frac{1}{BN} \right)$$
 (3.6)



**Fig . 3.10:** Typical ranges of electrical resistivities of earth materials (Perttu, 2008; after Palacky 1987)

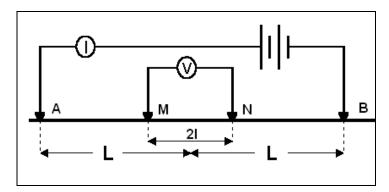
#### 3.2.2.2 Vertical Electrical Soundings

Resistivity measurements are carried out current electrodes (A and B) and then measure the resultant potential difference ( $\Delta V$ ) between two potential electrodes (M and N) (**Figs. 3.11** & **3.12**). As described by Kirsch (2006): "The basic idea of resolving the vertical resistivity layering is to stepwise increase the current-injection electrodes AB spacing (usually with a logarithmic electrode separation distribution), which leads to an increasing penetration of the current lines and in this way to an increasing influence of the deep-seated layers on the apparent resistivity  $\rho_{\alpha}$ "



**Fig. 3.11:** apparent resistivity measurements with increased current electrode spacing leading to increased penetration depths of the injected current (Kirsch, 2006)

Different types of electrode configurations are used, depending on the type of investigation, field condition and the sensitivity of the resistivity meter. Because of practical and methodical advantages, VES mostly use the symmetrical Schlumberger configuration. Sounding with that array is carried out by keeping the electrode array centred over the field site while increasing the distance between current electrodes, thus increasing the depth of investigation. Work in this thesis has been carried out using a Schlumberger electrode configuration.



**Fig. 3.12:** Outline of a Schlumberger array for Vertical Electrical Soundings (VES). A, B for current electrodes, and M, N for potential electrodes.

**Equation 3.5** is only true for a homogeneous earth. For an inhomogeneous earth the resistivity as computed will vary, and, therefore, the resistivity obtained is designated as 'apparent resistivity',  $\rho_{\alpha}$ .

In Schlumberger array (**Fig. 3.12**), the simplified formula for apparent resistivity (Sharma, 1997) is:

$$\rho_{\alpha} = \frac{\pi L^2}{I} \frac{\Delta V}{2l}$$

#### 3.2.2.3 Instrumentation for DC measurements

In our fieldwork, resistivity data were acquired with a SYSCAL R1 PLUS Switch-48 from IRIS. It is an all-in-one multinode resistivity imaging system that it features an internal switching

board for 48 electrodes and a voltage up to 600V. Automatic ranging is also available, where the output current is automatically adjusted in order to optimize the input voltage values and therefore, certify the best measurement quality. It is ideal for environmental and especially for hydrogeologic applications such as salinity control and shallow groundwater exploration (depth and thickness of aquifers) (IRIS instruments, 2009).

#### 3.3 Geochemical Analyses

The analytical chemistry of groundwater in general is beyond the scope of this section. In most cases water analyses were carried out by standard procedures as described mainly in "Standard Methods for the examination of water and wastewater" (2005) handbook, and in some other reference sources, as mentioned in the text. In the first part of this chapter some information about the sample collection, preservation and storage is given. Then the physical and aggregate properties, the metals and the inorganic nonmetallic constituents, that have been analyzed within the frames of this thesis, are summarized, and some short descriptions of each method of each chemical parameter is given (**Table 3.4**).

#### 3.3.1 Collection & Preservation of Samples

Correct sampling and preservation are critical for accurate results. Substantial errors involving the faulty identification and classification of materials on sites may be induced by the usage of inappropriate sampling techniques or procedures (Ostler & Holley, 1997).

#### 3.3.1.1 Collection of Samples

The purpose of water sampling is to collect a portion of material large enough to be representative and small enough in volume to be transported easily, i.e. essentially similar in chemical and physical properties with the total body of the material under investigation.

For each sample location 500 mL of water was collected, amount enough for the analysis of all the chemical parameters.

Very important issue is to ensure that all sampling equipment is clean and quality-assured before use. For all the samplings of this thesis, the sample containers that were used were clean and free of contaminants as they were first washed thoroughly and then swilled many times with distilled water. Finally, the containers were rinsed several times with the water to be sampled before taking the sample.

A very detailed and exact sample-tracking data base was kept during the whole period of this study in order to avoid errors or mistakes coming from sample mixing and/or sample misidentification. Each sample collected was recorded and identified with a unique sample number and date, marked on each bottle using waterproof ink. Other sufficient information, including the unique sample identification number, the date, exact location, water temperature, etc. were recorded in a sample book in the field at the sampling site at the time of sample collection in order to provide positive sample identification at a later date.

For fixing the sampling points, Global Positioning Systems (GPS) were used, as they supply accurate sampling position data. After the sampling points were chosen, they were all marked by GPS, so it was finally easy for the sampler/ author to find each time the sample location guided by the GPS.

A general rule for water sampling from wells is to collect samples only after the water has run long enough to draw fresh groundwater into the system and the samples should be collected from a tap near the well. Purging stagnant water is critical, that's why the well was pumping for about 10 minutes at least before water sample collection (2 times the well volume was emptied approximately). For the 2 springs, the samples there were taken very close to the place where the water flowed, in order to have a representative sample from each spring for analysis. The samples were taken under the surface water and the caps were submerged before removing.

#### 3.3.1.2 Sample Storage and Preservation

The type of sample container used is of extreme importance as well. Glass sample containers are generally avoided (due to their fragile nature), but sometimes are the only solution because some sample analytes may dissolve (be absorbed) into the walls of plastic containers; and, similarly, contaminants from plastic containers may leach into samples. For this thesis, all the samples were stored in high-density Polyethylene (HDPE) bottles of 500 mL with watertight lids.

In general, it is known that the reliability of the analytical results depends on the time that elapses between collection of a sample and its analysis. For certain physical values (e.g. temperature) and constituents, instant analysis in the field is required. In order to avoid changes in the chemical composition of the samples between sampling and analyses, they were kept refrigerated ( $\approx$ 4°C). Of course, some chemical parameters that should be measured immediately (pH-Value, Electrical Conductivity, Alkalinity, Cl̄,  $NO_3^-$ ), their determination were started without delay after the arrival in the laboratory. The analyses of the samples were completed as soon as possible (within 2-3 days after collection). In some cases and in order to test the repeatability of the methods, and the procedures used in the study, a few samples were kept for longer time in the refrigerator, after acidification with conc.  $HNO_3$ .

#### 3.3.2 Physical and Aggregate Properties

This section comprises five physical and aggregate properties: Alkalinity (and  $HCO_3^-$  concentration), Total Hardness, Electrical Conductivity (and TDS), Salinity, and Temperature. These parameters were measured or calculated for the three samplings (except Alkalinity which was determined only for the October's 2008 sampling).

**Table 3.4:** All the measured chemical parameters and their methodologies used in the present study

| Chen                                     | nical Parameter         | Methodology                                      |  |  |
|--|-------------------------|--|--|--|
|  | Alkalinity              | Titration Method                                 |  |  |
| 51                                       | Hardness                | E.D.T.A. Titrimetric Method                      |  |  |
| Physical and<br>Aggregate                | Electrical Conductivity | Conductivity Cell                                |  |  |
| Properties                               | Salinity                | Electrical Conductivity Method                   |  |  |
|  | Temperature             | Digital Thermometer (in situ)                    |  |  |
| Metals                                   | Calcium                 |  |  |  |
|  | Magnesium               |  |  |  |
|  | Potassium               | Flame Atomic Absorption                          |  |  |
|  | Sodium                  |  |  |  |
|  | Iron                    |  |  |  |
|  | Boron                   | Azomethine-Hydrogen Method                       |  |  |
|  | Chloride                | Argentometric Method                             |  |  |
| Inorganic<br>Nonmetallic<br>Constituents | pH value                | pH Electrode                                     |  |  |
|  | Nitrate nitrogen        | Ultraviolent Spectrophotometric Screening Method |  |  |
|  | Sulfate                 | semi-quantitative Method<br>(Aquaquant 1.14411)  |  |  |
|  | Phosphate               | Spectrophotometric Method                        |  |  |

# 3.3.2.1 Alkalinity (expressed as mg $CaCO_3/L$ ) and Bicarbonate concentration (as mg $HCO_3^-/L$ )

"The alkalinity of water represents a measurement of the water's capacity to neutralize an acid and as such is related to the water's buffering capacity, i.e. its capacity to resist a change

in pH as acid is added", AWWA Staff, 1995. The measured value may vary significantly with the end-point pH used (Standard Methods for examinations of water and wastewater, 2005).

"Alkalinity has a little identified significance for human health. Nevertheless, highly alkaline water has a horrible taste ("soda" taste) and may force consumers to look for other water sources", AWWA Staff, 1995. "In addition, as the alkalinity of many surface waters is primarily a function of carbonate, bicarbonate, and hydroxide content, it is taken as an indication of the concentration of these constituents. The measured values also may include contributions from borates, phosphates, silicates, or other bases if these are present ", Standard Methods for examinations of water and wastewater, 2005.

There is no regulation about alkalinity from WHO or European Council, but the EPA (U.S. Environmental Protection Agency) Secondary Drinking Water Regulations limit alkalinity only in terms of TDS (500 ppm) and by the limitation on pH (EPA, 2009).

The method that was chosen for determining alkalinity is the **Titration Method** (2320 B, Standard Methods for examinations of water and wastewater, 2005).

**Reagents** a) Sodium carbonate solution, approximately 0.05N (1.25 g  $Na_2CO_3$  were added (after drying at  $250^{\circ}$  for 4 h), and diluted to 500 mL with distilled water in a volumetric flask), b) Standard hydrochloric acid, 0.1 N (not precise value).

 $40~\text{mL}~0.05~\text{N}~\text{Na}_2\text{CO}_3$  solution and 60~mL water were added in a beaker, and the pH value equaled to 10.9. Then this solution was standardized against by titrating potentiometrically to pH of about 3. However, the volume of HCl solution used for titrating the  $\text{Na}_2\text{CO}_3$  solution to pH 4.5 was used to the calculations presented below.

The reactions which take place during the titration are:

$$Na_2CO_3 + H^+ + Cl^- \rightarrow 2Na^+ + Cl^- + HCO_3^-$$
 (1)

$$HCO_3^- + H^+ \rightarrow H_2CO_3$$
 (2)

So, the normality of the HCl was calculated as following:

Normality, 
$$N = \frac{A \times B}{53 \times C} = \frac{2.5 \times 40}{53 \times 17.55} = 0.107$$

where:

 $A=g\ Na_2CO_3$  weighted into  $1L\ flask$ 

B=mL Na<sub>2</sub>CO<sub>3</sub> solution taken for titration,

C= mL acid used

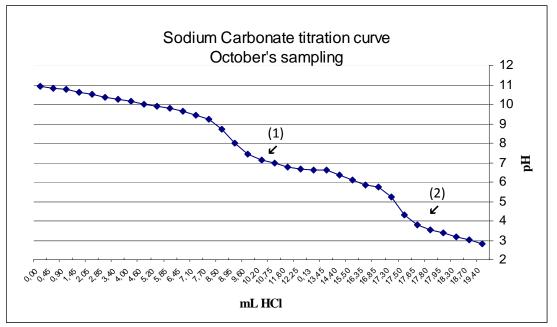


Fig. 3.13: Sodium carbonate titration curve for October's sampling for the HCl normality calculation. The equivalent points (1) and (2) correspond to the end of the reactions 1 and 2 respectively.

**Procedure** Potentiometric titration curves were constructed for each sample to end-point pH value of 4.5 according to the reference method 2320 B (Standard Methods for examinations of water and wastewater, 2005). The samples were not filtered, diluted, concentrated or altered.

**Calculation** Potentiometric titration to end-point pH:

Alkalinity (mg 
$$CaCO_3/L$$
) =  $\frac{A \times N \times 50000}{mL \ sample}$ 

where:

A=mL standard acid used

N=normality of standard acid (estimated as described above)

It is necessary to convert bicarbonate ion concentration (expressed as mg  $CaCO_3/L$ ) to bicarbonate ion activity (in mg  $HCO_3^-/L$ ), because it is needed for Piper, Durov, Stiff diagram etc. plotting. There is a practical method to do this: If the pH is less than about 8.4, to do that conversion, we just multiple the alkalinity (in mg  $CaCO_3/L$ ) by 1.22 to convert to bicarbonate  $[HCO_3^-]$  ions concentration (in mg  $HCO_3^-/L$ ). The titration curve in **Figure 3.13** also indicates that samples with pH values below 8 contain no  $CO_3^{2-}$  ions. As it can been seen in **Appendix C** all our samples fulfill this condition (all pH values below 8). Thus, for the conversion of the total alkalinity expression to bicarbonate concentration the utilization of the 1.22 factor is valid. That state is true in most cases as  $HCO_3^-$  is truly most dominant component of alkalinity in natural water (Coal Geology, 2009).

#### **3.3.2.2** Hardness (expressed as mg CaCO<sub>3</sub>/L)

Water hardness is considered to be a measure of the capacity of water to precipitate soap. Soap is precipitated mainly by the calcium and magnesium ions present. Therefore, hardness is a measure of Ca<sup>2+</sup> and Mg<sup>2+</sup> salts in water, which are present mainly as bicarbonate salts. Hard waters usually occur where topsoil is thick and limestone formations are present, whereas, soft waters occur where the topsoil is thin and limestone formations are sparse or absent (AWWA Staff, 1995). According to current practice, total hardness is defined as the sum of the calcium and magnesium concentrations, both expressed as calcium carbonate, in milligrams per liter (mg CaCO<sub>3</sub>/L) (Fresenius et al., 1988).

There is no regulation about hardness from WHO, but a taste threshold is suggested for the calcium ion in the range of 100-300~mg/L, depending on the associated anion, and a taste threshold for magnesium in a lower range than that for calcium. In some instances, consumers tolerate water hardness in excess of 500~mg/L (WHO, 2004).

The method that was chosen for determining hardness is **EDTA Titrimetric Method (2340C,** Standard Methods for examinations of water and wastewater, 2005).

**Reagents** a) Standard EDTA titrant: EDTA solution 0.01 M (3.723 g EDTA- $Na_2$  salt was added and diluted to 1~L with distilled water), b) Indicator: Eriochrome Black T. The indicator was included in the buffer tablet (see next), c) <u>Buffer system</u>: Tablets, containing  $NH_4Cl$  and the indicator, (Merck, 1-08430-1000), were used along with 1~mL of  $NH_3$  25% (w/v) to buffer the sample at pH  $10.0 \pm 0.1$ .

**Procedure** 25mL of sample were diluted to 50mL with distilled water in an erlenmeyer flask. 1mL buffer solution was added and then the indicator. standard EDTA titrant was added slowly with continuous stirring, until the last reddish tinge disappeared. At the end point the solution was blue. The procedure was repeated one more time and the average value was recorded.

Calculation Hardness (EDTA) as mg 
$$CaCO_3/L = \frac{A \times B \times 1000}{mL \ samle}$$

where: A = mL titrant for sample, and

 $B = mg \ CaCO_3$  equivalent to 1.00 mL EDTA titrant

#### 3.3.2.3 Electrical Conductivity ( $\mu$ S/cm) and TDS (mg/L)

Electrical Conductivity (EC) of water is based on the presence of ions. It can be regarded as a non-specific gauge for the content or the concentration of dissolved dissociable substances in water (Fresenius, 1988). Hence, it can be considered as a measure of the ionic strength of a solution and an indirect measure of the Total Dissolved Solids (TDS) in a water supply (AWWA Staff, 1995). An approved method for determining conductivity utilizes a self contained conductivity instrument with conductivity cells containing either platinum or non-platinum electrodes. The reference temperature or any conversion to a different temperature from the measuring temperature should always be indicated, as the results measured are dependent on temperature, since the movement of ions under an electrostatic potential increases with increasing temperature. EC is normally expressed in units of  $\mu$ S/cm and the reported values have already been normalized automatically to 20°C by the conductivity meter.

For groundwater, EC values greater than  $500~\mu\mathrm{S/cm}$  indicate that the water may be polluted, although values as high as  $2000~\mu\mathrm{S/cm}$  may be acceptable for irrigation water. In Europe, the EC of drinking water should be no more than  $2500~\mu\mathrm{S/cm}$  @  $20^{\circ}\mathrm{C}$  (European Council, 1998).

**Apparatus** The conductivity meter used was Consort, model C532.

**Procedure** The instrument was calibrated with fresh standards, at room temperature, at the beginning of the measurements. When the calibration was finished, the cell was rinsed several times with the sample and it was immersed in that solution. Low stirring was used. The conductivity in  $\mu S$  was displayed. Then, we rinsed again with distilled water and continued to the next sample. The same procedure was repeated for all the samples.

#### **EC to TDS Conversion**:

A rough approximation for EC to TDS conversion is commonly used:

TDS (ppm)  $\approx$  EC \* 0.65 (Mandel & Shiftan)

A second method was used (only for October's sampling) for TDS determination using the sum of the concentrations of the dominant elements present in each sample (anions:  $HCO_3^-$ ,  $Cl^-$ ,  $SO_4^{2-}$ , and cations:  $K^+$ ,  $Na^+$ ,  $Ca^{2+}$ ,  $Mg^{2+}$ ). The two different methods gave similar results for the TDS value (data from the second method not shown in next chapter).

No health-based guideline value for TDS was proposed in the 1993 Guidelines, as reliable data on possible health effects associated with the ingestion of TDS in drinking water were not available. However, the presence of high levels of TDS in drinking-water (greater than 1200 mg/L) may be objectionable to consumers. Water with extremely low concentrations of TDS may also be unacceptable because of its flat, insipid taste (WHO, 2004). Secondary maximum contaminant level is set to a lower value of 500 mg/L by EPA (EPA, 2009).

#### 3.3.2.4 Salinity (ppt)

"Salinity was originally conceived as a measure of the mass of dissolved salts in a given mass of solution. The experimental determination of the salt content by drying and weighing presents some difficulties due to the loss of some components. The only reliable way to determine the true or absolute salinity of natural water is to make a complete chemical analysis. However, this method is time-consuming and cannot yield the precision necessary for accurate work. Thus, to determine salinity, one normally uses indirect methods involving the measurement of a physical property such as electrical conductivity, density, sound speed, or refractive index", Standard Methods for examinations of water and wastewater, 2005.

When we measure the salinity of water, we estimate the amount of the dissolved salt in the water, or the concentration of salt in the water. Concentration can be expressed in parts per million (ppm) or parts per thousand (ppt), where  $1 \text{ ppm} = 10^{-3} \text{ ppt} = 1 \text{mg/L}$  (Windows to the Universe, 2009). There are no guidelines/recommendations for salinity from WHO, EU or EPA. The classes of the salinity of water are displayed on **Table 3.5**.

**Table 3.5**: Classifications of the Salinity of waters

| drinking water                | 0.1ppt      |
|-------------------------------|-------------|
| restriction on drinking water | 0.5ppt      |
| limit drinking water          | 1ppt        |
| limit agriculture irrigation  | 2ppt        |
| brackish water                | 0.5 - 30ppt |
| sea water                     | 30 - 50ppt  |
| Brine                         | >50ppt      |

The method that was chosen for determining salinity is **Electrical Conductivity Method** (2520B, Standard Methods for examinations of water and wastewater, 2005).

**Apparatus** See Electrical Conductivity, section 3.3.2.3.

**Reagent** KCl solution (we added a mass of 3.243g KCl in a mass of 100g of solution).

**Determination** For seawater measurements the Practical Salinity Scale 1978 was used. This scale was developed relatively to a KCl solution (see Reagent above). A seawater with a conductivity, C, at 15°C equal to that of the above indicated KCl solution is defined as having a practical salinity of 35. The conductivity of the KCl solution was measured, that was 59.3 at 24.5°C. The conductivity values of each sample already been measured at 24.5°C.

The conductivity ratio is defined as  $R_t = \frac{C \text{ (sample at t)}}{C \text{ (KCl solution at t)}}$  (valid from S=2 to 42), where t is temperature and C is conductivity.

The salinity dependence of the conductivity ratio,  $R_{\rm t}$ , as a function of temperature of a given sample to a standard S=35 seawater is used to determine the salinity ( $S_{\rm PSS}$ )

$$S = a_0 + a_1 R_t^{\frac{1}{2}} + a_2 R_t + a_3 R_t^{\frac{3}{2}} + a_4 R_t^2 + a_5 R_t^{\frac{5}{2}} + \Delta S$$

where  $\Delta S$  is given by

$$\Delta S = \left[ \frac{t - 15}{1 + 0.0162(t - 15)} \right] \left( b_0 + b_1 R_t^{\frac{1}{2}} + b_2 R_t + b_3 R_t^{\frac{3}{2}} + b_4 R_t^2 + b_5 R_t^{\frac{5}{2}} \right)$$

and

$$a_0 = 0.0080$$
  $b_0 = 0.0005$   $a_1 = -0.1692$   $b_1 = -0.0056$   $a_2 = 25.3851$   $b_2 = -0.0066$   $a_3 = 14.0941$   $b_3 = -0.0375$   $a_4 = -7.0261$   $b_4 = 0.0636$   $a_5 = 2.7081$   $b_5 = -0.0144$ 

The salinity of our samples was low, so the equation that is valid from 0 to 40 salinity is:

$$S = S_{PSS} - \frac{a_0}{1 + 1.5X + X^2} - \frac{b_0 f(t)}{1 + Y^{1/2} + Y^{3/2}}$$

where  $S_{\it PSS}$  = value determined from the Practical Salinity Scale given earlier,

$$a_0 = 0.008$$

$$b_0 = 0.0005$$

$$X = 400R_t$$

$$Y = 100R_t$$
, and

$$f(t) = (t-15)/[1+0.0162(t-15)]$$

# **3.3.2.5** Temperature ( $^{\circ}$ C)

Temperature is measured on the Celsius (°C) or the Fahrenheit (°F) scale. Water temperature is a physical parameter with great significance. The rate at which chemicals dissolve and react is, in part, dependent on temperature. From all the parameters measured in this thesis, temperature is the only one that was measured in situ during samplings.

**Apparatus** Digital Thermometer from FRIO-Temp® with range -50 to  $300^{\circ}$ C (-58 to  $572^{\circ}$ F). Accuracy:  $\pm 0.5^{\circ}$  from -20 to  $70^{\circ}$ C.

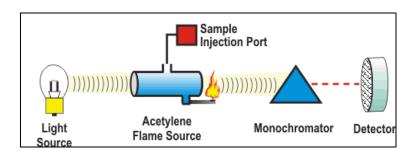
# 3.3.3 Metals (mg/L)

"Water contains trace amounts of metals, which are in general not harmful to human health. Actually, some metals (calcium, magnesium, potassium, and sodium) are essential to sustain life and for normal body functions. Metals in the water supply could occur naturally or may be the result of contamination. Naturally occurring metals are dissolved in water when it comes into contact with rock or soil material. Other sources of metal contamination are corrosion of pipes and leakage from waste disposal sites", Health Effects of Metals in Drinking Water, 2009.

For this thesis Ca (Calcium), Mg (Magnesium), K (Potassium), Na (Sodium), and Fe (Iron) were determined and the contaminant level of each metal is displayed in **Table 3.6** 

Flame Atomic Absorption Spectrometry (FAAS) is a very common technique for detecting metals and metalloids in water samples by using an acetylene-air flame. It is very reliable and easy to use. In summary, the technique is based on the fact that free metal atoms in ground state absorb light at specific wavelengths. Metal ions in a solution are converted to atoms which they spend a short amount of time in a flame. This area is targeted by a light-beam which consists of the emission spectrum of the specific metal under investigation. Since the atomic emission spectra include the lines of the corresponding absorption spectra, there is a certain probability atoms of the metal to absorb photons and to convert to an excited state. This absorption can be measured and quantified, and by means of a calibration curve, to be correlated with the concentration of the metal in the sample (Haswell, 1991; Meyers, 2001).

"The technique of Flame Atomic Absorption Spectroscopy (FAAS) requires a liquid sample to be aspirated, aerosolized, and mixed with combustible gases, such as acetylene and air or acetylene and nitrous oxide. The mixture is ignited in a flame whose temperature ranges from 2100 to 2800 C", Ma, G. & Wilson González, G. (2009). A flow diagram of FAAS instrumentation is shown in **Figure 3.14**.



**Fig. 3.14**: Operation principle of an atomic absorption spectrometer (ETS Labs, 2009).

**Instrumentation** All metal (Ca, Mg, K, Na, and Fe) concentrations were determined by Perkin Elmer, AA100 flame atomic absorption spectroscopy.

**Procedure** <u>Calibration and standard curves</u>: "As with other analytical techniques, FAAS requires careful calibration. Calibration through several steps is required, including

interference check sample, calibration verification, calibration standards, bland control, and linear dynamic range determination. The idealized calibration or standard curve is stated by Beer's law that the absorbance of an absorbing analyte is proportional to its concentration. FAAS tends to have calibration curves that have a limited linear dynamic range relative to the other atomic spectrometric techniques", Sevostianova, 2009.

In this study, the correlation coefficient (R value) of all the accepted and finally used calibration curves for all the metal determinations (Ca, Mg, K, Na, and Fe) was between 0.999 and 1 (high-quality correlation)!

#### 3.3.4 Inorganic Nonmetallic Constituents

This section comprises six inorganic nonmetallic parameters: **Boron**, **Chloride**, **pH value**, **Nitrate**, **Sulfate**, and **Phosphate**. These parameters were measured or calculated for the three samplings (except Boron and Nitrate which were determined only for the October's 2008 sampling, and Phosphate, which was determined only for July's 2008 sampling).

# **3.3.4.1 Boron** (B, mg/L)

"The average abundance of boron in groundwaters is 0.01 to 10 mg/L, and although it is an element essential for plant growth, in excess of 2 mg/L it can be harmful to certain plants. Drinking water rarely contains more than 1 mg B/L and normally the range tends to be below 0.01 to 0.1 mg/L. Higher values of boron concentration are generally due to the presence of wastewater (industrial, commercial or domestic origin)", Lenntech, 2009.

A health-based guideline value of  $0.3~\mathrm{mg/L}$  for boron was established in the 1993 Guidelines by WHO, which guideline value was increased to  $0.5~\mathrm{mg/L}$  in the addendum to the Guidelines published in 1998 (WHO, 2004). EU standard for boron is  $1~\mathrm{mg/L}$  (European Council, 1998).

The method that was chosen for determining B is **Azomethine-Hydrogen Method** (Sparks, 1996).

Apparatus UVmini-1240 UV-Visible Spectrophotometer from Shimadzu Corporation.

**Reagents** a) Azomethine-H solution (0.9 g azomethine-H were dissolved and 2 g of L-ascorbic acid were added in about 200 mL of lukewarm distilled water. It was cooled and then it was diluted to 250 mL), b) EDTA solution, 0.025 M (4.563 g of EDTA were dissolved in 200 mL of distilled water and the volume was adjusted with distilled water to 500 mL), c) buffer solution (250 g of ammonium acetate were dissolved in 500 mL distilled water and acetic acid was added (approximately 300 mL) to bringing the pH of the final solution to 4.8, d) Standard B solution (0.5174 g of B(OH)<sub>3</sub> were dissolved in distilled water and the volume of solution was adjusted to 1 L with distilled water. One milliliter of that solution contained 100 μg B. That solution was diluted 10-fold to have the 10 μg/mL standard B solution. That solution was used to prepare the calibration curve.

#### **Procedure**

- a) <u>Calibration curve standards</u>: 0, 0.2, 0.4, 0.8, and 1 mL of the  $10 \mu g \text{ mL}^{-1} \text{ B}$  stock solution were transferred to 5 -mL tubes and then appropriate volume of distilled water was added to bring the solution volume to 2 mL. 0.2 mL of EDTA solution and 0.4 mL of buffer solution were added and mixed well. Then 1 mL of azomethine-H solution was added and the volume was adjusted to 5 mL with distilled water. The contents of the tubes were mixed and were kept at room temperature for 2 h for colour development. The final B concentrations in these standard solutions were: 0, 0.4, 0.8, 1.6, and  $2 \mu g/\text{mL}$ , respectively.
- b) <u>Samples</u>: All samples were prepared exactly as described for standards, using  $3.4\ mL$  of each water sample.

The absorbance of the solutions (both standards & samples) was measured at a wavelength of  $420\ \mathrm{nm}$ .

# **3.3.4.2** Chloride (Cl<sup>-</sup>, mg/L)

"Chlorine, in the form of chloride ion,  $Cl^-$ , is one of the major inorganic elements in water and wastewater. Chlorides are salts resulting from the combination of the gas chlorine with a metal. Some common chlorides include sodium chloride (NaCl) and magnesium chloride (MgCl<sub>2</sub>). Chlorine alone as  $Cl_2$  is highly toxic and it is often used as a disinfectant. In combination with a metal, such as sodium, it becomes essential for life. Small amounts of chlorides are required for normal cell functions in plant and animal life. The salty taste produced by chloride concentrations is variable and depent on the chemical composition of water", Lenntech, 2009.

No health-based guideline value is proposed for chloride in drinking-water. However, chloride concentrations in excess of about  $250~\rm mg/L$  can give rise to detectable taste in water (WHO, 2004). The same contaminant level comes from EPA Secondary Drinking Water Regulations (secondary standard for  $Cl=250~\rm mg/L$ ) (EPA, 2009) and EU (European Council, 1998).

The method that was chosen for determining  $Cl^-$  is the **Argentometric Method** (4500-Cl B, Standard Methods for examinations of water and wastewater, 2005).

**Reagents** a) Potassium chromate indicator solution (2 g of  $K_2CrO_4$  were dissolved in distilled water and was diluted to 100 mL, 2% w/v), and b) standard silver nitrate titrant, 0.0141 M ( $0.598 \text{ g } AgNO_3$  were dissolved in distilled water and was diluted to 250 mL).

**Procedure** First  $AgNO_3$  titrant was standardized and reagent blank value was determined by the titrant method outlined below. Then, the samples were prepared. 2.5 mL sample were diluted to 25 mL with distilled water in a conical flask. Then, 1 mL of the indicator solution was added. We titrated with standard  $AgNO_3$  titrant slowly with continuous stirring to a pinkish yellow end point. The procedure was repeated one more time and kept the average value.

Calculation mg Cl<sup>-</sup> / L = 
$$\frac{(A-B) \times N \times 35450}{mL \text{ sample}}$$

where A = mL titration for sample,

B = mL titration for blank, and

 $N = \text{normality of } Ag(NO_3)_2$ 

# **3.3.4.3 pH** value (H<sup>+</sup>)

Some books usually include pH in the physical parameters section. The standard methods handbook's structure (Standard Methods for examinations of water and wastewater, 2005) was followed, where  $H^+$  considered as inorganic nonmetallic constituent. Water quality and pH are often mentioned in the same sentence. The pH is a very important factor, because certain chemical processes can only take place when water has a certain pH.

"At a given temperature, the intensity of the acidic or basic character of a solution is indicated by pH or hydrogen ion activity. pH is defined as  $-\log[H^+]$ ; it is the "intensity" factor of acidity. Pure water is very slightly ionized and at equilibrium the ion product is:

$$[H^+][OH^-] = K_w = 1.01 \times 10^{-14}$$
 at 25°C

and

$$[H^{+}] = [OH^{-}] = 1.005 \times 10^{-7}$$

where

 $\lceil H^+ \rceil$  = activity of hydrogen ions (moles/L)

 $[OH^-]$  = activity of hydroxyl ions (moles/L)

 $K_{_{\scriptscriptstyle W}}={\rm ion~product~of~water~"}$  (Standard Methods for examinations of water and wastewater, 2005)

No health-based guideline value was proposed for pH in the 1993 Guidelines. Although pH usually has no direct impact on consumers, it is one of the most important operational water quality parameters, the optimum pH required often being in the range 6.5-9.5 (WHO, 2004). The EPA (U.S. Environmental Protection Agency) Secondary Drinking Water Regulations limit to a range between 6.5-8.5 (EPA, 2009).

**Apparatus** pH meter used was Consort, model C532.

**Procedure** The instrument was calibrated with fresh standards, at room temperature, at the beginning of the measurements. When the calibration was finished, the electrode was rinsed several times with the sample and it was immersed in that solution. The pH value was displayed. Then, we rinsed again with distilled water and continued to the next sample. The same procedure was repeated for all the samples. Slow stirring was used for faster homogenization.

# **3.3.4.4 Nitrogen (**Nitrate nitrogen, NO: -N, mg/L)

"Measurement of UV absorption at  $220~\rm nm$  enables rapid determination of  $NO_3^-$ . Because dissolved organic matter also may absorb at  $220~\rm nm$ , but it does not absorb at  $275~\rm nm$ , a second measurement at  $275~\rm nm$  may be used to correct the values. The extent of this empirical correction is related to the nature and concentration of organic matter and may vary from one water sample to another", Standard Methods for examinations of water and wastewater, 2005.

The guideline value for nitrate is 50 mg/L (WHO, 2004). Because of the possibility of simultaneous occurrence of nitrite and nitrate in drinking-water, it was recommended in the 1993 and 1998 Guidelines that the sum of the ratios of the concentration of each to its guideline value should not exceed 1 (WHO, 2004). The same limit has been set by EU (European Council, 1998).

The method that was chosen for determining  $NO_3^-$ -N is **Ultraviolet Spectrophotometric Screening Method** (**4500**-  $NO_3^-$  **B,** Standard Methods for examinations of water and wastewater, 2005).

**Procedure** First the standard curve was prepared. Three  $NO_3^-$  calibration standards were prepared in the range of 0 to 7 mg  $NO_3^-$  – N/L (1, 3, 7 mg/L) and they were treated in the same manner as samples.  $KNO_3$ , dried at  $105^\circ$  for 2h, was used for the preparation of standard solutions. Absorbance at 220 nm and 275 nm was measured for all standards and samples.

**Calculation** For samples and standards, the absorbance reading at 275 nm was multiplied by two and the result was subtracted from the reading at 220 nm to obtain absorbance due only to  $NO_3^-$ . A standard curve was constructed by plotting absorbance due to  $NO_3^-$  against  $NO_3^- - N$  concentration of standard. Using corrected sample absorbances, sample concentrations were obtained directly from standard curve.

The correlation coefficient (R value) of the accepted and finally used calibration curve for nitrates concentration was 1 (high-quality correlation).

# **3.3.4.5** Sulfate ( $SO_4^{2-}$ )

"Sulfate is widely distributed in nature and may be present in natural waters in varying concentrations. Health concerns regarding sulfate in drinking water have been raised because of reports that diarrhea may be associated with the ingestion of water containing high levels of sulfate. Of particular concern are groups within the general population that may be at greater risk from the laxative effects of sulfate when they experience an abrupt

change from drinking water with low sulfate concentrations to drinking water with high sulfate concentrations", EPA, 2009.

No health-based guideline value for sulfate was proposed in the 1993 Guidelines. However, because of the gastrointestinal effects resulting from ingestion of drinking-water containing high sulfate levels, it was recommended that health authorities be notified of sources of drinking-water that contain sulfate concentrations in excess of  $500 \, \mathrm{mg/L}$  (WHO, 2004). EU is stricter, and the maximum level for sulfate concentration in water is  $250 \, \mathrm{mg/L}$  (European Council, 1998). The same maximum contamination level is given by EPA Secondary Drinking Water Regulations (EPA, 2009).

For the determination of the  $SO_4^{2^-}$  in water samples, a semi-quantitative method was used (visual colour kit Aquaquant® 1.14411 Sulfate, Merck). The method kit which was used was appropriate for  $SO_4^{2^-}$  determination in the range of 0-300 mg  $SO_4^{2^-}/L$ . This colourimetric method is based on the reaction of iodate with tannin in a weak acid medium resulting in a reddish-brown colour. It is not an exact method, but the ranges that are determined for  $SO_4^{2^-}$  are quite reliable.

# **3.3.4.6** Phosphate ( $PO_4^{3-}$ )

"Phosphorus is one of the major elements required for growth of plants and animals. There are phosphates in natural waters at concentrations which do not cause any health issues to humans. However, high concentration of Phosphorus in waters (mainly from agricultural fertilisers or wastewaters) can promote excessive algae or plant growth", Drinking Water Testing, Water Quality and Pathogenic Disease Laboratories, Wilkes University, 2009.

No phosphate guideline proposed by WHO, EU or EPA.

Phosphate determination was carried out spectrophotometrically using a modification of the method of Murphy and Riley (Murphy & Riley, 1962). Water samples were acidified with

 $H_2SO_4$  and then ammonium molybdate solution was added. With the assistance of potassium antimonyl-tartrate, a blue colour was developed the intensity of which was a linear function of the phosphorus content of the sample. The absorption of the samples at 882 nm was measured and the  $PO_4^{3\text{-}}$  content was determined using a calibration curve constructed by  $KH_2PO_4$  standard solutions.

Table 3.6: Water Quality Regulations

| Contaminant                | WHO (1993)*             | EU (1998)**   | Secondary MCL<br>(EPA)*** |
|----------------------------|-------------------------|---------------|---------------------------|
| Alkalinity                 | No guideline            | Not mentioned | Not mentioned             |
| Hardness                   | No guideline (1)        | Not mentioned | Not mentioned             |
| Electrical<br>Conductivity | No guideline            | 2,500 μS/cm   | Not mentioned             |
| TDS                        | No guideline (2)        | Not mentioned | 500mg/L                   |
| Salinity                   | No guideline            | Not mentioned | Not mentioned             |
| Calcium                    | No guideline (3)        | Not mentioned | Not mentioned             |
| Magnesium                  | No guideline (4)        | Not mentioned | Not mentioned             |
| Potassium                  | No guideline <b>(5)</b> | Not mentioned | Not mentioned             |
| Sodium                     | No guideline <b>(6)</b> | 200mg/L       | Not mentioned             |
| Iron                       | No guideline (7)        | 0.2mg/L       | 0.3mg/L                   |
| Boron                      | 0.3mg/L <b>(8)</b>      | 1.00mg/L      | Not mentioned             |
| Chloride                   | No guideline (9)        | 250mg/L       | 250mg/L                   |
| рН                         | No guideline (10)       | Not mentioned | 6.5 - 8.5                 |
| Nitrate                    | 50 mg/L <b>(11)</b>     | 50mg/L        | Not mentioned             |
| Sulfate                    | No guideline (12)       | 250mg/L       | 250mg/L                   |
| Phosphate                  | No guideline            | Not mentioned | Not mentioned             |

- (1) Desirable: less than 500mg/L
- (2) Desirable: less than 1200mg/L
- (3) Desirable less than 300mg/L
- (4) Desirable less than 300mg/L
- (5) Desirable less than 250mg/L
- (6) Desirable: less than 200mg/L
- (7) Desirable less than 0.3mg/L
- (8) Guideline value was increased to 0.5 mg/L in the addendum to the Guidelines published in 1998 by WHO.
- (9) Desirable less than 250mg/L
- (10) Desirable between 6.5-9.5
- (11) Because of the possibility of simultaneous occurrence of nitrite and nitrate in drinkingwater, it was recommended in the 1993 and 1998 Guidelines that the sum of the ratios of the concentration of each to its guideline value should not exceed 1.
- (12) Desirable less than 500mg/L

<sup>\*</sup>WHO's (World Health Organization) Guidelines for Drinking-water Quality, set up in Geneva, 1993, are the international reference point for standard setting and drinking-water safety.

<sup>\*\*</sup>Council Directive 98/83/EC on the quality of water intented for human consumption. Adopted by the Council, on 3 November 1998.

<sup>\*\*\*</sup>EPA (U.S. Environmental Protection Agency) has established National Secondary Drinking Water Regulations that set non-mandatory water quality standards for 15 contaminants.

#### 3.4 GIS and Remote Sensing methods and techniques

#### 3.4.1 GIS methods and techniques

#### 3.4.1.1 Defining Geographic Information System

"Geographic Information System (GIS) is defined as a computer-assisted mapping and cartographic application, a set of spatial-analytical tools, a type of database systems, or a field of academic study", Lo & Yeung, 2003. A simple working definition is: "GIS is an integrated system of computer hardware and software coupled with procedures and a human analyst which together support the capture, management, manipulation, and analysis, modelling, and display of spatially referenced data" (Lusch, 1999) (Fig. 3.15).

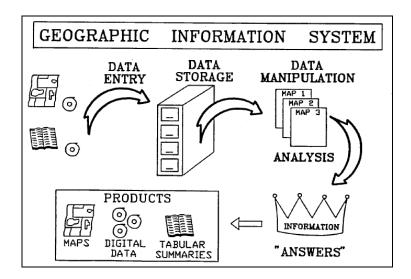


Fig. 3.15: Several steps describing a GIS procedure (Lusch, 1999)

#### 3.4.1.2 GIS software and extensions

The GIS software that was used is ArcView Desktop 9.1 from ESRI. It is a commercial software for visualizing, managing, creating, and analyzing geographic data. ESRI (Environmental Systems Research Institute) is located in Redlands, California (ESRI, 2009).

ESRI has built plug-in extensions which add functional capabilities to the main desktop products. In especial, three extensions were used for this thesis: **3D Analyst, Spatial Analyst**, and **Geostatistical Analyst**.

"ArcGIS 3D Analyst enables the operator to visualize and analyze surface data in three dimensions. Slope, aspect, hillshade and curvature maps were derived with 3D Analyst, giving the power to the user to effectively relate the data to real-world elevation", ESRI, 2009.

"ArcGIS Spatial Analyst is an extension which provides powerful tools for comprehensive, raster-based spatial analysis. Among others, it contains specialized tools for working with and deriving new information from hydrologic data and its toolset includes methods for describing hydrologic characteristics and tools to calculate flow across an elevation surface and derive features such as watersheds and stream networks, which were used for this thesis", ESRI, 2009.

"ArcGIS Geostatistical Analyst is an extension for advanced surface modelling using deterministic and geostatistical methods. Geostatistical Analyst extends ArcMap by adding an advanced toolbar containing tools for exploratory spatial data analysis and a geostatistical wizard to create a statistically valid surface", ESRI, 2009.

#### 3.4.1.3 Digital Elevation Models (DEMs) and derivatives

Paper and computer screens are two dimensional and the world is three dimensional; incorporating the third dimension into GIS has been an ongoing struggle. Cartographers have developed several conventions for representing the third dimension -elevation, topography, or terrain- on paper and computer screens. Most common is still the use of contour lines, but requiring more craft and skill, shaded relief and analytical hill shading are ways to depict the third dimension on a paper map or computer screen.

The raster data model incorporates elements of the third dimension as values in a cell. This is sometimes referred to as a 2.5-D model because the elevation is not directly part of the

model but is stored as an attribute of a two dimensional pixel. These models are also referred to as Digital Elevation Models (DEMs) (Harmon & Anderson, 2003).

Namely, DEMs are used to represent the surface topography of the earth. These models are commonly built from remote sensing data or from contour lines digitization from topographic maps (Shekhar & Xiong, 2008). As aforementioned, they are cell-based models and they are considered as the most common digital data of the shape of the Earth's surface.

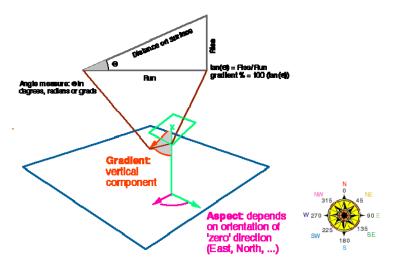
In the frame of this thesis, DEM was extracted by the digitization of 1:50,000 scale topographic map using a contour interval of 20m from Hellenic Military Geographical Service, Perama sheet (IGME, 1991).

The derivatives from DEM are: Slope, Aspect, Hillshade, and Curvature in ArcGIS 3D Analyst. Short description of each one is given next.

#### 3.4.1.3.1 Slope gradient

"Slope is the change in elevation between two points over a given distance, i.e. it identifies the steepest downhill slope for a location on a surface. Slope is calculated for each cell in rasters and, actually, it is the maximum rate of change in elevation over each cell and its eight neighbours", ESRI ArcGIS Desktop Help, 2004.

"The Slope function of ArcView calculates the maximum rate of change between each cell and its neighbours, for example, the steepest downhill descent for the cell. Every cell in the output raster has a slope value. The lower the slope value is, the flatter the terrain; and vice versa. The output slope raster can be calculated as percent of slope or degree of slope. When the slope angle equals 45 degrees, the rise is equal to the run. Note that as the slope approaches vertical (90°), the percentage slope approaches infinity", ESRI ArcGIS Desktop Help, 2004. For this thesis, degree option was chosen (Fig. 3.16).



**Fig. 3.16:** Slope components: slope gradient can be express in percent or in degrees and aspect is measured clockwise in degrees from 0 (due north) to 360, (again due north, coming full circle). (Modified from Dept of Geography - University of British Columbia, 2009).

#### 3.4.1.3.2 Slope aspect

"Aspect is the direction that a slope faces. It identifies the steepest downslope direction at a location on a surface. It can be thought of as slope direction or the compass direction a hill faces. Aspect is calculated for each cell in rasters", ESRI ArcGIS Desktop Help, 2004.

"It is measured clockwise in degrees from 0 (due north) to 360, (again due north, coming full circle). The value of each cell in an aspect dataset indicates the direction the cell's slope faces. Flat areas having no downslope direction are given a value of -1 (**Fig. 3.16**)", ESRI ArcGIS Desktop Help, 2004.

# 3.4.1.3.3 Hillshade

"A common use of the 2.5-D raster data model is hill shading. It is possible to shine artificial light on the area from a certain direction and elevation above the horizon and create a pattern of light and shadow that provides a visual sense of hills and valleys", ESRI ArcGIS Desktop Help, 2004.

"The Hillshade function of ArcView obtains the hypothetical illumination of a surface by determining illumination values for each cell in a raster. It does this by setting a position for a hypothetical light source and calculating the illumination values of each cell in relation to neighbouring cells", ESRI ArcGIS Desktop Help, 2004.

"By default, shadow and light are shades of gray associated with integers from 0 to 255 (increasing from black to white). The azimuth is the angular direction of the sun, measured from north in clockwise degrees from 0 to 360. An azimuth of 90 is east. The default is 315 (NW). The altitude is the slope or angle of the illumination source above the horizon. The units are in degrees, from 0 (on the horizon) to 90 degrees (overhead) and the default is 45 degrees", ESRI ArcGIS Desktop Help, 2004.

#### 3.4.1.3.4 Curvature

"As with slope, curvature values depend upon the line or plane along which such calculations are made. There are several alternative measures of surface curvature. The three most frequently provided within GIS software are profile curvature, plan curvature and tangential curvature", Geospatial analysis, 2009.

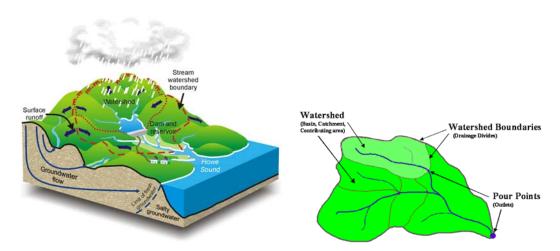
"The curvature of a surface is calculated on a cell-by-cell basis. A positive curvature indicates that the surface is upwardly convex at that cell. A negative curvature indicates that the surface is upwardly concave at that cell. A negative profile indicates that the surface is upwardly convex at that cell. A positive profile indicates that the surface is upwardly concave at that cell. A positive plan indicates that the surface is upwardly convex at that cell. A negative plan indicates that the surface is upwardly concave at that cell. A value of zero indicates that the surface is flat for all the three measures", ESRI ArcGIS Desktop Help, 2004.

#### 3.4.1.4 Hydrology - Basins

"In geomorphology, a drainage system is the pattern formed by the streams, rivers, and lakes in a particular drainage basin (which is also called watershed in the USA and catchment in

UK). In other words, drainage basin is the area upon which water falls, and the network through which it travels to an outlet is referred to as a drainage system (Fig. 3.17a)", Huggett, 2007.

"The drainage basin area is normally defined as the total area flowing to a given outlet, or pour point (Fig. 3.17b). An outlet, or pour point, is the point at which water flows out of an area. This is usually the lowest point along the boundary of the drainage basin. The boundary between two basins is referred to as a drainage divide or watershed boundary (Figs. 3.17a & 3.17b). The network through which water travels to the outlet can be visualized as a tree, with the base of the tree being the outlet. The branches of the tree are stream channels. The intersection of two stream channels is referred to as a node or junction. The sections of a stream channel connecting two successive junctions, or a junction and the outlet are referred to as stream links (Fig. 3.17b)", ESRI ArcGIS Desktop Help, 2004.



**Fig. 3.17**: Cartoon images illustrating a Drainage basin: a)(Geoscape Canada, 2009), b) (ESRI ArcGIS Desktop Help, 2004).

Hydrologic analysis was accomplished exclusively in ArcGIS Spatial Analyst, using the hydrologic tools. These tools were applied in sequence to extract hydrologic information from the DEM. We were allowed to identify and fill **sinks**, determine the **flow direction**, calculate the **flow accumulation**, **order** the segments in the network (Strahler ordering),

delineate the Geropotamos watershed and sub-watersheds, and finally, extract the stream network. A brief description of each tool and its application follows.

#### 3.4.1.4.1 Identifying and filling sinks

"Errors in DEMs are regularly classified as either sinks or peaks. A sink is an area surrounded by higher elevation values. In other words, a cell in the DEM that is lower than all surrounding cells. Some of these may be natural, although many sinks are imperfections in the DEM. Likewise, a spike or peak is an area surrounded by cells of lower value, and they are more commonly natural features. Sinks in DEMs are usually removed by common GIS software before attempting to derive any surface information because they can induce endless processing loops and truncate flow networks. To create an accurate representation of flow direction and, therefore, accumulated flow, it is best to use a dataset that is free of sinks", Maidment & Djokic, 2000.

In order to recognize the sinks in DEM, "Identify sinks" tool was used. "Finding sinks depends on knowing flow direction. At the end, as the sinks are recognised, they were removed using the "Fill Sinks" option", ESRI ArcGIS Desktop Help, 2004.

#### 3.4.1.4.2 Flow Direction

"Establishing the flow direction in a geometric network determines the direction in which commodities flow along each edge. The output of Flow Direction is an integer raster whose values range from 1 to 255. The values for each direction from the centre are shown in **Figure 3.18**", ESRI ArcGIS Desktop Help, 2004.

| 32 | 64 | 128 |
|----|----|-----|
| 16 |    | 1   |
| 8  | 4  | 2   |

Fig. 3.18: The values for each direction from the centre (ESRI ArcGIS Desktop Help, 2004).

"The direction of flow is determined by finding the direction of steepest descent from each cell. This is calculated as:

change in z value / distance \* 100

The distance is determined between cell centers. Therefore, if the cell size is 1, the distance between two orthogonal cells is 1, and the distance between two diagonal cells is 1.414", ESRI ArcGIS Desktop Help, 2004.

"If the descent to all adjacent cells is the same, the neighbourhood is enlarged until a steepest descent is found. If all neighbours are higher than the processing cell, it will be considered noise and filled to the lowest value of its neighbours, and have a flow direction towards this cell. However, if a one-cell sink is next to the physical edge of the raster or has at least one NoData cell as a neighbour, then it is not filled due to insufficient neighbour information. To be considered a true one-cell sink, all neighbour information must be present. If two cells flow to each other, they are sinks, and have an undefined flow direction", ESRI ArcGIS Desktop Help, 2004; after Jenson & Domingue, 1988.

#### 3.4.1.4.3 Delineating drainage basins

In order to delineate the drainage basins of the broad study area (and of course, Geropotamos drainage basin), the Basin function was used. "This creates a raster delineating all drainage basins within the analysis window. Basin analyzes the flow direction raster to find all sets of connected cells that belong to the same drainage basin. The drainage basins are created by locating the pour points at the edges of the analysis window (where water would pour out of the raster), as well as sinks, then identifying the contributing area above each pour point", ESRI ArcGIS Desktop Help, 2004.

#### 3.4.1.4.4 Flow Accumulation

After creating the flow direction grid (3.4.1.4.2 section), the flow accumulation grid was acquired. "Flowaccumulation" function creates a raster of accumulated flow to each cell, by

accumulating the weight for all cells that flow into each downslope cell (ESRI ArcGIS Desktop Help, 2004).

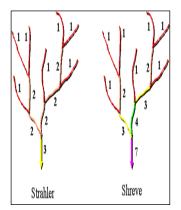
"The output of "FlowAccumulation" function represents the amount of rain that would flow through each cell, assuming that all rain became runoff and there was no interception, evapotranspiration, or loss to groundwater. This could also be viewed as the amount of rain that fell on the surface, upslope from each cell", ESRI ArcGIS Desktop Help, 2004.

"Output cells with a high flow accumulation are areas of concentrated flow and may be used to identify stream channels", ESRI ArcGIS Desktop Help, 2004.

#### 3.4.1.4.5 Stream Order and Stream Link

"Stream ordering is a method of assigning a numeric order to links in a stream network. This order is a method for identifying and classifying types of streams based upon their number of tributaries. Some characteristics of streams can be inferred by simply knowing their order", ESRI ArcGIS Desktop Help, 2004.

"For example, first-order streams are dominated by overland flow of water; they have no upstream concentrated flow. Because of this, they are most susceptible to nonpoint source pollution problems and can derive more benefit from wide riparian buffers than other areas of the watershed", ESRI ArcGIS Desktop Help, 2004.



**Fig. 3.19**: Strahler method for stream ordering. Stream order increases when streams of the same order intersect (ESRI ArcGIS Desktop Help, 2004).

"The Stream Order function has two methods you can use to assign orders. The Strahler method was chosen in the frame of this thesis. In the Strahler method, which is the most common, stream order increases when streams of the same order intersect (Fig. 3.19). Therefore, the intersection of two first-order links will create a second-order link, and the intersection of two second-order links will create a third-order link. The intersection of two links of different order, however, will not result in an increase in order. For example, the intersection of a first-order and second-order link will not create a third order link, but will retain the order of the highest ordered link", ESRI ArcGIS Desktop Help, 2004.

"The results of "FlowAccumulation" were used to create a stream network by applying a threshold value to select cells with a high accumulated flow. For this thesis, all cells that had more than 200 cells flowing into them were assigned 1; all other cells were assigned NoData", ESRI ArcGIS Desktop Help, 2004.

"The resulting stream network can be used as input to the "StreamOrder" and "StreamLink" functions. "Stream Link" function assigns unique values to sections of a raster linear network between intersections, ESRI ArcGIS Desktop Help, 2004.

# 3.4.1.4.6 Delineating watersheds (basins)

"A watershed is the upslope area contributing flow to a given location. Such an area may also referred to as a basin, catchment, subwatershed, or contributing area. A subwatershed is simply part of a hierarchy implying that a given watershed is part of a larger watershed. Watersheds can be delineated from a DEM by computing the flow direction and using it in the Watershed function. The Watershed function uses a raster of flow direction to determine contributing area. A flow accumulation threshold or the pour points were used to delineate watersheds. When the threshold is used to define a watershed, the pour points for the watershed will be the junctions of a stream network derived from flow accumulation. Therefore, a flow accumulation raster must be specified as well as the minimum number of cells that constitute a stream (the threshold value). When a feature dataset is used to define a watershed, the features identify the pour points", ESRI ArcGIS Desktop Help, 2004.

#### 3.4.1.5 Spatial Interpolation

As was mentioned in the introduction, ArcGIS Geostatistical Analyst Extension was used for the kriging estimations. Kriging was used to obtain the spatial distribution of groundwater quality parameters over the area and geophysical TEM data (3D imaging).

"Kriging is a moderately quick interpolator that can be exact or smoothed depending on the measurement error model. It is very flexible and allows you to investigate graphs of spatial autocorrelation. Kriging uses statistical models that allow a variety of map outputs including predictions, prediction standard errors, probability, etc. The flexibility of kriging can require a lot of decision-making", ESRI ArcGIS Desktop Help, 2004.

In this study, ordinary kriging was used. "Instead of weighting nearby data points by some power of their inverted distance, ordinary kriging relies on the spatial correlation structure of the data to determine the weighting values. This is a more rigorous approach to modelling, as correlation between data points determines the estimated value at an unsampled point. Furthermore, ordinary kriging makes the assumption of normality among the data points", Isaaks & Srivastava, 1989.

Therefore, kriging methods work best if the data are approximately normally distributed. Transformations were used to make data normally distributed and satisfy the assumption of equal variability for the data. In the ArcGIS Geostatistical Analyst, the histogram and normal QQPlots were used to check what transformations, if any, are needed to make the data more normally distributed. For a perfect normal distribution pattern skewness should be 0 and kurtosis 3. For those parameters which did not show normal distribution, a Log transformation has been applied to make the distribution closer to normal.

In this study, the semivariogram models (Circular, Spherical, Tetraspherical, Pentaspherical, Exponential, Gaussian, Rational Quadratic, Hole effect, K-Bessel, J-Bessel, Stable) were tested for each parameter data set. Prediction performances were assessed by cross-validation. Cross-validation allows determination of which model provides the best predictions.

#### 3.4.2 Remote Sensing

Among others, Campbell (2002) defines remote sensing as "the practice of deriving information about the earth's land and water surfaces using images acquired from an overhead perspective, using electromagnetic (EM) radiation in one or more regions of the EM spectrum, reflected or omitted from the earth's surface". Therefore, RS includes data analysis as well which involves the methods and processes for extracting significant spatial information from the remotely sensed data for direct input to a GIS. The software used for analysing satellite imagery in order to increase the value of the available geospatial information is ERDAS Imagine 9.1 from Leica Geosystems. It is a valuable survey tool, used throughout the geospatial community.

Within the frame of this thesis preliminary remote sensing analysis was attempted for detection and mapping of photo-lineaments indicating possible faulting. More details are given in **section 4.4** of *Chapter 4*.

# 3.5 Summary

A short description of the methodologies that were applied was given in this chapter. The two geophysical techniques: TEM and VES were presented first: basic principles, instrumentation used, etc. Then the standard procedures of the 15 chemical parameters determination followed, as described mainly in "Standard Methods for the examination of water and wastewater" (2005) handbook. After that, GIS was defined and its methods and techniques that used for this thesis were described. Finally, a short reference to remote sensing analysis was made. The results, processing, analyses and modelling chapter comes next, where all the extracted raw data after the application of the aforementioned methodologies are presented, as well as the results after their analyses and modelling.

# [RESULTS, PROCESSING, ANALYSIS & MODELLING]

# **Chapter Contents**

- **▶** Introduction
- ► Geomorphology Geropotamos Basin and Study Area
- ► Hydrology Geropotamos Basin and Study Area
- ► Remote Sensing analysis
- ► Geological Cross-sections
- ► Geophysical Approach
  - o EM Method TEM Technique
  - o DC Resistivity Method VES Technique
- **▶** Geochemical Analyses
  - Results of Chemical Analyses
  - Special Interpretation of the results
  - Ion exchange
- **▶** Summary

#### 4.1 Introduction

This chapter includes all the results derived from methods described in the previous chapter. GIS derivatives, RS preliminary results, and geophysical and geochemical data are presented first, and their processing, analysis and modelling are then described and final images are given.

# 4.2 Geomorphology - Geropotamos Basin and Study Area

An initial critical part of the analysis of the data for this thesis is to determine the geomorphological features of the area, which have been analysed using GIS, based on a Digital Elevation Model (DEM) and derivatives from it. The following sections show the various aspects of the geomorphology, of relevance to analysis of aquifer problems.

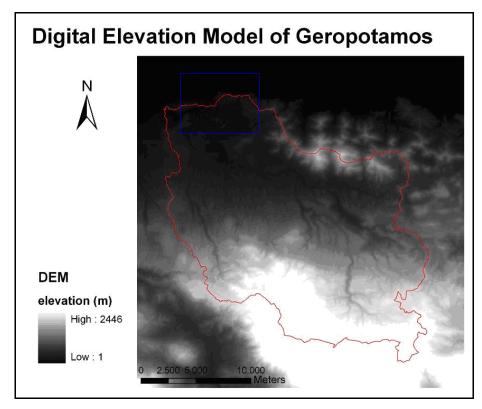
#### 4.2.1 Digital Elevation Model of Geropotamos area

A DEM (**Fig. 4.1**) was extracted by the digitization of 1:50,000 scale topographic map using a contour interval of 20m from the Hellenic Military Geographical Service, Perama sheet (HMGS, 1994). The method is described in **section 3.4.1.3** of *Chapter 3*. White colour indicates the high elevation, whereas the black colour indicates the low.

#### 4.2.2 DEM Reclassification

In order to use the DEM effectively, reclassification of the elevation was performed, using the "Spatial analyst" tool of ArcGIS. The Geropotamos basin was classified into 25 elevation zones (100m range), while the study area was divided into 10 elevation zones (50m range).

From **Table 4.1**, column diagram (**Fig. 4.2**) and elevation map (**Fig.4.3**), it can be seen that most of the area falls into zones 1-3 (101-400m). Within the study area, (**Table 4.2** & **Fig. 4.4**) the major elevation range is 50-100m.



**Fig. 4.1:** Digital Elevation Model (DEM) as extracted by the digitization of 1:50,000 scale topographic map using a contour interval of 20m. White colour indicates the high elevation, whereas the black colour indicates the low. The blue box specifies the study area.

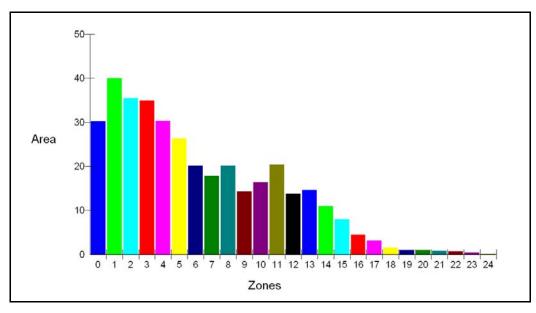


Fig. 4.2: Spatial extension of the 25 classes of elevation of Geropotamos basin.

# a) For Geropotamos basin

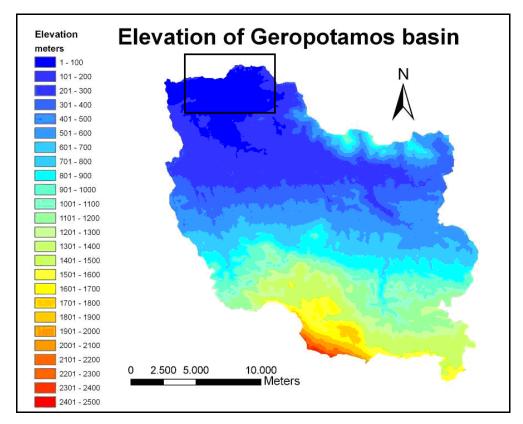
**Table 4.1:** Statistical analysis of the Geropotamos basin's elevation classified using an equal internal of 100 meters.

| Zones | Ranges    | AREA   | MEAN    | STD   |
|-------|-----------|--------|---------|-------|
| 0     | 0-100     | 30.286 | 65.31   | 21.81 |
| 1     | 101-200   | 40.083 | 151.33  | 29.32 |
| 2     | 201-300   | 35.543 | 249.47  | 28.86 |
| 3     | 301-400   | 35.004 | 349.38  | 28.72 |
| 4     | 401-500   | 30.328 | 449.10  | 29.33 |
| 5     | 501-600   | 26.350 | 548.87  | 28.63 |
| 6     | 601-700   | 20.247 | 647.34  | 28.37 |
| 7     | 701-800   | 17.924 | 752.57  | 28.90 |
| 8     | 801-900   | 20.231 | 847.91  | 28.28 |
| 9     | 901-1000  | 14.294 | 945.90  | 28.47 |
| 10    | 1001-1100 | 16.447 | 1057.57 | 28.00 |
| 11    | 1101-1200 | 20.362 | 1149.73 | 29.88 |
| 12    | 1201-1300 | 13.799 | 1247.97 | 29.74 |
| 13    | 1301-1400 | 14.684 | 1351.22 | 28.30 |
| 14    | 1401-1500 | 10.957 | 1447.59 | 29.22 |
| 15    | 1501-1600 | 8.031  | 1547.72 | 28.62 |
| 16    | 1601-1700 | 4.474  | 1644.07 | 29.58 |
| 17    | 1701-1800 | 3.117  | 1748.72 | 28.85 |
| 18    | 1801-1900 | 1.504  | 1842.48 | 28.32 |
| 19    | 1901-2000 | 1.000  | 1951.63 | 28.51 |
| 20    | 2001-2100 | 0.981  | 2050.59 | 28.92 |
| 21    | 2101-2200 | 0.771  | 2151.44 | 29.08 |
| 22    | 2201-2300 | 0.676  | 2250.22 | 28.85 |
| 23    | 2301-2400 | 0.482  | 2343.47 | 28.46 |
| 24    | 2401-2500 | 0.069  | 2420.45 | 16.89 |

# b) Study area

**Table 4.2:** Statistical analysis of study area's elevation.

| Zones | Ranges  | AREA    | MEAN   | STD   |
|-------|---------|---------|--------|-------|
| 1     | 0-50    | 10.7904 | 33.66  | 12.46 |
| 2     | 51-100  | 25.0100 | 75.02  | 14.05 |
| 3     | 101-150 | 16.4192 | 122.06 | 14.32 |
| 4     | 151-200 | 10.1656 | 174.35 | 14.26 |
| 5     | 201-250 | 2.2772  | 220.26 | 14.58 |
| 6     | 251-300 | 1.0428  | 272.37 | 14.57 |
| 7     | 301-350 | 0.4208  | 322.64 | 14.66 |
| 8     | 351-400 | 0.1952  | 369.07 | 17.53 |
| 9     | 401-450 | 0.1148  | 420.89 | 19.70 |
| 10    | 451-500 | 0.0556  | 471.09 | 14.63 |



**Fig. 4.3:** The Geropotamos basin showing the 25 elevation zones (100 m range). The black box specifies the study area.

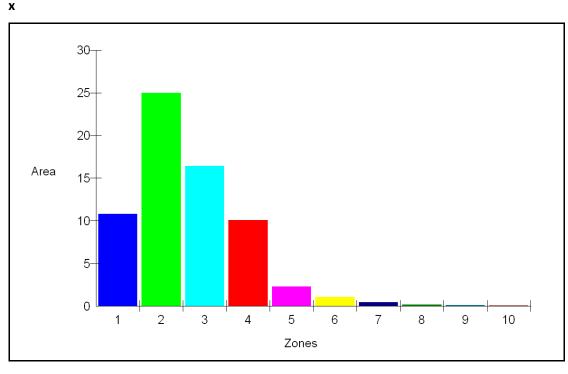


Fig. 4.4: Spatial extension of the 10 classes of elevation of the study area.

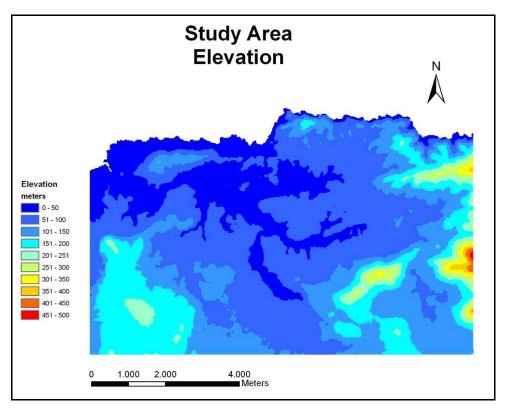
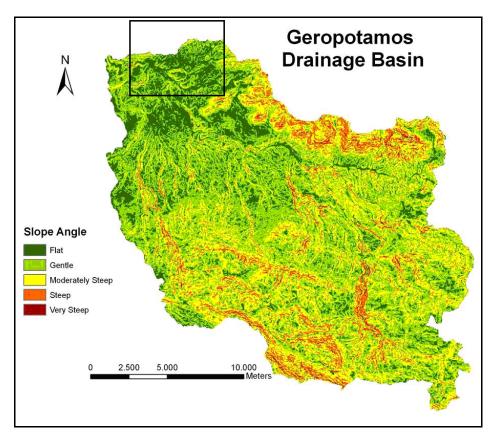


Fig. 4.5: The study area showing the 10 elevation zones (50 m range).

# 4.2.3 Slope angle & Curvature Maps

**Figures 4.6** and **4.7** present the slope gradient of Geropotamos basin and study area respectively, based on **Table 4.3**. The steepest slope areas are located on the north-east and south of the basin (**Fig. 4.6**).

A slope angle map and a curvature map were constructed for the study area showing similar results (Fig. 4.7 & 4.8). Excluding the far east part, the study area is generally flat (Fig. 4.7 & Table 4.3).



**Fig. 4.6:** Slope angle map of Geropotamos basin. The black box specifies the study area.

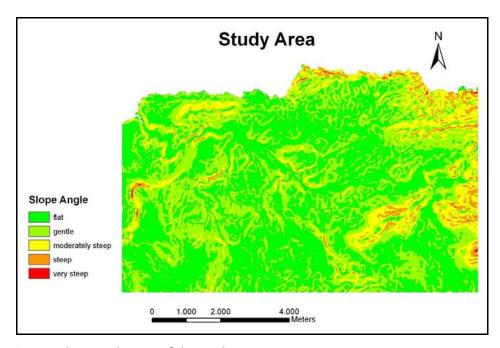


Fig. 4.7: Slope angle map of the study area

Slope Angle Characterization **AREA** MEAN STD flat 29.614 3.491 1.477 0-5.99 Gentle 26.390 9.628 2.727 6-15.99 21.974 Moderately steep 8.665 4.164 16-30.99 Steep 1.668 35.524 3.547 31-45.99 Very steep 0.058 49.190 2.956 >46

Table 4.3: Statistical analysis of slope angles of the study area

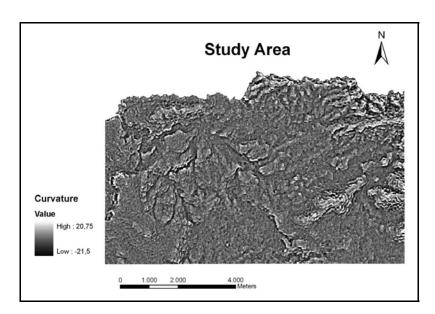


Fig. 4.8: Ground curvature map of the study area.

### 4.2.4 Aspect Map

**Figure 4.9** presents the aspect of the Geropotamos basin. It is shown that on the north-eastern part of the basin the aspect is mainly SSW.

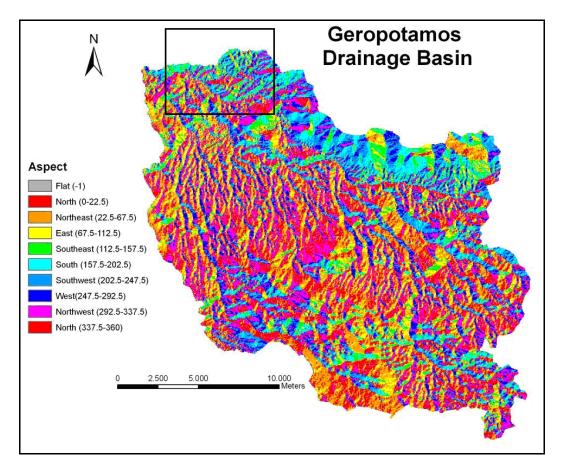
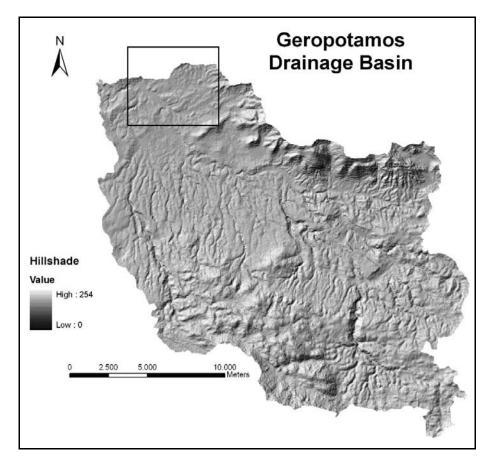


Fig. 4.9: Aspect map of Geropotamos basin. The black box indicates the study area.

# 4.2.5 Hill-shade Maps

Hill-shade maps were constructed to show the terrain of the Geropotamos and the study area (Figs. 4.10 & 4.11).



**Fig. 4.10:** Hill-shade map of the Geropotamos basin. The black box indicates the study area.

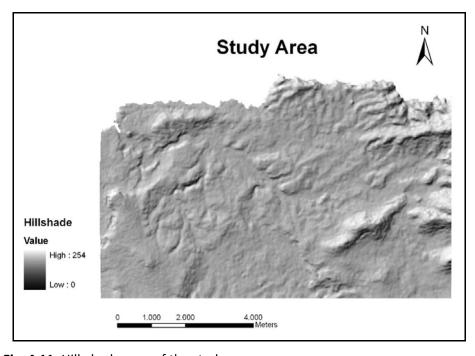


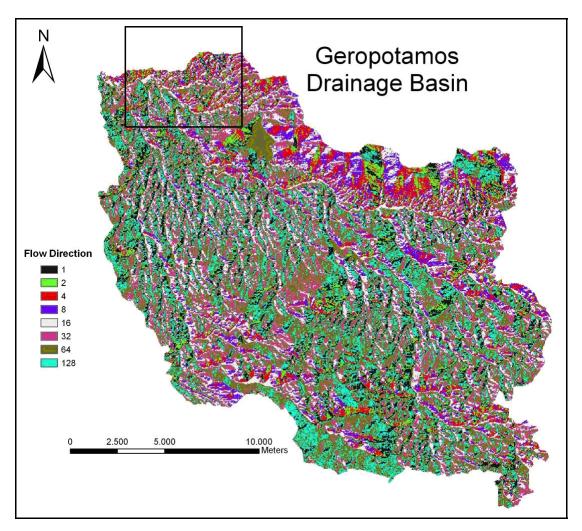
Fig. 4.11: Hill-shade map of the study area

# 4.3 Hydrology - Geropotamos Basin and Study Area

The Geropotamos basin, its drainage network and its sub-basins were extracted following the steps that described in **section 3.4.1.4** of *Chapter 3*.

#### 4.3.1 Flow Direction Map

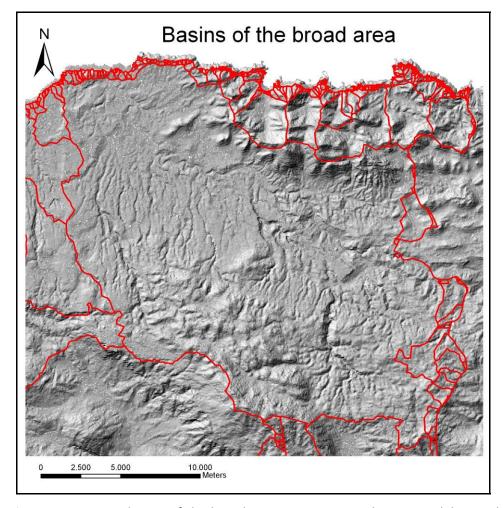
Initially, flow direction map of Geropotamos basin was extracted first. Each value (1, 2, 4, ..., 128) indicates a flow direction based on **Figure 3.18** of **section 3.4.1.4.2** of **Chapter 3**.



**Fig. 4.12:** Flow direction of the Geropotamos basin. The black box specifies the study area. Each value (1, 2, 4, ..., 128) indicates a flow direction based on **Figure 3.18** of **section 3.4.1.4.2** of **Chapter 3**.

# 4.3.2 Delineating Drainage Basins of the broad area

Next, the drainage basins of the broad area (including Geropotamos drainage basin) were delineated (Fig. 4.13).

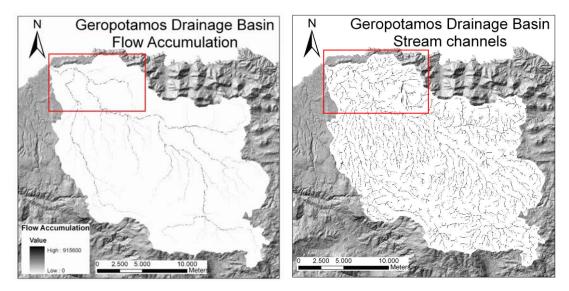


**Fig. 4.13:** Drainage basins of the broad area. Geropotamos basin was delineated as well.

#### 4.3.3 Flow Accumulation

As described in **section 3.4.1.4.4** of *Chapter 3*, the output of "Flow Accumulation" tool represents the amount of rain that would flow through each cell (Fig. 4.14a). Then, output cells with high flow accumulation (areas of concentrated flow) were used to identify stream

channels. The stream network was created by applying a threshold value of 200 to select cells with a high accumulated flow (Fig. 4.14b).



**Fig. 4.14**: a) Flow accumulation of Geropotamos basin and b) stream network created by applying a threshold value of 200

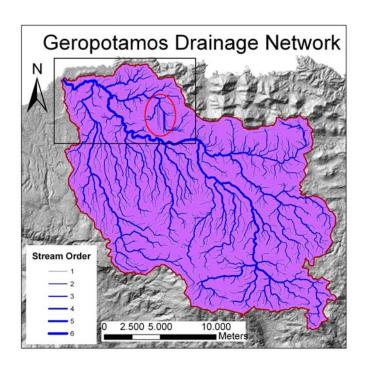
# 4.3.4 Drainage Network of Geropotamos

The resulting stream network, as shown above, was used as input to the "StreamOrder" function. So, by applying Strahler's method (section 3.4.1.4.5 of *Chapter 3*) stream orders were determined (Fig. 4.15). Data on the number of channels and length of channel in each Strahler category is given in Table 4.4.

Drainage network of Geropotamos basin, as extracted from DEM, is in a good agreement with the satellite image. In addition, it is more detailed (20m DEM) than previous drainage networks existed up to now (e.g. topographic map). However, when network is extracted by DEM sometimes errors occur. For Geropotamos application, generally there was not such a problem, except from some possible artefacts at the north-eastern part of the basin (within red ellipsis). Usually, possible artefacts are recognised as 1<sup>st</sup> order streams that seem perfectly linear and parallel to each other.

| Strahler Ordering | Number of channels | Length of channels (m) |  |  |
|-------------------|--------------------|------------------------|--|--|
| Order 1           | 1103               | 442,513                |  |  |
| Order 2           | 529                | 231,146                |  |  |
| Order 3           | 301                | 143,237                |  |  |
| Order 4           | 152                | 66,405                 |  |  |
| Order 5           | 46                 | 21,366                 |  |  |
| Order 6           | 58                 | 19 708                 |  |  |

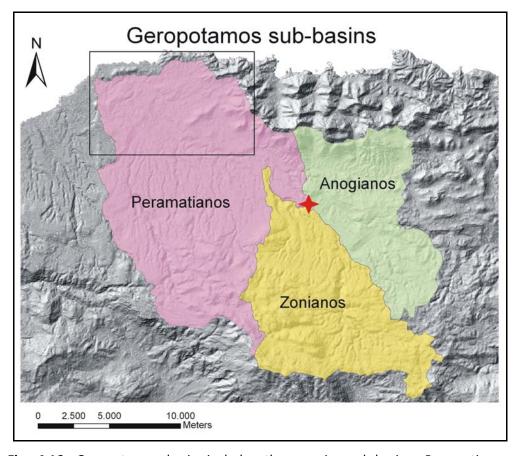
**Table 4.4:** Information for number of channels and length of channels in each Strahler's order



**Fig. 4.15:** Drainage network of Geropotamos basin as extracted from DEM. Geropotamos River has 6 orders. The black box indicates the study area. Red ellipse shows some possible errors (see text).

#### 4.3.5 Delineating sub-basins

Geropotamos basin includes 3 major sub-basins, Peramatianos, Anogianos, and Zonianos. These sub-basins were delineated again within the frame of this thesis, using DEM based on the classified drainage network, as described above (**Fig. 4.16**). As the Geropotamos drainage network has 6 orders, the pour point at the beginning of the fifth class segments (red star), were chosen to define the three 5<sup>th</sup> order sub-basins.



**Fig. 4.16**: Geropotamos basin includes three major sub-basins: Peramatianos, Anogianos, and Zonianos. The black box defines the study area, and the red star indicates the pour point at the beginning of the fifth class segments (see text for more explanation).

#### 4.4 Remote Sensing analysis- Digital processing of Landsat-ETM imagery

Preliminary remote sensing analysis ensued for detection and mapping of photolineaments indicating possible faulting. The term lineament has been propagated in remote sensing geology the last years and represents the most obvious linear features on aerial or satellite images (Gupta, 2003). Among others (roads, tree arrays, etc), lineaments are indicators of possible faulting.

The output images were generated from the analysis and processing of a cloud-free Landsat-ETM (Landsat 7) satellite image acquired on 30/06/2000 with a resolution of 30 m. Remote sensing analysis was taken place in the Laboratory of Geoinformatics of TEI of Crete (Branch

of Chania), in collaboration with Dr. Maria Kouli. Imagery and ERDAS software were also provided by the institute.

Primarily, **Figure 4.17** shows only for visual purposes (visual interpretation) Landsat-ETM satellite image with band combination 5,7,3 (R,G,B). Several band combinations were produced and that combination (5-7-3) was selected as the most informative band combination since bands 5, 7 and 3 are less correlated, since band 4 was excluded because we wished to eliminate the effect of vegetation.

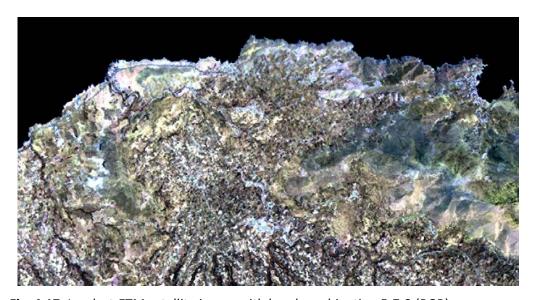


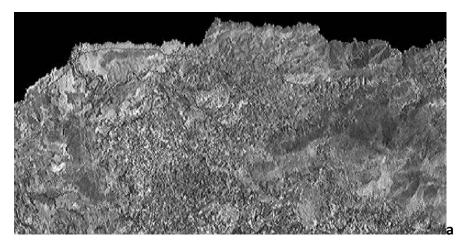
Fig. 4.17: Landsat-ETM satellite image with band combination 5-7-3 (RGB).

The lineament-enhancement techniques, and specifically directional spatial filtering (Rigol & Chica-Olmo, 1998; Rokos et al., 2000), were applied on Band 5 of Landsat-ETM image in order to investigate the basic tectonic pattern of the study area. Specifically, band 5 was chosen as it has little vegetation effect, and is a band which records well the geology (i.e. gives the best discrimination of rock. As a result four enhanced images were created (**Fig. 4.18a**, **Fig. 4.18b**, **4.18c** & **4.18d**) after the application of the following directional masks (Miliaresis, 2003; Tso & Mather, 2009).

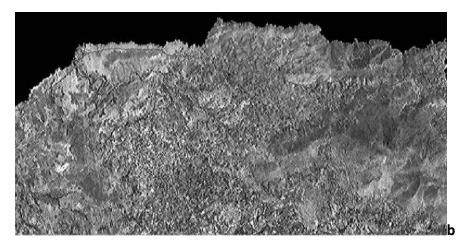
| N  | orth-So | uth | V | Vest-Eas | st |    | NE-SW |    |    | SE-NW |    |
|----|---------|-----|---|----------|----|----|-------|----|----|-------|----|
| 0  | -1      | 0   | 0 | -1       | 0  | -1 | 0     | 0  | 0  | 0     | -1 |
| -1 | 2       | 0   | 0 | 2        | 0  | 0  | 2     | 0  | 0  | 2     | 0  |
| 0  | 0       | -1  | 0 | -1       | 0  | 0  | 0     | -1 | -1 | 0     | 0  |

After the filter application, the initial image (band 5) was added on them.

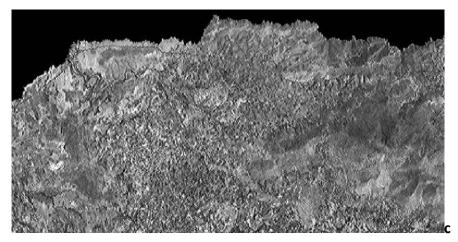
N-S



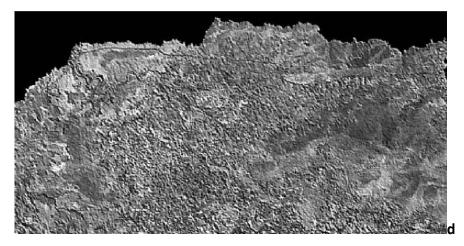
W-E



NE-SW



#### **NW-SE**

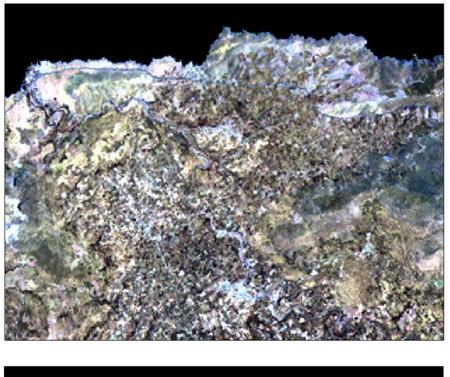


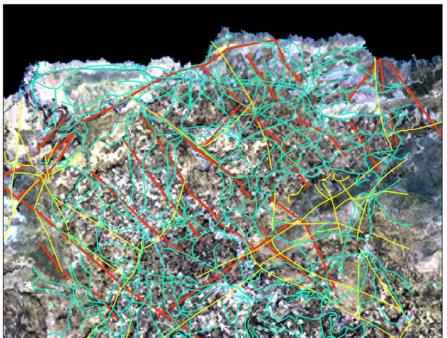
**Fig. 4.18 a, b, c, d**: Enhanced images generated using N-S, W-E, NE-SW, and NW-SE directional masks respectively, applied on band 5

Finally, one individual vector layer of lineaments was created by "on-screen digitizing" (process in which a map is created using previously digitized of scanned information or it is used to trace features from a scanned map or image to create new layers or themes) of the lineaments derived from the four enhanced images (after N-S, W-E, NE-SW, and NW-SE directional filtering) (**Fig. 4.19b**, vector layer of lineaments with red colour).

The derived lineament vector layer was statistically analyzed and a rose diagram was generated in order to extract the major lineament orientation. **Figure 4.20a** presents the rose diagram, and it seems that the dominant direction that the lineaments follow is NNW-SSE. There are some more minor directions, e.g. one similar to the major, one with NNE-SSW direction, etc.

**Figure 4.20b** shows a second rose diagram that was created as well, using a vector layer containing the faults digitized from IGME map (**section 2.2.4** of **Chapter 2**). The two rose diagrams show that lineament patterns of Landsat-ETM and IGME map are similar. It was concluded from both diagrams that lineaments follow the NNW-SSE dominant direction (one major fault group). Note that this remote sensing analysis is preliminary and fieldwork for identification of possible faults, derived from satellite image interpretation (RS faults), is required as future work.





**Fig. 4.19: a)** Satellite image of the study area (Landsat-ETM satellite image with band combination 5,7,3 (R,G,B), and **b)** the same image with vector layers of lineaments overlaid: i) faults derived from satellite image interpretation (RS faults) (red colour), ii) faults and thrusts digitized from IGME map (yellow colour), and iii) road network derived from air-photos interpretation as provided by municipality of Geropotamos (turquoise colour)

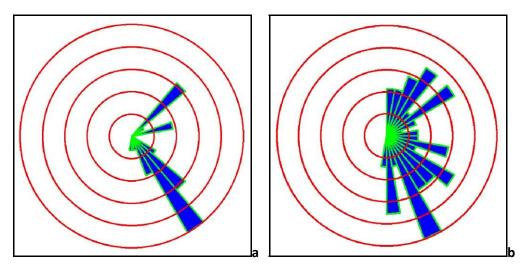


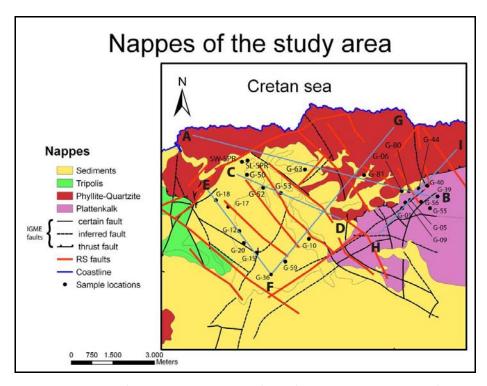
Fig. 4:20: Rose diagrams of lineament density (length) for a) RS faults, b) IGME faults and thrusts

#### 4.5 Geological cross-sections

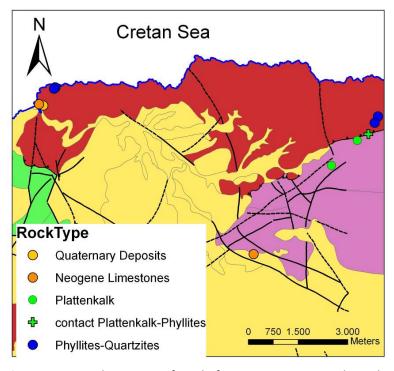
Five simple geological cross-sections (AB, CD, EF, FG, and HI) were constructed for better comprehension of the geological setting of the study area (Figs. 4.25a, 4.25b, 4.25c, 4.25d & 4.25e).

The cross-sections were positioned to meet the following requirements: a) the lines should cross through all the nappes, b) they should cross near the geochemical sample locations (**Fig 4.21**), c) they should cross near the three VES soundings (**section 4.6.2.1**), and d) wherever TEM grid was dense enough (**Fig. 4.2.6**).

The data sources that were used for their construction were: a) the 1:50,000 IGME map (section 2.2.4 of *Chapter 2*), b) information from the borehole logs (Appendix A), whenever it was available, c) possible faults that were extracted from Remote Sensing analysis (section 4.4), and d) data that collected after 4-day fieldwork for geological observations with my supervisor, Dr. Stephen Kershaw, in February 2008. A short description of this fieldwork follows.



**Fig. 4.21:** Nappes of the study area with: i) the five geological sections (AB, CD, EF, FG, and HI), ii) the faults derived from satellite image interpretation (RS faults), and iii) IGME faults layers overlaid. Source of nappes mapping is IGME geological map.



**Fig. 4.22:** GPS locations of rock formations examined in the study area.



**Fig. 4.23: a)** and b) depict from different directions the contact between phyllite/quartzite and plattenkalk nappe located at the north-eastern part of the study area: a) shows the iron-stained yellow colour of the quartzite-phyllite thrust over the grey-coloured limestones of the Plattenkalk nappe, view to south; **b)** shows the same site view to north, so the thrust is clearly visible in the centre of the photograph; **c)** the phyllites near the thrust fault showing distortion and pervasive fracturing due to friction between the two rock masses; d) the dolomitic limestones (plattenkalk nappe) below the fracture portion of the thrust fault zone.

Between 16 - 19 February, with the guidance of my supervisor Dr. Stephen Kershaw, brief geological observation was accomplished. All rock formations of the study area were recognized, located by GPS, and rock samples were collected (Fig. 4.22). A key feature is the contact (thrust fault) between phyllites/quartzites and plattenkalk nappe at the north-eastern part of the area (Fig. 4.23a, 4.23b, 4.23c, & 4.23d).

In addition we visited for the first time the site where the salty-sweet spring phenomenon takes place (section 2.3 of *Chapter 2*). Mr. Vassilis Simitzis joined us on this visit, providing useful information (Fig. 4.24a & Fig. 4.24b). A similar occurrence takes place at the Loutraki

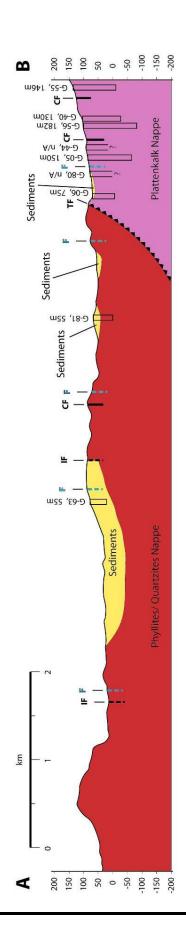
spring on the Perahora peninsula just north of Korinthos in central Greece, where at that case the distance between the two springs is only 1 m (Steve Kershaw, personal communication).

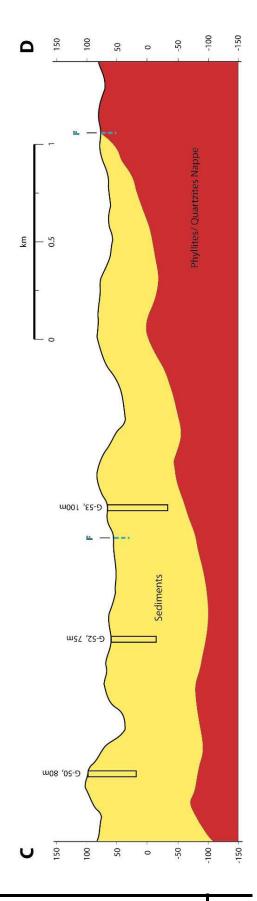


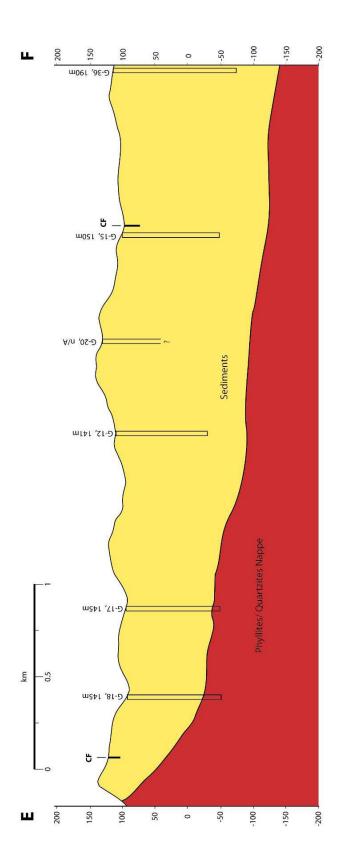


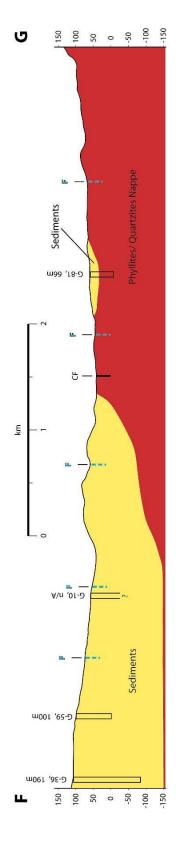
**Fig. 4.24:** Sweet-salty spring phenomenon in Geropotamos study area.In the left-hand photograph, the salty spring is out of view near the left hand side of the photo, and the stream from the salty spring is directed along the cliff base. Water from the sweet spring is shown directed away from the cliff in the right hand photograph. The two springs meet just to the right of the two people off the edge of the right-hand photograph.

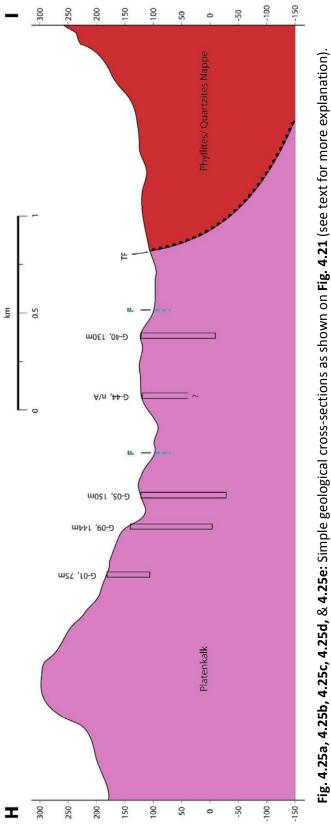
The five simple geological cross-sections follow next: AB (9 km), CD (4 km), EF (4 km), FG (7 km) and HI (4 km). Above each borehole is situated its name and its depth. Boreholes with (?) continue below the level drawn but the amount of borehole below that level is not known. The boundaries of rock units are the best estimated obtainable for the map and the borehole data. Solid and dashed black colour lines indicate Certain Faults (CF) and Inferred Faults (IF) as derived from IGME map respectively, while blue solid lines (RS faults) indicate faults derived from satellite image after remote sensing analysis (section 4.4 of this chapter). There is no information about the direction of the faults (from the geological map or from fieldwork), so they are drawn as short line.





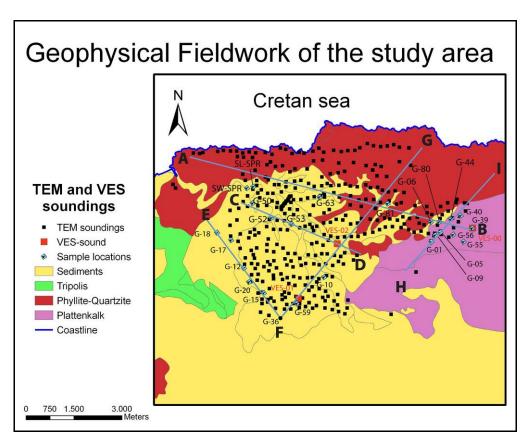






#### 4.6 Geophysical Approach

This section presents the complete TEM and VES surveys and results. The instrumentations and softwares were provided by Laboratory of Geophysics and Seismology of TEI of Crete (Branch of Chania) and the geophysical surveys were designed and accomplished in collaboration with Dr. Pantelis Soupios, Associate Professor of TEI, Dept of Natural Resources and Environment.



**Fig. 4.26:** Nappes of the study area with: TEM profiles (having the same position with AB, CD, EF, FG, and HI cross-sections), VES soundings, and sample locations layers overlaid.

# 4.6.1 EM method - TEM technique

#### 4.6.1.1 TEM measurements in Geropotamos study area

All TEM data were collected mainly within 3 months (June, July, and August of 2008) (**Fig. 4.27**). In total, one thousand one hundred seventy-nine (1179) TEM soundings were acquired

in three hundred seventy-two (372) different locations in a detailed survey grid (about 200-250 m in X and Y dimension) using mainly single loop 50 x 50 m, Stack 5 (65 complete cycles) and Time 5 or 6 (i.e. 32 or 36 time gates), in order to be able to image a possibly complex (3D or due to the tectonic) subsurface. The large number of the TEM soundings reflects the fact that the measurements were repeated several times at each sounding location, in order to define and avoid aliasing effects (high frequency - HF noise from radio sources) and generally for optimisation of the raw data.

During the TEM fieldwork, the author/operator was very careful for the best possible site selection, the correct installation of the loop, and other conditions which can produce noisy and bad quality data, like man-made noise (power and telephone lines, pipelines, fences, etc). Notwithstanding, some of the final acquired data were affected by resonance of power lines, by strong SPM (Super Para Magnetic) effects in the locations composed of dolomitic limestones (Plattenkalk nappe at the eastern part of the study area), and rarely aliasing effects from high frequency noise (section 3.2.1.3.3 of *Chapter 3*). Some of those data were totally removed. Finally, data of 350 of the 372 locations were used (Appendix B). Those data were filtered, smoothed and corrected prior to the final modelling and imaging.

## 4.6.1.2 Processing & analysis of TEM data

TEM data from a field instrument consist of an approximately exponential voltage decay curve. The way to interpret these data is to convert the field data to apparent resistivities,  $\rho(t)$ . TEM-Fast 48 raw data come directly in ohm.m (resistivity data) (an example of sounding 0071-B is shown in **Fig. 4.32a**).

TEM-RES software, available with the TEM-Fast 48 instrument, is a Windows integrated software system, which was the tool for data processing of TEM data and then for the inverse problem solution. This program is used for TEM data editing, smoothing, analysis, processing, and modelling (TEM-RES manual, 2007).







Fig. 4.27: TEM data acquisition in Geropotamos study area. At the two lower photos, the two participants set the antenna  $(50 \times 50 \text{ m square})$ .

Once the resistivity data were derived, the next stage was modelling of the data, as the ultimate goal was to deduce the subsurface resistivity distribution (resistivity-depth information) from these sounding curves. Before that, editing and smoothing of the data was required.

Editing was a very important part of the analysis of the data of the study area. For example, the author/analyst had to correct mistakes contained in the head of the field data (Name, TR, REC, coordinates). Other options were the exclusion of points from the resistivity curves and the change of position of a point. Generally, the quality of the data was very high and almost no editing was required, except the head correction of the files.

The next step after editing, and before modelling, was the smoothing of the data, as the manufacturer strongly suggests. In **Figure 4.32a** an example of data smoothing is shown. Two more curves, except the resistivity curve, are given as result of the raw data smoothing. The first (upper) continuous curve approximates initial  $\rho_{\alpha}(t)$  data and the second (lower) curve is the calculated dependence  $\rho_{\text{full}}(t)$ .

At that stage, before modelling, it was decided which locations finally would be used for further modelling, and then the best measurement of each location was chosen. In some areas a strong superparamagnetic effect (section 3.2.1.3.3 of *Chapter 3*) destroyed the data, which at the end were excluded. Two such examples are Maniaki site at the eastern part), and Melidoni cave (at the south-eastern part).

## Super ParaMagnetic Effect in Geropotamos study area

• Maniaki is a place lying on dolomitic limestones very close to G-39 sample location. (50x50 loop size, Time=6, stack=7). The site that was chosen for the following TEM sounding was on "terra rossa" kind of soil which generally considered to contain large amount of magnetic constituents, like magnetite. Figure 4.28 presents the resistivity curve which was excluded from further analysis and modelling.

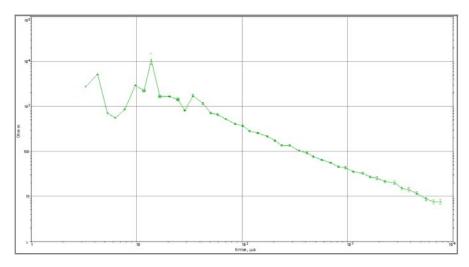
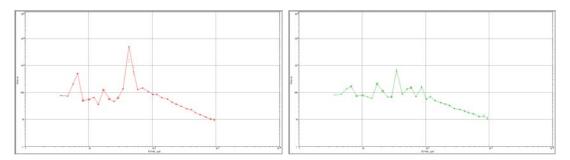
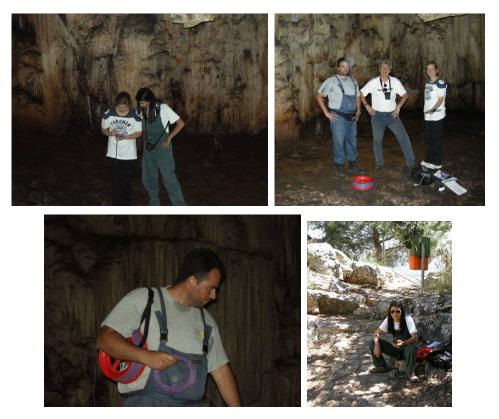


Fig. 4.28: Resistivity curve of Maniaki (near G-39 sample location) (50 x 50 m loop size, Time=6, stack=7)

Two TEM soundings took place at Melidoni cave: one exactly at the entrance of the cave and the other in it, after special permission (Figs. 4.30a, 4.30b, 4.30c & 4.30d).
 Both measurements showed SPM effect and they were not used any further (Fig. 4.29).



**Fig. 4.29:** Resistivity curves with SPM effect. Red=in Melidoni cave, Green=out of the cave (25 x 25 m loop size, Time=5, Stack=5)



**Fig. 4.30a, 4.30b** & **4.30c**: TEM measurements in Melidoni cave; **4.30d**: TEM measurements in front of the cave

#### 4.6.1.3 Modelling of TEM data

Construction of a section can be completed in two ways by the TEM-RES software: transformation and inversion.

The first involves the description of the theory of transformation of the resistivity curve  $\rho_{\alpha}(t) = \mathrm{Res}(t)$  (section 3.2.1.3.2 of *Chapter 3*) in pseudosection  $\rho(h) = \mathrm{Res}(h)$ , where  $\mathrm{Res}(h)$  is the specific resistivity, is not the scope of this section, as it is described analytically in Svetov & Barsukov (1984). It is a quick and simple approach to EM interpretation, which can be used in situ, as well, immediately after the acquisition of the TEM data.

Next, the section deals with basic concepts underlying geophysical inversion, where an overview of essential ideas without mentioning mathematical details is provided, as first described by D.W. Oldenburg and F.H.M. Jones (2007).

"In a typical geophysical survey, we put energy into the ground and record a response, which we refer to as data or observations. The values of the data depend upon the distribution of physical properties in the subsurface. The goal of the inverse problem is to determine the distribution of the physical property or properties that gave rise to the data. Unfortunately, this is not rigorously possible in practical surveys because only a limited number of data can ever be recorded and the data are also inaccurate. Nevertheless, approximate solutions can be found, and the methodology is designed to include other information about the problem so that the calculated solution is more likely to represent the true earth structure", Oldenburg and Jones, 2007.

"Inversion is a mathematical procedure that can take on several forms. In order to generate understanding about the subsurface without digging or drilling, measurements must be gathered, data must be generated from these measurements, and some degree of understanding about what is being investigated ("prior knowledge") should exist. Then inversion processing can be carried out, using the data and prior knowledge as input. The result will be a set of "models" characterizing how the relevant physical property is

distributed in the ground. These models will have characteristics determined by the inversion method used, by the data and by prior knowledge (**Fig. 4.31**)", Oldenburg and Jones, 2007.

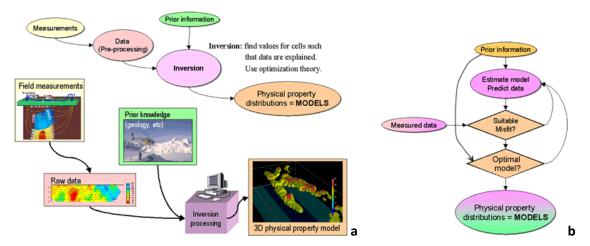


Fig 4.31: a),b) Flow charts showing the basic ingredients of inversion, b) The arrows in Figure 3b show how information is used and where iteration (feedback) occurs (Oldenburg and Jones, 2007)

"The **Inversion** section of **Fig. 4.31** consists of a model estimation algorithm and two decisions which must be made before the model is considered satisfactory. The principle requirements of inversion are: **1**) A model must be estimated and resulting predicted data must be calculated, **2**) Predicted and measured data must compare favourably, and**3**) The model must optimal in some well-defined sense", Oldenburg and Jones, 2007.

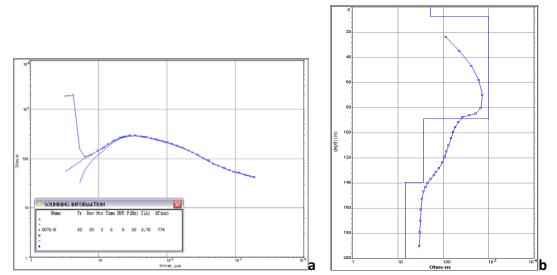
"A solution to the inverse problem is obtained by estimating a model, testing it using misfit and acceptibility criteria, and then iteratively perturbing (i.e. adjusting) the model until the two testing criteria are satisfied. The arrows in Figure 3b show how information is used and where iteration (feedback) occurs", Oldenburg and Jones, 2007.

As mentioned above, TEM soundings are commonly used to define aquifer properties and other subsurface characteristics. Of course, those kinds of structures are multi-dimensional, but 1D inversions are used to determine geologic structure for groundwater flow models. Generally, they can be imaged without significant errors. For this thesis it is not necessary to describe the formulae that TEM-RES software uses for the inversion procedure.

## 4.6.1.3.1 1D Modelling

As already mentioned, **Figures 4.32a** & **4.32b** show 0071-B sounding, as an example. Transformation Res(h), which is distribution of specific resistivity versus apparent depth (smooth curve), and the model after 1D inversion (piecewise-uniform diagram) are presented in **Figure 4.32b**. Together with the resistivity curve (**Fig. 4.32a**), two more curves are shown as result of the raw data smoothing. The first (upper) continuous curve approximates initial  $\rho_a(t)$  data and the second (lower) curve is the calculated dependence  $\rho_{full}(t)$ . For better interpretation, after Dr. Pavel Barsukov's recommendation, an upper threshold 1000 ohm.m was set.

These kinds of diagrams were extracted for all the 350 TEM locations. Results after 1D inversion are included in Appendix E (CD attached to the back cover of the thesis).



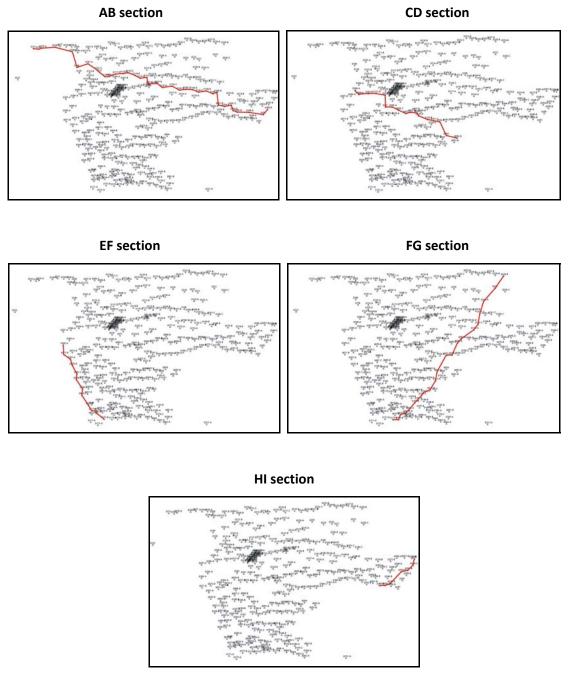
**Fig. 4.32: a)** Curve of apparent resistivity pa(t) (example of sounding 0071). Two more curves are given as result of the raw data smoothing. The first (upper) continuous curve approximates initial pa(t) data and the second (lower) curve is the calculated dependence pfull(t), **b)** The transformation (p(h)) and inversion (example of sounding 0071) are presented by the smooth curve and the piecewise-uniform diagram, respectively.

## 4.6.1.3.2 2D Imaging of TEM data

Since the 1D modelling is not enough to reconstruct and describe the subsurface, 2D imaging is required. TEM-RES software is a great tool for geoelectrical sections construction as well. The sections that were chosen for 2D imaging stay at the same position with the geological cross-sections that were constructed as shown previously (section 4.5 of this chapter) (Fig. 4.21). Exactly the same positions were used to allow for direct comparison between the geology and TEM results (section 5.4 of *Chapter 5*).

So, data from transformation and 1D inversion were received, and 6 different versions of each profile (AB, CD, EF, FG, and HI) were illustrated: 1) transformation loggings, 2) transformation as tomography, 3) transformation as tomography with 1D inversion loggings, 4) 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, and 6) 1D inversion as tomography. 2D geoelectrical sections (as Tomographies) are the colour presentation of the structure. Hot colours (red) represent high resistivity formations, while the cold colours (blue) depict the low resistivity units. All the different versions of each section are following. The 3x exaggeration of all the sections is that same as that used for the construction of the geological cross-sections.

Note that, even though the sections that were chosen for 2D imaging stay at the same position with the geological cross-sections for direct comparison, each 2D section is a crooked line and not exactly the same straight line (Figs. 4.33a, 4.33b, 4.33c, 4.33d & 4.33e) like the geological cross sections. TEM data are scarcer than DEM, so for TEM resistivity tomographies construction the best estimated lines where selected (red crooked lines). In addition, each profile is composed only by the elevation of points (sites located in fieldwork by GPS), which means that any elevation changes between them is not visible.



**Fig. 4.33:** TEM soundings acquired in the study area. Red colour crooked lines were selected for AB, CD, EF, FG and HI 2D geoelectrical sections construction.

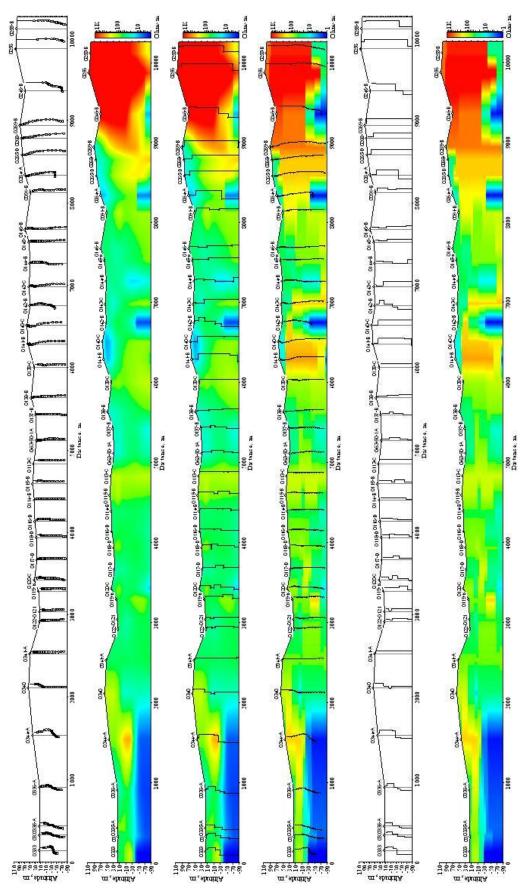
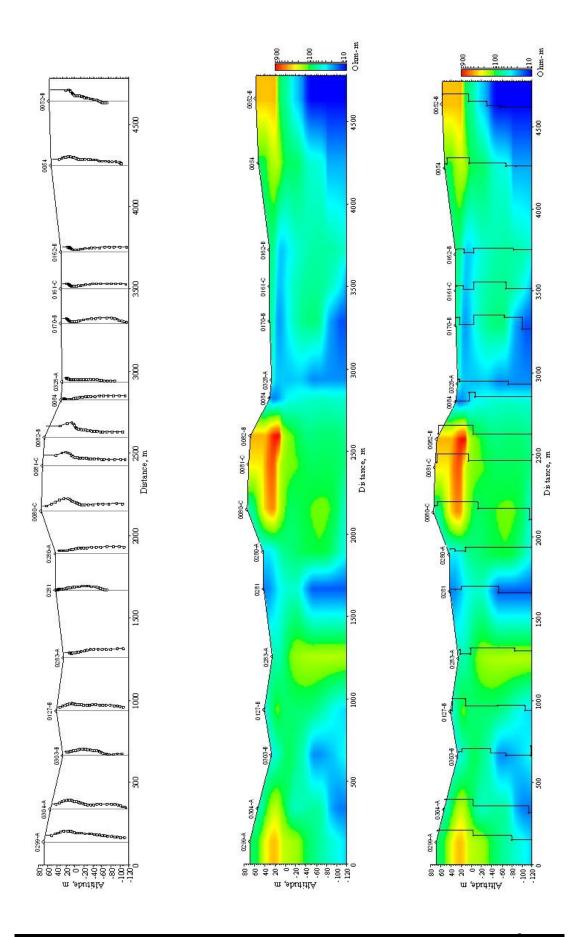


Fig. 4.34: 2D imaging of section AB: 1) transformation loggings, 2) transformation as tomography, 3) transformation as tomography with 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, 4) 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, 4) 1D inversion as tomography.



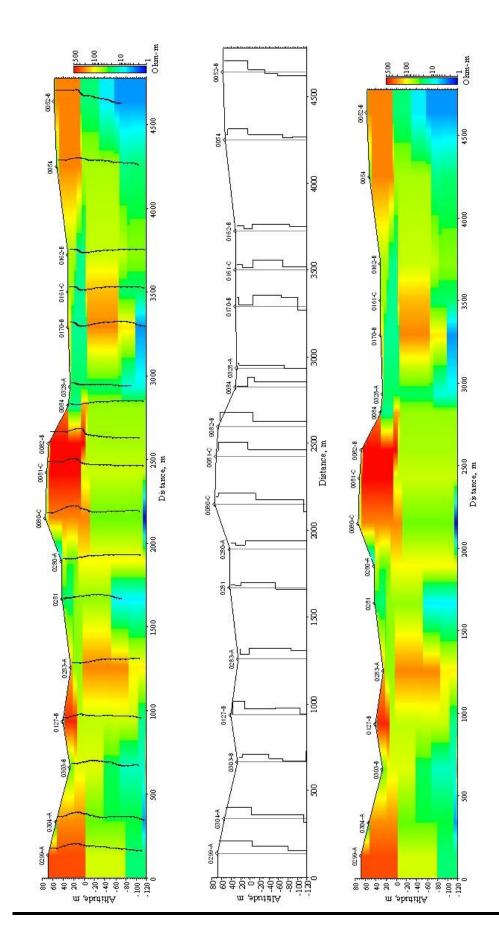
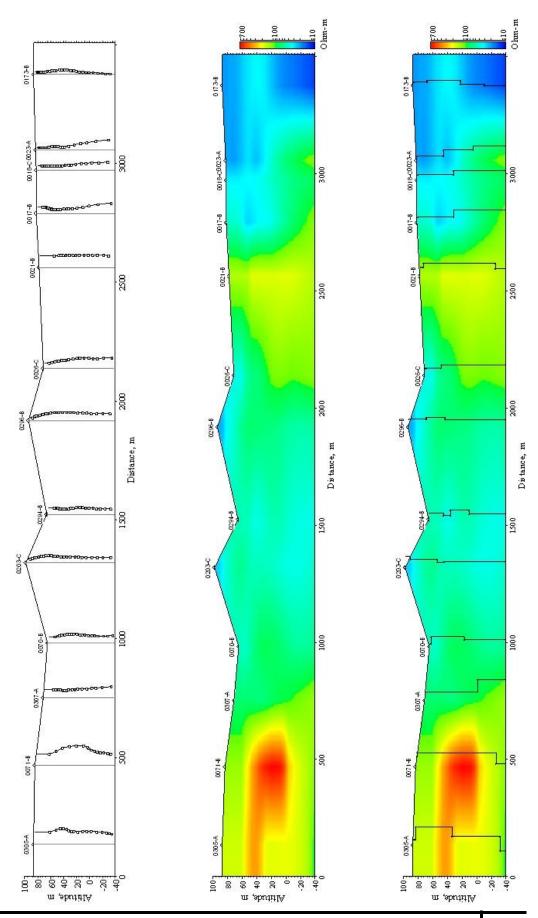


Fig. 4.35: 2D imaging of section CD: 1) transformation loggings, 2) transformation as tomography, 3) transformation as tomography with 1D inversion loggings, 4) 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, and 6) 1D inversion as tomography.



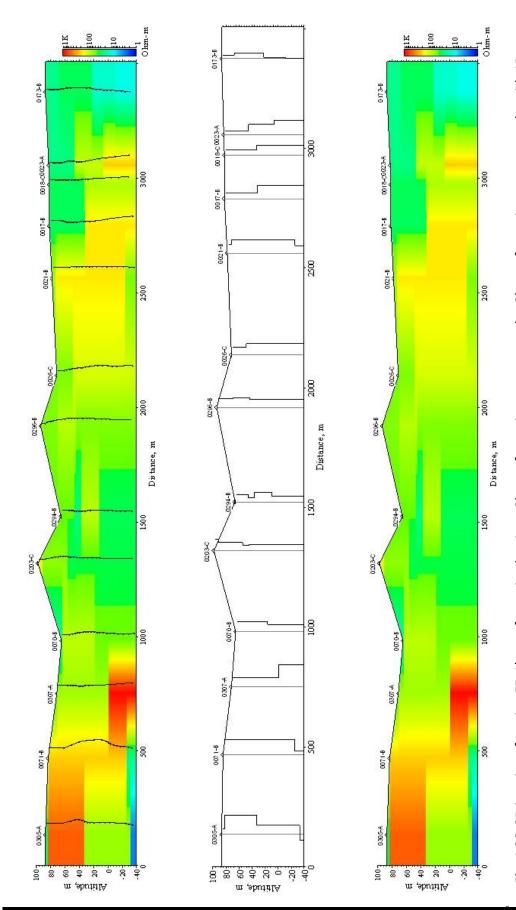
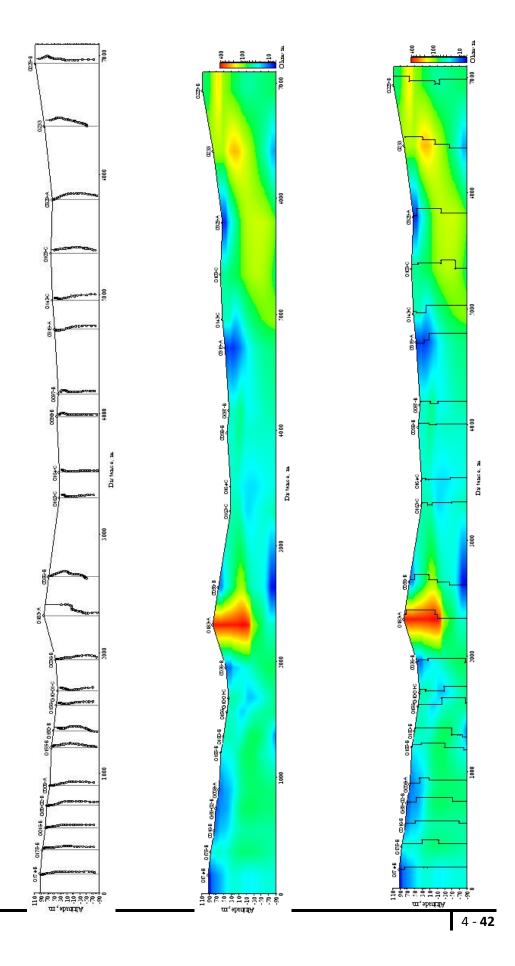
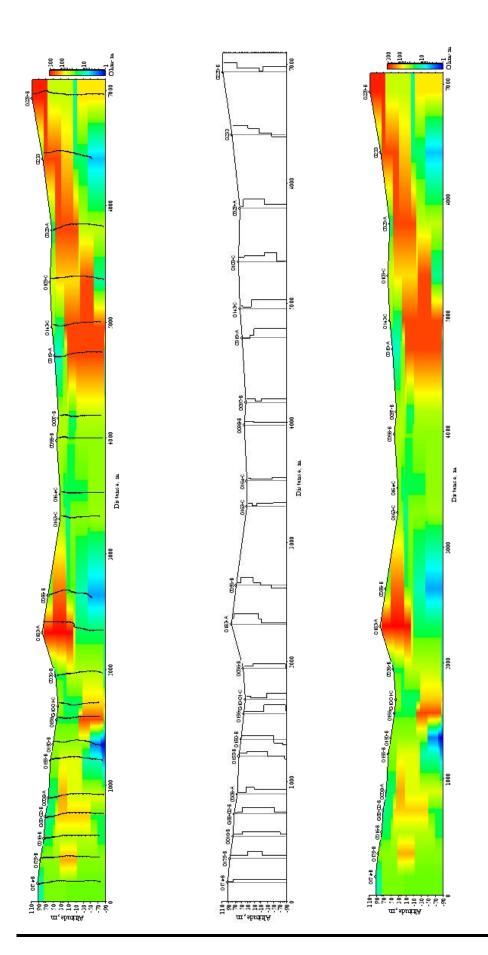
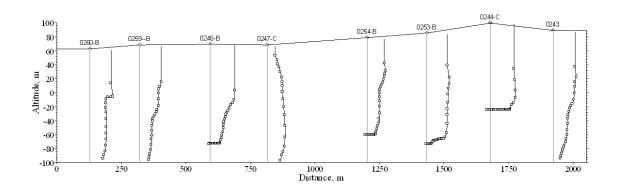


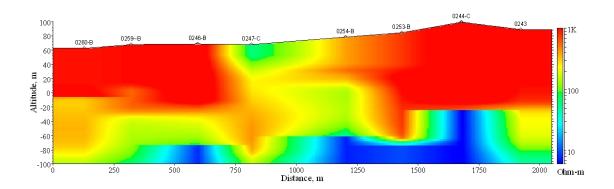
Fig. 4.36: 2D imaging of section EF: 1) transformation loggings, 2) transformation as tomography, 3) transformation as tomography with 1D inversion loggings, 4) 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, 4) 1D inversion as tomography.

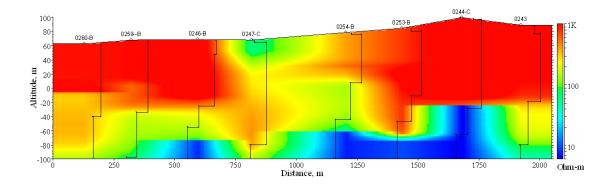


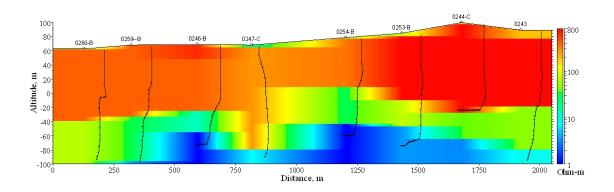


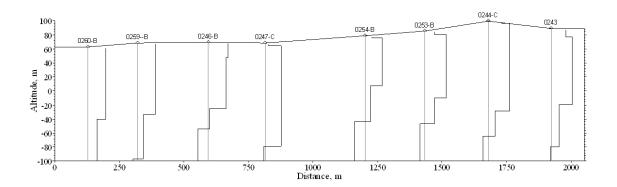
inversion loggings, 4) 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, and 6) 1D inversion as tomography. Fig. 4.37: 2D imaging of section FG: 1) transformation loggings, 2) transformation as tomography, 3) transformation as tomography with 1D

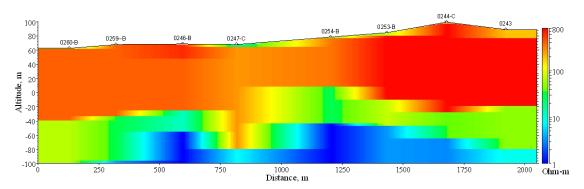












**Fig. 4.38:** 2D imaging of section HI: 1) transformation loggings, 2) transformation as tomography, 3) transformation as tomography with 1D inversion loggings, 4) 1D inversion as tomography and transformation loggings, 5) 1D inversion loggings, and 6) 1D inversion as tomography.

## 4.6.1.3.3 3D imaging of TEM data

The final 1D inverted models from all the available TEM data were finally merged to form slices differentiated with depth.

The roof and the bottom of each layer [for example see next: for layer A, roof = 0.0 m (surface) and bottom = 20.0 m (20 m deep from the ground surface)] are defined using the TEM-RES software. So, the selected layers are extracted, where each layer includes the information of the average resistivity (in Log ohm.m) of each point. For example, for layer A (0.0 - 20.0 m depth from the ground surface) for each of the 350 points an average resistivity value was extracted (for these 20 m only).

Then, all this information was inserted in a GIS environment for spatial distribution map construction (one map for each layer). Ordinary kriging interpolator was used for the construction of the spatial distribution maps of resistivity parameter as described in **section 3.4.1.5** of *Chapter 3*. Therefore, in the first place, the data were checked (by the histogram and normal QQPlots in the ArcGIS Geostatistical Analyst) if they need any transformation in order to make them more normal distributed (for perfect normal distribution pattern skewness should be 0 and kurtosis 3). So, for the resistivity of layer A, which did not show normal distribution, a log transformation has been applied to make the distribution closer to normal (Tables 4.5 & 4.6).

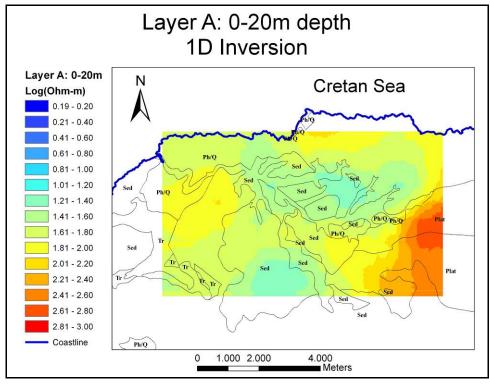
**Table 4.5:** Normal distribution check for Log ohm.m parameter (see text for explanation)

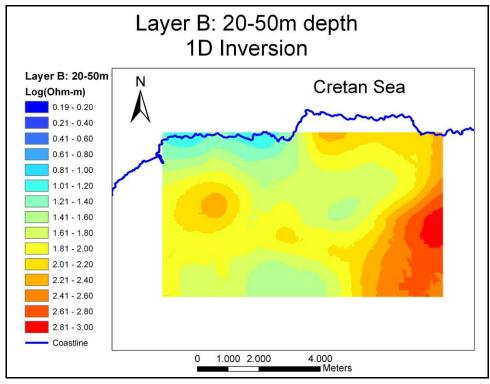
|         | Kurtosis | Skewness | Transformation |
|---------|----------|----------|----------------|
| Layer A | 4.4348   | 0.9581   | Log            |
| Layer B | 4.6666   | 0.0032   | None           |
| Layer C | 3.8425   | -0.5057  | None           |
| Layer D | 2.7532   | 0.0083   | None           |

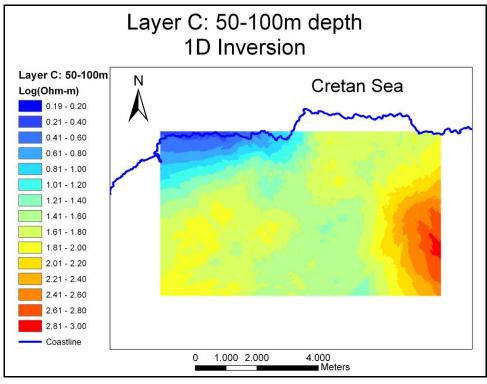
**Table 4.6** shows the semivariogram models that were chosen for each layer. For each chosen model, the standardized mean (MS) error was close to 0, the root-mean-square (RMS) error and average standard (ASE) error were as small as possible, and the Root-Mean Square Standardized (RMSS) error was close to 1.

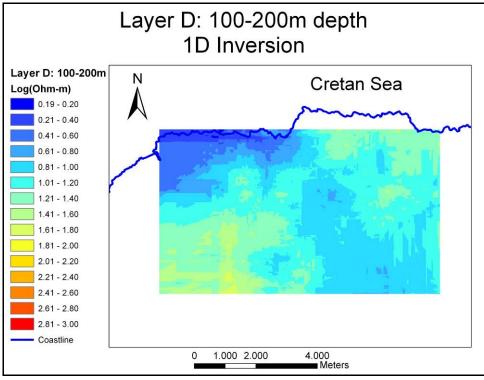
The positions of all the 350 soundings are not included in the final presented slices, in order to have clear images, but the density of the measurements (for coverage control) can be shown in previous **Figure 4.26**. The estimated model is represented as four different depth slices with depths: Layer A=0.0-20.0 m, Layer B=20.0-50.0 m, Layer C=50.0-100.0 m, and Layer D=100.0-200.0 m, respectively (**Figures 4.39a, 4.39b, 4.39c** & **4.39d**). Only for the uppermost resistivity layer A the nappes layer is superimposed, depicting the surficial geology. Note that resistivity values (ohm.m) for 3D models construction were converted into Log (ohm.m) units.

**Figures 4.41a, 4.41b, 4.41c** & **4.41d** illustrate the interpolated maps of TEM resistivity values with heights obtained by DEM. All the layers together are shown in **Figure 4.40**.







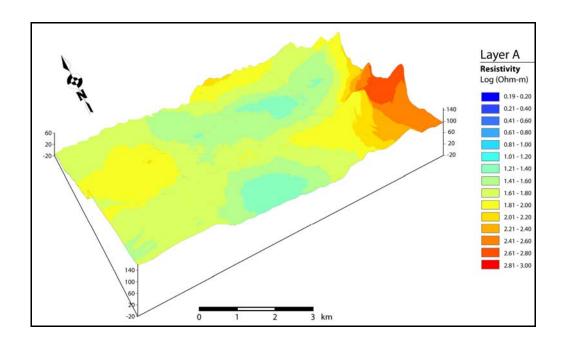


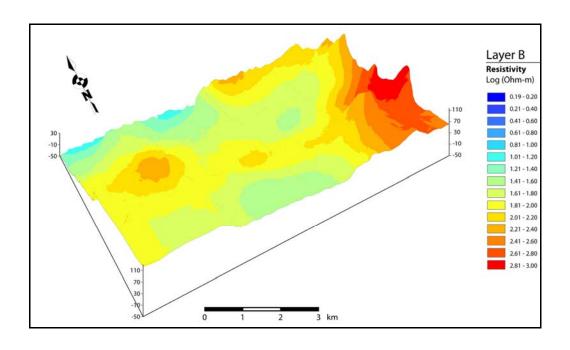
**Fig. 4.39a, 4.39b, 4.39c** & **4.39d:** 3D imaging of Resistivity data (spatial distribution map of 1D inversion results). Geoelectrical interpretation of intervals to a depth of 200 m is presented. Hot (red) colours represent high resistivity formations and the cold (blue) colours depict the low resistivity. a) Only for slice A the nappes layer is superimposed, depicting the surficial geology.

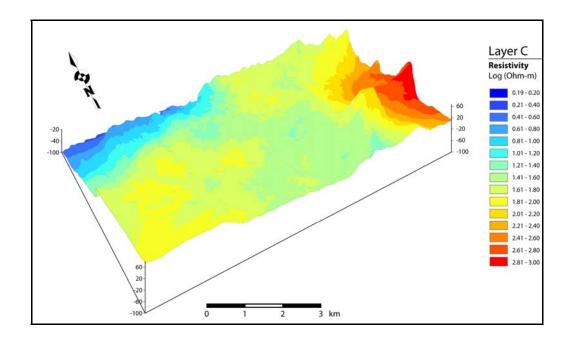
|         |       |                       |                              | Neigh               | Neighbourhood                          |                  |         |                                  | Prediction Errors                     | n Errors                     |  |
|---------|-------|-----------------------|------------------------------|---------------------|--|------------------|---------|----------------------------------|---------------------------------------|------------------------------|--|
|         | Trans | Models                | Neighbourhoods<br>to include | Include<br>at least | Shape Type                             | No of<br>Sectors | Mean    | Root-<br>Mean<br>Square<br>(RMS) | Average<br>Standard<br>Error<br>(ASE) | Mean<br>Standardized<br>(MS) | Root-Mean-<br>Square<br>Standardized<br>(RMSS) |
| Layer A | рот   | Rational<br>Quadratic | 5                            | 2                   | Neighbours in the<br>centre of Ellipse | 4                | 0.0007  | 0.2661                           | 0.3131                                | 9600:0                       | 0.8565   |
| Layer B | None  | Rational<br>Quadratic | 5                            | 2                   | Neighbours in the<br>centre of Ellipse | 8                | 0.0038  | 0.3648                           | 0.3131                                | 0.0141                       | 1.0050   |
| Layer C | None  | J-Bessel              | 5                            | 2                   | Neighbours in the<br>centre of Ellipse | 4                | 0.0026  | 0.4501                           | 0.4491                                | 0.0067                       | 1.0020   |
| Layer D | None  | Gaussian              | 5                            | 7                   | Neighbours in the centre of Ellipse    | 4                | -0.0082 | 0.5350                           | 0.5263                                | -0.0157                      | 1.0170   |

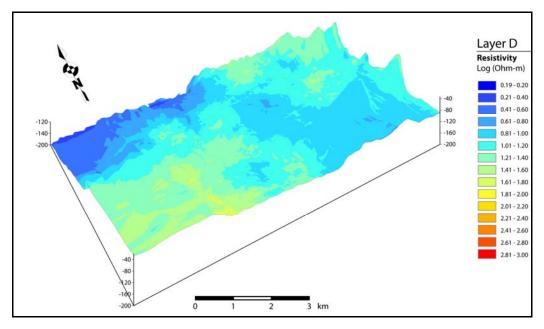
Fig.

Fig. 40: The four extracted slices A, B, C and D (interpolated maps of TEM resistivity values in different depths) as a 3D imaging









**Fig. 4.41a, 4.41b, 4.41c** & **4.41d:** The four resistivity layers (Layer A: 0 - 20 m, Layer B: 20 - 50 m, Layer C: 50 - 100 m, Layer D: 100 - 200 m) that described previously with heights obtained by DEM showing the relief of the study area

#### 4.6.2 DC resistivity method - VES technique

In addition to TEM, the VES technique was also used. A limited number of soundings took place in the study area testing different geological conditions. This section describes the fieldwork DC measurements and presents the results of the resistivity research.

#### 4.6.2.1 DC measurements in Geropotamos study area

Three VES soundings were acquired in three different sites (different geological formations): the first sounding VES-00 on dolomitic limestones (Plattenkalk series), the second VES-01 on Neogene sediments, and the last VES-02 near the boundary between phyllite/quartzite nappe and Neogene sediments. For the two of them (VES-01 and VES-02), multidirectional measurements were also acquired since the structure is more complex than a 1D model that VES technique is able to model (Kalisperi et al, 2008). Moreover, for VES-01 and VES-02 two short TEM profiles (A and B) were acquired, crossing through the centres of VES-01 ans VES-02 soundings respectively, just for direct comparison between the two methods. For these particular TEM soundings (comprising the A and B profiles) 25x25 m loop was used, for better resolution of the shallow depth.

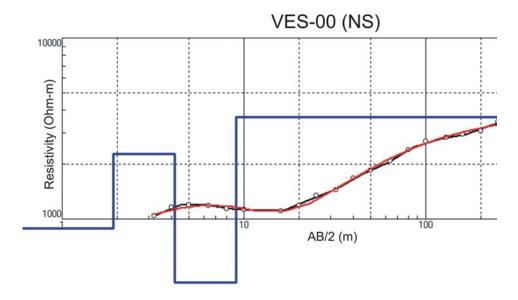
#### 4.6.2.2 Processing, Analysis & 1D Modelling

IPI2Win v.2.1 software by Geoscan-M Ltd was the tool for data processing of VES data. It is designed for processing vertical electrical sounding and/or induced polarization data curves 1D interpretation.

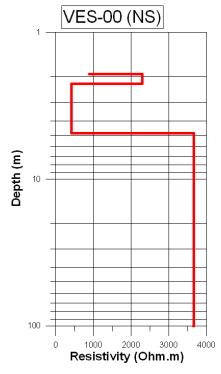
### VES-00

The first VES sounding, VES-00, took place on the dolomitic limestones at the eastern part of the study area (**Fig. 4.42**) at Maniaki site. As described in **section 4.6.1.2** of this chapter, SPM effect influenced TEM method to have reliable results, so only resistivity data are finally

available from this site. Concerning VES, only NS measurements were acquired for this location, because there was not enough space in the other direction (WE).



**Fig. 4.42a:** Curve of apparent resistivity of VES-00 (NS) and 1D inversion model after processing and modelling by IPI2Win software

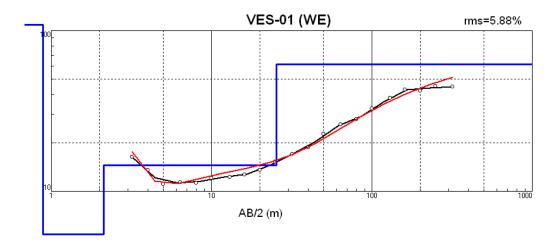


| Depth | Resistivity |
|-------|-------------|
| (m)   | (ohm.m)     |
| 1.92  | 890         |
| 2.24  | 2293        |
| 4.87  | 416         |
|       | 3658        |

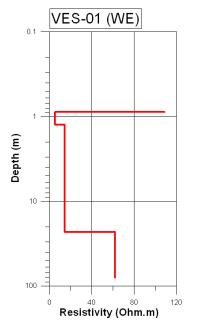
Fig. 4.42b: 1D inversion model of VES-00 (NS)

#### **VES-01**

The second VES sounding, VES-01, was carried out at the southern part of the study area on Neogene sediments, which consisted mainly of Neogene limestones. Multidirectional measurements acquired in both directions (NS and WE). The resistivity curves and resulted 1D models for the same location, but using different directions are shown in **Figures 4.43** & **4.44.** The 1D resistivity models were almost identical.

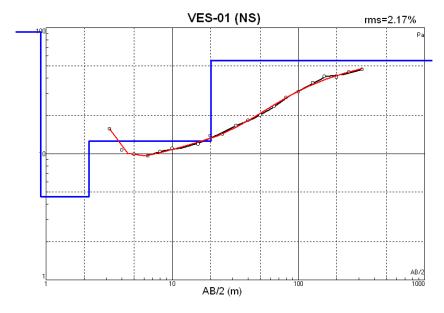


**Fig. 4.43a:** Curve of apparent resistivity 1D inversion model (WE) after processing and modelling by IPI2Win software

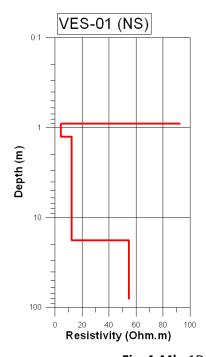


| Depth | Resistivity |  |  |  |
|-------|-------------|--|--|--|
| (m)   | (ohm.m)     |  |  |  |
| 0.887 | 109         |  |  |  |
| 1.25  | 5.39        |  |  |  |
| 23.1  | 14.5        |  |  |  |
|       | 62          |  |  |  |

Fig. 4.43b: 1D inversion model of VES-01 (WE)



**Fig. 4.44a:** Curve of apparent resistivity and 1D inversion model (NS) after processing and modelling by IPI2Win software

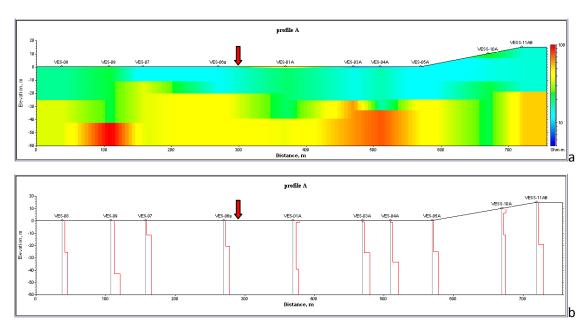


| Depth | Resistivity |
|-------|-------------|
| (m)   | (ohm.m)     |
| 0.909 | 92.4        |
| 1.27  | 4.57        |
| 18    | 12.6        |
|       | 54.8        |

Fig. 4.44b: 1D inversion model of VES-01 (NS)

## VES-01 with TEM profile A

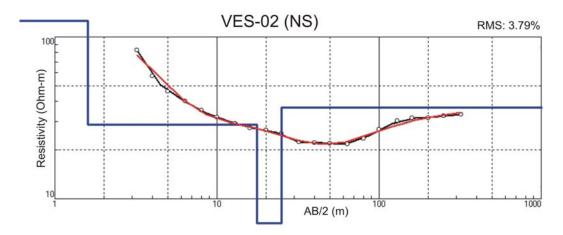
TEM profile A had WE direction and crossed the VES-01 sounding about in the middle (red arrow in Figs. 4.45a & 4.45b). It was 500m long and consisted of 10 TEM soundings (approximately 50m distance to each other) (Figs. 4.45a & 4.45b).



**Fig. 4.45**: TEM Profile A: TEM resistivity tomography with 2x exaggeration (distance to elevation ratio). Red arrow indicates the exact position of VES-01.

#### **VES-02**

The last of the three VES soundings, VES-02, took place in the central part of the area, near the contact between phyllite/quartzite unit and Neogene sediments. Multidirectional measurements acquired in both directions (NS and WE). This sharp change in the experimental curve of VES-02 (EW), as it is shown in **Figure 4.47a**, is usually correlated with tectonic features (faults or tectonic geological contacts).



**Fig. 4.46a:** Curve of apparent resistivity and 1D inversion (NS) after processing and modelling by IPI2Win software

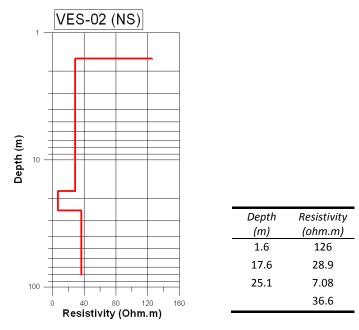
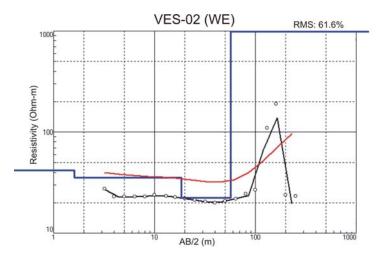


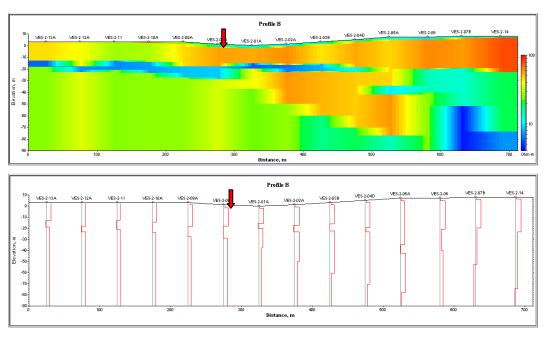
Fig. 4.46b: 1D inversion model of VES-02 (NS)



**Fig. 4.47:** Curves of apparent resistivity and 1D inversion model (WE). The sharp change in the experimental curve of VES-02 (EW), as it is shown, is usually correlated with tectonic features (faults or tectonic geological contacts)

## - VES-02 with TEM profile B

TEM profile B had WE direction too, and crossed VES-02 sounding about in the middle, like profile A did to VES-01 (red arrow in Figs. 4.48a & 4.48b). It was 700m long, i.e. longer than profile A, and consisted of 14 TEM soundings (approximately 50m distance to each other) (Figs. 4.48a & 4.48b).



**Fig. 4.48**: TEM Profile B: TEM resistivity tomography with 1.7x exaggeration (distance to elevation ratio). Red arrow indicates the exact position of VES-02.

#### 4.7 Geochemical Analyses

Along with the geophysical data (TEM and VES soundings), groundwater chemistry data were obtained in this study in order to check the quality of the waters and to test the hypotheses of evaporite domes or seawater intrusion in the area (section 2.4, *Chapter 2*). Three water samplings took place during 2008: a) first days of June, b) end of July, and c) first day of October, that is to say approximately every 2 months. Especially, the summer period was chosen for sampling as it is the dry period and high pumping rates for water supply take place (irrigation season). May is actually the month when generally the rainfalls stop in Crete, and October is the beginning of the wet period. So, in the case of the seawater intrusion problem in Geropotamos study area, of the worst groundwater quality would be expected to be found in the October samples.

As already described in *Chapter 3*, 16 chemical parameters were measured in the frame of this thesis (**Table 3.4** of **section 3.3**). The first water sampling (June 2008) was a pilot study of 10 samples. More comprehensive analysis was undertaken of 24 locations in July and October 2008 (**Table 4.7**). Alkalinity, nitrate, Boron and phosphate measured only once for October's sampling.





**Fig. 4.49: a)** & **b)** During October's water sampling, G-55 sample location, and G-09 sample location respectively.

Municipality of Geropotamos offered both financial and human support for the water sampling and chemical analyses of the study area's groundwaters. In the three water samplings, Mr. Stefanakis Manolis and Mr. Moschonas Dimitris, employers at Municipality of

Geropotamos, were participated, while the chemical analyses were financially supported by the same source.

All the chemical analyses took place in Laboratory of Environmental Chemistry and Biochemical Processes of TEI of Crete (Branch of Chania) in collaboration with Dr. Nikolaos Lydakis.

## 4.7.1 Results of Chemical Analyses

The chemical parameters measured may potentially originate either from natural sources or from anthropogenic activity. For example,  $Ca^{2+}$  and  $Mg^{2+}$  may originate mainly from the weathering of several mineral deposits like limestone or dolomites etc;  $SO_4^{2-}$  can come from dissolution of gypsum and other mineral deposits containing this ion;  $Na^+$  and  $Cl^-$  can originate from evaporites (i.e. halites) or groundwaters which have been affected by seawater intrusion or by agricultural or irrigation discharges;  $NO_3^-$  and  $PO_4^{3-}$  may come from the extensive use of fertilizers. Boron was also measured as a quality parameter of water. Its origin can be correlated mainly with anthropogenic activities. As will be shown, the concentrations of  $K^+$  and  $Fe^{2+}$  were generally small in our samples and may originate from several rock formations in the area. Alkalinity values are correlated with the bicarbonate ( $HCO_3^-$ ) content of the waters. The rest of the measured parameters (total hardness, electrical conductivity, total dissolved solids, and salinity) have values which are strongly related with the values of the abovementioned parameters, whereas pH and temperature were also measured.

In this section, all the geochemical results are presented separately. For each parameter there is a column graph with all the results and two tables of statistical analysis, (using OriginPro 7.5 software). The first table has the statistical analysis of each parameter for all the samplings (June, July, October 2008), while the second table has the statistical analysis for the same 10 samples of each parameter for all the samplings (June, July, October 2008), for direct comparison. In addition, for each parameter of July's and October's samplings a spatial distribution map has been created.

**Table 4.7:** Chemical parameters that were measured in Geropotamos study area for all the samplings. June's sampling was a pilot sampling and samples were collected only from 10 of 24 sample points: G-01, G-05, G-06, G-09, G-50, G-53, G-80, G-81, Sweet Spr., and Salty Spr.

|            | Pł         |          | l & Ag<br>operti           |          | te          |          | ŗ        | Иetal    | S        |          | Inc      | organi   | ic Nor   | nmetallio       | Constit                       | uents                         |
|------------|------------|----------|----------------------------|----------|-------------|----------|----------|----------|----------|----------|----------|----------|----------|-----------------|-------------------------------|-------------------------------|
|            | Alkalinity | Hardness | Electrical<br>Conductivity | Salinity | Temperature | Ca       | Mg       | К        | Na       | Fe       | В        | Cl       | pH value | NO <sub>3</sub> | SO <sub>4</sub> <sup>2-</sup> | PO <sub>4</sub> <sup>3-</sup> |
| 04/06/2008 |            | <b>√</b> | <b>√</b>                   | <b>√</b> | <b>√</b>    | <b>✓</b> | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b> |          | <b>√</b> | <b>√</b> |                 | <b>√</b>                      |                               |
| 28/07/2008 |            | <b>√</b> | <b>√</b>                   | <b>√</b> | <b>√</b>    | <b>√</b> | <b>✓</b> | <b>√</b> | <b>√</b> | <b>√</b> |          | <b>√</b> | <b>√</b> |                 | <b>√</b>                      |                               |
| 01/10/2008 | <b>√</b>   | <b>√</b> | <b>√</b>                   | <b>√</b> | <b>√</b>    | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b> | <b>√</b>        | <b>√</b>                      | <b>√</b>                      |

#### 4.7.1.1 Spatial Interpolation of geochemical parameters

For spatial interpolation maps of the geochemical data, the same steps that were followed for 3D resistivity maps construction (section 4.6.1.3.3 of this chapter), were followed again, as already described in section 3.4.1.5 of *Chapter 3*. Therefore, initially the data were checked (by the histogram and normal QQPlots in the ArcGIS Geostatistical Analyst) to see if they need any transformation in order to make them more normally distributed (for perfect normal distribution pattern skewness should be 0 and kurtosis 3). So, for those parameters which did not show normal distribution, a Log transformation has been applied to make the distribution closer to normal (Tables 4.8 & 4.9).

This type of map was produced for July's and October's samplings (24 sample locations), but not for June's data, as only 10 sample locations were available. Ten samples is a very low number for spatial distribution map construction and the results may not give a fully representative indication of the geochemical patterns.

**Table 4.8:** Normal distribution check for July's Sampling

| Parameters     | Kurtosis | Skewness  | Transf |
|----------------|----------|-----------|--------|
| Total Hardness | 2.6299   | -0.076156 | None   |
| Conductivity   | 5.6143   | 1.7729    | Log    |
| TDS            | 5.6143   | 1.7729    | Log    |
| Salinity       | 5.852    | 1.8414    | Log    |
| Temperature    | 3.8007   | 0.10974   | Log    |
| Ca             | 2.7775   | 0.61909   | None   |
| Mg             | 3.419    | 1.0233    | Log    |
| K              | 7.8473   | 2.4141    | Log    |
| Na             | 5.7435   | 1.8419    | Log    |
| CI-            | 6.0602   | 1.9098    | Log    |
| pH-value       | 2.4309   | 0.47287   | None   |
| SO4            | 6.5924   | 2.1263    | Log    |

**Table 4.9**: Normal distribution check for October's sampling

| Parameters     | Kurtosis | Skewness | Transf |
|----------------|----------|----------|--------|
| Alkalinity     | 2.721    | 0.16802  | None   |
| Total Hardness | 5.1693   | 1.2916   | Log    |
| Conductivity   | 6.1829   | 1.7823   | Log    |
| TDS            | 6.1829   | 1.7823   | Log    |
| Salinity       | 6.5541   | 1.8711   | Log    |
| Temperature    | 3.746    | 0.4074   | Log    |
| Ca             | 3.1731   | 0.8026   | Log    |
| Mg             | 2.6117   | 0.62697  | None   |
| K              | 9.9119   | 2.6254   | Log    |
| Na             | 6.9023   | 1.9591   | Log    |
| Cl-            | 6.6064   | 1.8983   | Log    |
| pH-value       | 2.222    | 0.42177  | None   |
| NO3            | 8.0327   | 2.2092   | Log    |
| SO4            | 5.5126   | 1.7189   | Log    |

**Tables 4.10** & **4.11**: show the semivariogram models that were chosen for each parameter data set (July and October). That chosen model the standardized mean (MS) error was close to 0, the root-mean-square (RMS) error and average standard (ASE) error were as small as possible, and the Root-Mean Square Standardized (RMSS) error was close to 1.

Table 4.10 Fitted parameters of the theoretical variogram model for groundwater quality parameters (July's sampling)

|              |       |                    |                | Neigh    | Neighbourhood                          |         |          |         | Prediction Errors | Errors       |              |
|--------------|-------|--------------------|----------------|----------|--|---------|----------|---------|-------------------|--------------|--------------|
|              |       |                    |                |          |  |         |          | Root-   | Average           | 9000         | Root-Mean-   |
| Parameters   | Trans | Models             | Neighbourhoods | Include  | Chana Tuna                             | No of   | Moon     | Mean    | Standard          | Standardized | Square       |
|              |       |                    | to include     | at least | aldha i Aha                            | Sectors | NEG      | Square  | Error             | (MS)         | Standardized |
| Total        |       |                    |                |          |  |         |          | (CIMIN) | (ASE)             |              | (SCIMIN)     |
| Hardness     | None  | Rational Quadratic | 5              | 2        | One Sector                             | 1       | 15.11    | 126.6   | 127.2             | 0.1103       | 1.005        |
| Conductivity | Log   | K-Bessel           | 5              | 2        | Neighbours in the<br>centre of Ellipse | 4       | -20.45   | 151.5   | 1480              | -0.04312     | 1.02         |
| TDS          | Log   | K-Bessel           | 5              | 2        | Neighbours in the<br>centre of Ellipse | 4       | -13,48   | 984.2   | 961.2             | -0.04323     | 1.02         |
| Salinity     | Log   | K-Bessel           | 5              | 2        | Neighbours in the<br>centre of Ellipse | 4       | -0.01186 | 0.7447  | 0.7439            | -0.04684     | 1.004        |
| Temperature  | Fog   | Exponential        | 5              | 2        | One Sector                             | 1       | -0.05101 | 0.7776  | 0.6214            | -0.04638     | 1.003        |
| Ca           | None  | J-Bessel           | 5              | 2        | One Sector                             | 1       | 0.64     | 24.38   | 24.38             | 0.02987      | 1.003        |
| Mg           | Log   | K-Bessel           | 5              | 2        | Neighbours in the<br>centre of Ellipse | 4       | 0.3196   | 28.97   | 32.65             | -0.04515     | 1.017        |
| К            | Log   | Rational Quadratic | 5              | 2        | Neighbours in the<br>centre of Ellipse | 80      | 0.01004  | 8.33    | 10.9              | -0.03795     | 0.8496       |
| Na           | Log   | Pentaspherical     | 5              | 2        | Neighbours in the<br>centre of Ellipse | 8       | 2.737    | 158.2   | 214.4             | -0.06087     | 0.8972       |
| Cl-          | Log   | Hole Effect        | 2              | 2        | One Sector                             | 1       | 3.378    | 568.7   | 947.7             | -0.0833      | 0.9105       |
| pH-value     | None  | Hole Effect        | 2              | 2        | One Sector                             | 1       | 0.04827  | 0.303   | 0.32              | 0.1425       | 0.9884       |
| 504          | Log   | J-Bessel           | 5              | 2        | Neighbours in the<br>centre of Ellipse | 4       | -5.948   | 96.91   | 93.04             | -0.07198     | 1.019        |

Table 4.11 Fitted parameters of the theoretical variogram model for groundwater quality parameters (October's sampling)

|                |       |                       |                              | Neigh               | Neighbourhood                       |                  |           |                              | Prediction Errors                  | n Errors                     |  |
|----------------|-------|-----------------------|------------------------------|---------------------|-------------------------------------|------------------|-----------|------------------------------|------------------------------------|------------------------------|--|
| Parameters     | Trans | Models                | Neighbourhoods<br>to include | Include<br>at least | Shape Type                          | No of<br>Sectors | Mean      | Root-Mean<br>Square<br>(RMS) | Average<br>Standard<br>Error (ASE) | Mean<br>Standardized<br>(MS) | Root-Mean-Square<br>Standardized<br>(RMSS) |
| Alkalinity     | None  | J-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | -1.304    | 50.92                        | 53.72                              | -0.01732                     | 0.942                                      |
| Total Hardness | Log   | K-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | 0.5655    | 208.3                        | 185.3                              | -0.02084                     | 1.117                                      |
| Conductivity   | Log   | K-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | -4.273    | 1487                         | 1473                               | 86980'0-                     | 1.041                                      |
| TDS            | Log   | K-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | 2.834     | 966.3                        | 1.726                              | -0.03705                     | 1.041                                      |
| Salinity       | Log   | K-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | -0.003683 | 0.7306                       | 0.7377                             | -0.04112                     | 1.03                                       |
| Temperature    | Log   | Exponential           | 5                            | 2                   | One sector                          | 1                | -0.07549  | 0.9456                       | 0.6567                             | -0.06921                     | 1.205                                      |
| Са             | Log   | J-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | 0.4111    | 26.76                        | 29.29                              | 0.003981                     | 0.9407                                     |
| Mg             | None  | J-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 8                | 0.3646    | 26.39                        | 23.05                              | 0.009216                     | 1.129                                      |
| ×              | Log   | Rational<br>Quadratic | 5                            | 2                   | One sector                          | 1                | 0.1054    | 6.529                        | 8.186                              | -0.03781                     | 0.9545                                     |
| Na             | Log   | J-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | 6.532     | 334.6                        | 430.1                              | -0.08099                     | 0.9725                                     |
| 8              | Log   | Pentaspherical        | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | 0.0006169 | 0.05808                      | 0.05461                            | -0.03176                     | 1.009                                      |
| -tö            | Log   | Hole Effect           | 5                            | 2                   | One sector                          | 1                | 9.924     | 535.9                        | 771                                | -0.08637                     | 1.008                                      |
| pH-value       | None  | Stable                | 5                            | 2                   | Neighbours in the centre of Ellipse | 4                | -0.004946 | 0.2332                       | 0.2356                             | -0.02171                     | 0.9938                                     |
| NO3            | Log   | Rational<br>Quadratic | 5                            | 2                   | One sector                          | 1                | -0.2039   | 3.774                        | 3.13                               | -0.1272                      | 1.261                                      |
| 804            | Log   | K-Bessel              | 5                            | 2                   | Neighbours in the centre of Ellipse | 8                | -1.395    | 99.79                        | 97.15                              | -0.0554                      | 1.026                                      |

### 4.7.1.2 Physical and Aggregate Properties

Total alkalinity and bicarbonate concentration, total hardness, electrical conductivity and TDS, salinity, and temperature belong in physical and aggregate properties, as already mentioned on **section 3.3.2** of *Chapter 3*. Column graphs, tables of statistics and prediction maps of those parameters for the three samplings (June, July, October 2008) are following.

# **4.7.1.2.1** Alkalinity (expressed as mg $CaCO_3/L$ ) and Bicarbonate concentration (as mg $HCO_3^-/L$ )

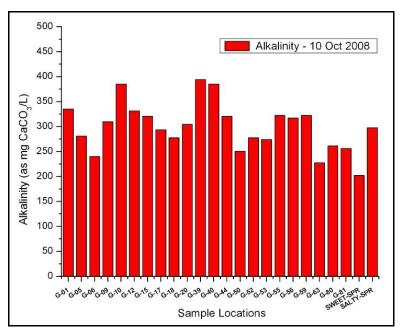


Fig. 4.50: Column graph of alkalinity expressed as  $mg\ CaCO_3/L$  for October's 2008 sampling

**Table 4.12:** Statistical analysis of alkalinity expressed as  $mg\ CaCO_3/L$  for October's 2008 sampling

| DATE               | 01/10/2008 |
|--------------------|------------|
| Number of Samples  | 24         |
| Mean               | 299.6      |
| Standard Deviation | 48.51      |
| Standard Error     | 9.901      |
| Minimum Value      | 202.5      |
| Maximum Value      | 394.2      |
| Median             | 301.0      |
| Kurtosis           | -0.049     |

As described in section **3.3.2.1** of *Chapter 3*, it was necessary to convert bicarbonate ion concentration (expressed as  $mg\ CaCO_3/L$ ) to bicarbonate ion activity (in  $mg\ HCO_3^*/L$ ). The results are presented next.

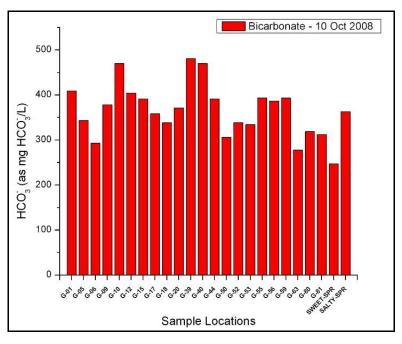


Fig. 4.51: Column graph of bicarbonate (as  $mg\ HCO_3/L)$  for October's 2008 sampling

**Table 4.13:** Statistical analysis of bicarbonate (as  $mg\ HCO_3/L$ ) for October's 2008 sampling

| DATE               | 01/10/2008 |
|--------------------|------------|
| Number of Samples  | 24         |
| Mean               | 365.5      |
| Standard Deviation | 59.18      |
| Standard Error     | 12.08      |
| Minimum Value      | 247.0      |
| Maximum Value      | 480.9      |
| Median             | 367.3      |
| Kurtosis           | -0.049     |

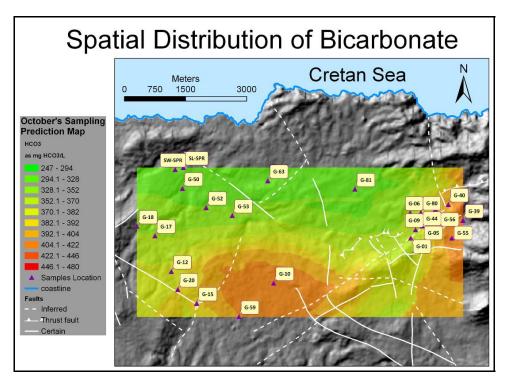


Fig. 4.52: Spatial distribution map of bicarbonate (as  $mg\ HCO_3/L$ ) for October's 2008 sampling

## **4.7.1.2.2** Total Hardness (expressed as mg CaCO<sub>3</sub>/L)

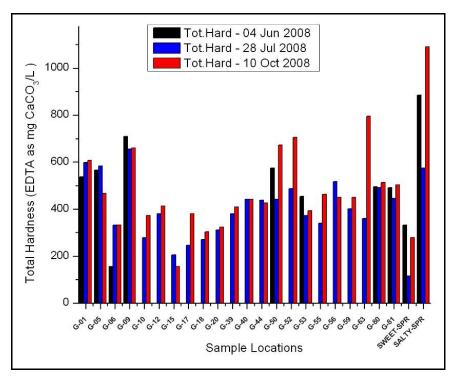


Fig. 4.53: Column graph of total hardness (expressed as  $mg\ CaCO_3/L)$  for all the samplings (June, July, October 2008)

**Table 4.14**: Statistical analysis of total Hardness (expressed as mg CaCO<sub>3</sub>/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 520.3      | 403.3      | 483.9      |
| Standard Deviation | 196.7      | 131.8      | 195.3      |
| Standard Error     | 62.21      | 26.90      | 39.86      |
| Minimum Value      | 155.8      | 114.8      | 155.8      |
| Maximum Value      | 885.6      | 656.0      | 1090.6     |
| Median             | 516.6      | 391.6      | 446.9      |
| Kurtosis           | 1.201      | -0.162     | 2.998      |

**Table 4.15**: Statistical analysis of total Hardness for the same 10 samples only (expressed as  $mg\ CaCO_3/L$ ) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 520.3      | 461.4      | 551.9      |
| Standard Deviation | 196.7      | 160.1      | 230.5      |
| Standard Error     | 62.21      | 50.62      | 72.90      |
| Minimum Value      | 155.8      | 114.8      | 278.8      |
| Maximum Value      | 885.6      | 656.0      | 1090.6     |
| Median             | 516.6      | 469.5      | 508.4      |
| Kurtosis           | 1.201      | 1.298      | 2.859      |

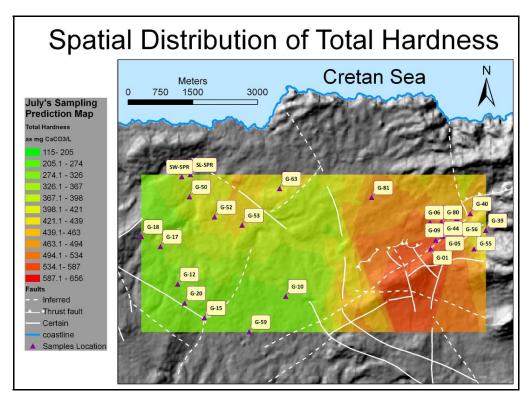
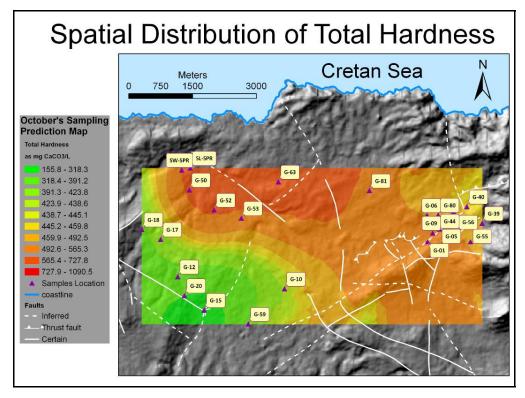
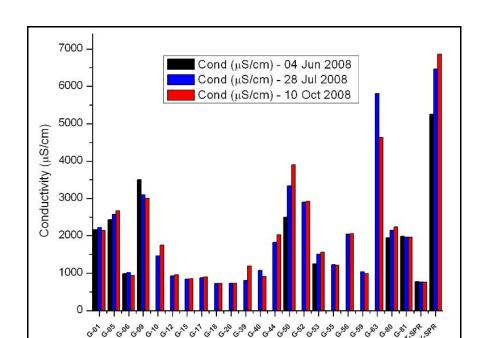


Fig. 4.54: Spatial distribution map of total hardness (expressed as  $mg\ CaCO_3/L$ ) for July's 2008 sampling



**Fig. 4.55:** Spatial distribution map of total hardness (expressed as  $mg\ CaCO_3/L$ ) for October's 2008 sampling



## 4.7.1.2.3 Electrical Conductivity (EC) and Total Dissolved Solids (TDS)

Fig. 4.56: Column graph of electrical conductivity (as  $\mu S/cm$ ) for all the samplings (June, July, October 2008)

Sample Locations

**Table 4.16:** Statistical analysis of electrical conductivity (as  $\mu S/cm$ ) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 2281       | 1976       | 1995       |
| Standard Deviation | 1315       | 1511       | 1472       |
| Standard Error     | 416        | 308        | 301        |
| Minimum Value      | 776        | 726        | 721        |
| Maximum Value      | 5250       | 6470       | 6860       |
| Median             | 2080       | 1490       | 1655       |
| Kurtosis           | 2.15       | 3.55       | 4.26       |

**Table 4.17:** Statistical analysis of electrical conductivity for the same 10 samples (as  $\mu S/cm$ ) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 2281       | 2510       | 2603       |
| Standard Deviation | 1315       | 1617       | 1764       |
| Standard Error     | 416        | 511        | 558        |
| Minimum Value      | 776        | 767        | 757        |
| Maximum Value      | 5250       | 6470       | 6860       |
| Median             | 2080       | 2185       | 2190       |
| Kurtosis           | 2.15       | 4.02       | 3.59       |

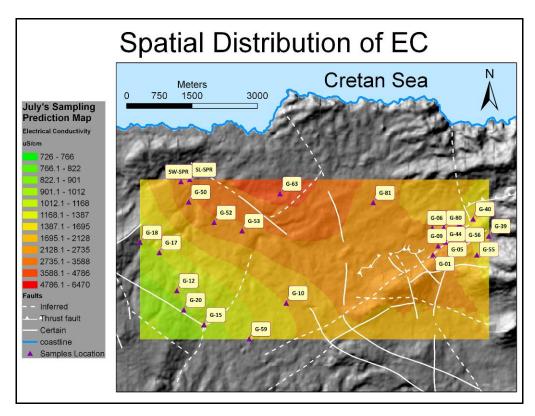


Fig. 4.57: Spatial distribution map of electrical conductivity ( $\mu S/cm$ ) for July's 2008 sampling

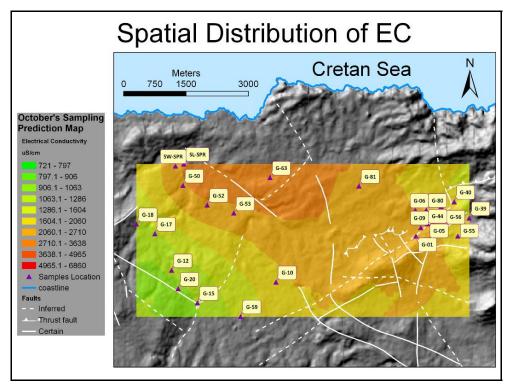
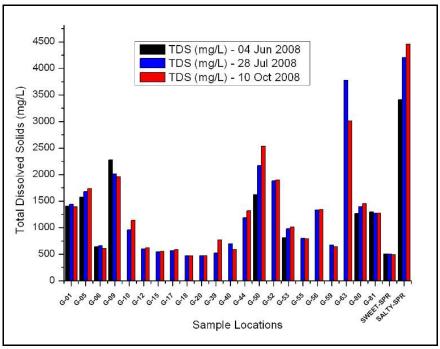


Fig. 4.58: Spatial distribution map of electrical conductivity ( $\mu S/cm$ ) for October's 2008 sampling

As described in section **3.3.2.3** of *Chapter 3*, the electrical conductivity can be roughly converted into TDS (expressed as mg/L). The results are presented next.



**Fig. 4.59:** Column graph of TDS (as mg/L) for all the samplings (June, July, October 2008)

Table 4.18: Statistical analysis of TDS (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 1482       | 1284       | 1297       |
| Standard Deviation | 855        | 982        | 957        |
| Standard Error     | 270        | 201        | 195        |
| Minimum Value      | 504        | 472        | 469        |
| Maximum Value      | 3412       | 4205       | 4459       |
| Median             | 1352       | 968        | 1076       |
| Kurtosis           | 2.15       | 3.55       | 4.26       |

**Table 4.19:** Statistical analysis of TDS for the same 10 samples (as  $\mu S/cm$ ) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 1482       | 1632       | 1692       |
| Standard Deviation | 855        | 1050       | 1146       |
| Standard Error     | 270        | 332        | 363        |
| Minimum Value      | 504        | 499        | 492        |
| Maximum Value      | 3412       | 4205       | 4459       |
| Median             | 1352       | 1420       | 1424       |
| Kurtosis           | 2.15       | 4.02       | 3.59       |

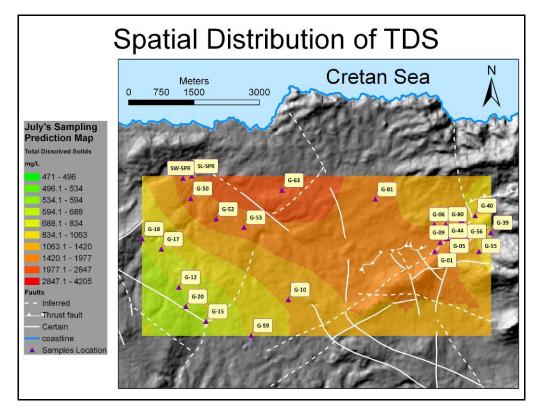


Fig. 4.60: Spatial distribution map of TDS (as mg/L) for July's 2008 sampling

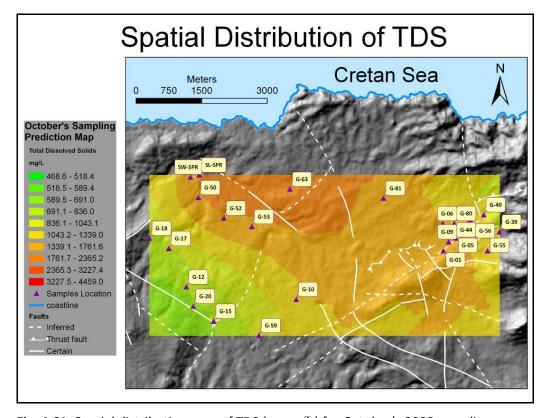


Fig. 4.61: Spatial distribution map of TDS (as mg/L) for October's 2008 sampling

# 4.7.1.2.4 Salinity

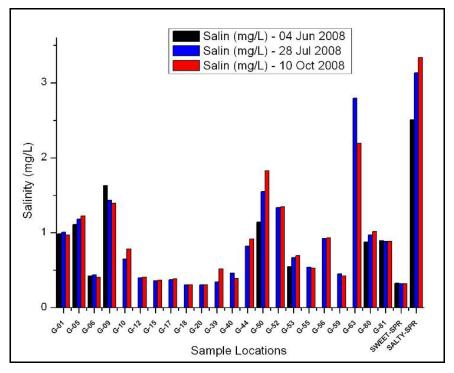


Fig. 4.62: Column graph of salinity (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.20:** Statistical analysis of salinity (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 1.0        | 0.9        | 0.9        |
| Standard Deviation | 0.6        | 0.7        | 0.7        |
| Standard Error     | 0.2        | 0.2        | 0.1        |
| Minimum Value      | 0.3        | 0.3        | 0.3        |
| Maximum Value      | 2.5        | 3.1        | 3.3        |
| Median             | 0.9        | 0.7        | 0.7        |
| Kurtosis           | 2.4        | 3.8        | 4.7        |

**Table 4.21:** Statistical analysis of salinity for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 1.0        | 1.2        | 1.2        |
| Standard Deviation | 0.6        | 0.8        | 0.9        |
| Standard Error     | 0.2        | 0.3        | 0.3        |
| Minimum Value      | 0.3        | 0.3        | 0.3        |
| Maximum Value      | 2.5        | 3.1        | 3.3        |
| Median             | 0.9        | 1          | 1          |
| Kurtosis           | 2.4        | 4.3        | 3.9        |

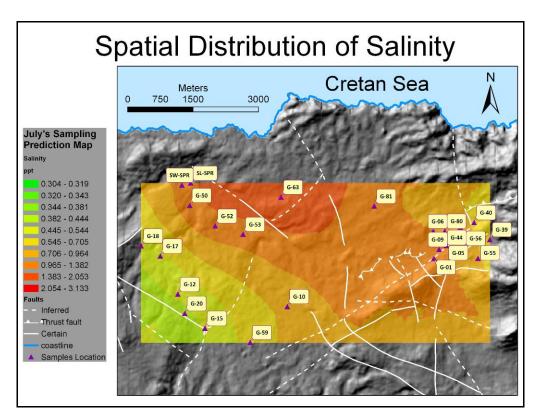


Fig. 4.63: Spatial distribution map of salinity (as mg/L) for July's 2008 sampling

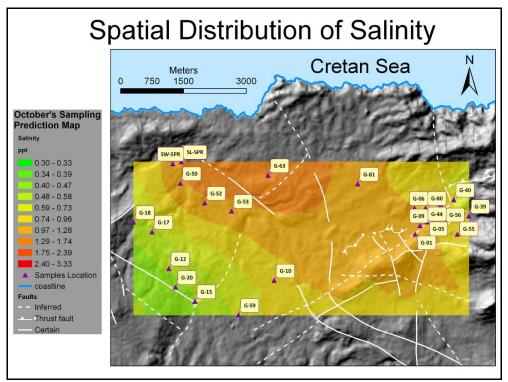
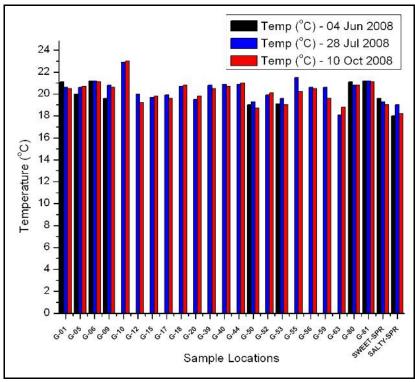


Fig. 4.64: Spatial distribution map of salinity (as mg/L) for October's 2008 sampling

## **4.7.1.2.5 Temperature (**in °C)



**Fig. 4.65:** Column graph of temperature (°C) for all the samplings (June, July, October 2008)

**Table 4.22:** Statistical analysis of temperature (°C) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 19.9       | 20.4       | 20.1       |
| Standard Deviation | 1.13       | 0.98       | 1.04       |
| Standard Error     | 0.36       | 0.20       | 0.21       |
| Minimum Value      | 18.0       | 18.1       | 18.2       |
| Maximum Value      | 21.2       | 22.9       | 23.0       |
| Median             | 19.8       | 20.6       | 20.4       |
| Kurtosis           | -1.00      | 1.29       | 1.23       |

**Table 4.23:** Statistical analysis of temperature for the same 10 samples (°C) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 19.9       | 20.2       | 19.9       |
| Standard Deviation | 1.13       | 0.85       | 1.11       |
| Standard Error     | 0.36       | 0.27       | 0.35       |
| Minimum Value      | 18.0       | 19.0       | 18.2       |
| Maximum Value      | 21.2       | 21.2       | 21.1       |
| Median             | 19.8       | 20.6       | 20.6       |
| Kurtosis           | -1.00      | -1.78      | -1.68      |

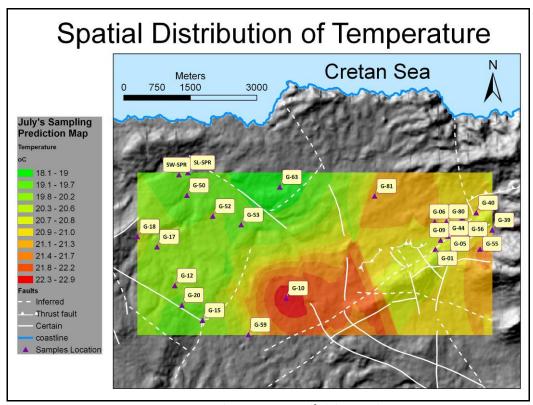


Fig. 4.66: Spatial distribution map of temperature (°C) for July's 2008 sampling

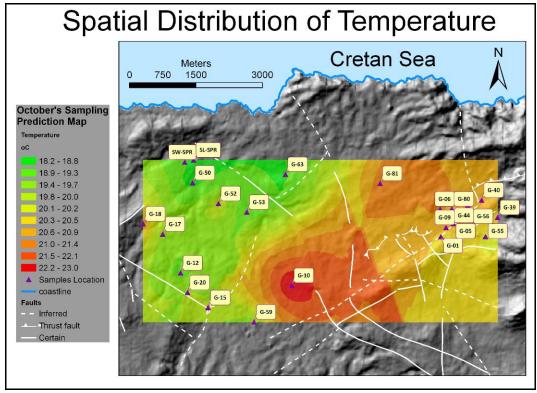


Fig. 4.67: Spatial distribution map of temperature (°C) for October's 2008 sampling

## 4.7.1.3 Metals

## 4.7.1.3.1 Calcium (Ca)

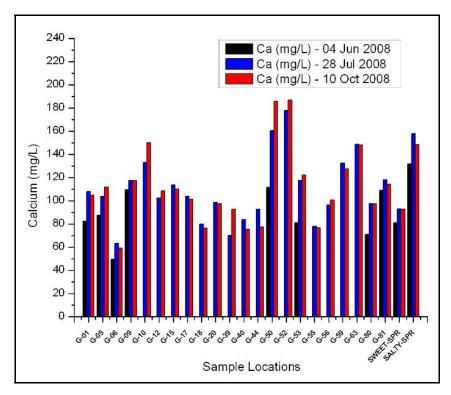


Fig. 4.68: Column graph of calcium (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.24:** Statistical analysis of calcium (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 91.48      | 110.42     | 111.84     |
| Standard Deviation | 23.99      | 29.31      | 32.83      |
| Standard Error     | 7.587      | 5.982      | 6.702      |
| Minimum Value      | 49.50      | 63.25      | 59.40      |
| Maximum Value      | 132.00     | 178.00     | 186.83     |
| Median             | 85.00      | 104.00     | 106.60     |
| Kurtosis           | -0.141     | 0.022      | 0.514      |

**Table 4.25:** Statistical analysis of calcium for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 91.50      | 113.78     | 115.46     |
| Standard Deviation | 23.90      | 28.96      | 33.65      |
| Standard Error     | 7.590      | 9.150      | 10.64      |
| Minimum Value      | 49.50      | 63.25      | 59.40      |
| Maximum Value      | 132.00     | 160.50     | 185.63     |
| Median             | 85.00      | 112.88     | 113.08     |
| Kurtosis           | -0.140     | 0.407      | 1.739      |

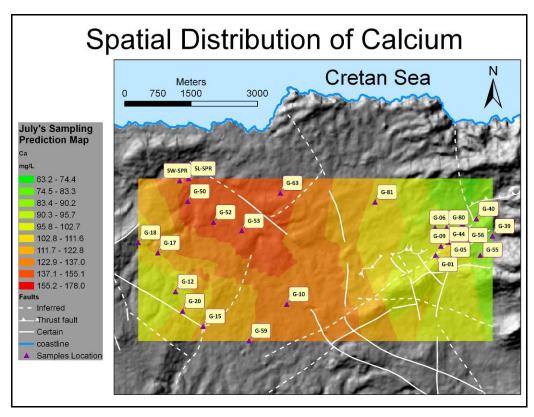


Fig. 4.69: Spatial distribution map of calcium (as mg/L) for July's 2008 sampling

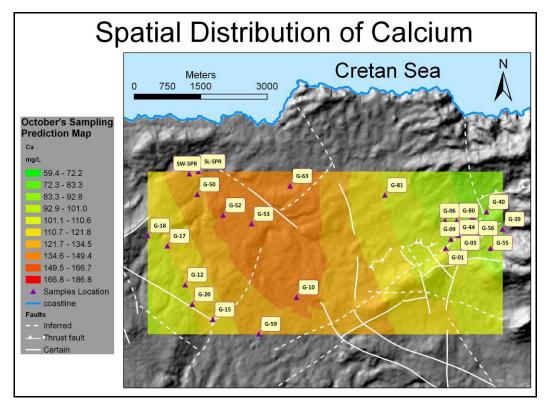


Fig. 4.70: Spatial distribution map of calcium (as mg/L) for October's 2008 sampling

### 4.7.1.3.2 Magnesium (Mg)

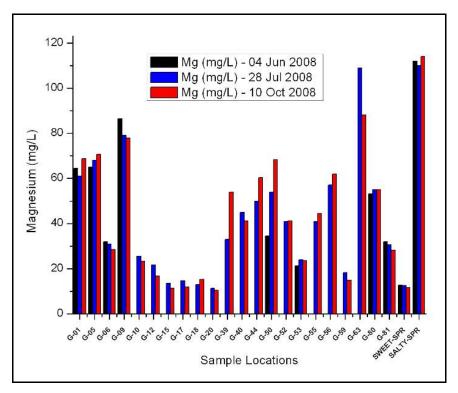


Fig. 4.71: Column graph of magnesium (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.26:** Statistical analysis of magnesium (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 51.38      | 42.47      | 43.42      |
| Standard Deviation | 31.10      | 28.16      | 28.56      |
| Standard Error     | 9.835      | 5.748      | 5.829      |
| Minimum Value      | 12.75      | 11.25      | 10.38      |
| Maximum Value      | 112.00     | 110.00     | 114.00     |
| Median             | 43.88      | 37.00      | 41.20      |
| Kurtosis           | -0.022     | 0.820      | -0.185     |

**Table 4.27:** Statistical analysis of magnesium for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 51.38      | 52.53      | 54.69      |
| Standard Deviation | 31.10      | 29.21      | 31.44      |
| Standard Error     | 9.835      | 9.236      | 9.942      |
| Minimum Value      | 12.75      | 12.50      | 11.70      |
| Maximum Value      | 112.00     | 110.00     | 114.00     |
| Median             | 43.88      | 54.50      | 61.75      |
| Kurtosis           | -0.022     | 0.200      | -0.293     |

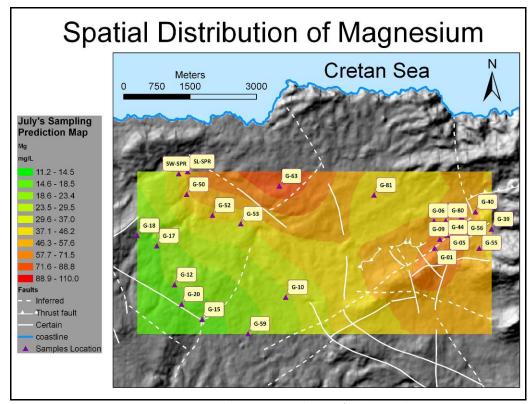


Fig. 4.72: Spatial distribution map of magnesium (as mg/L) for July's 2008 sampling

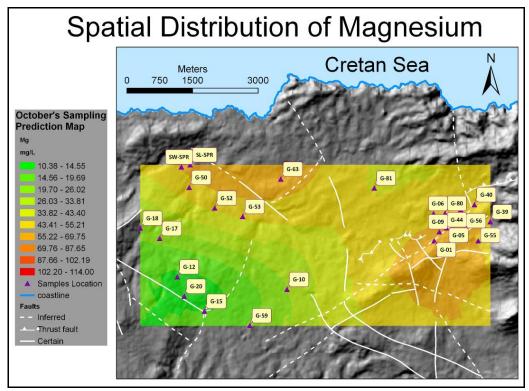


Fig. 4.73: Spatial distribution map of magnesium (as mg/L) for October's 2008 sampling

### 4.7.1.3.3 Potassium (K)

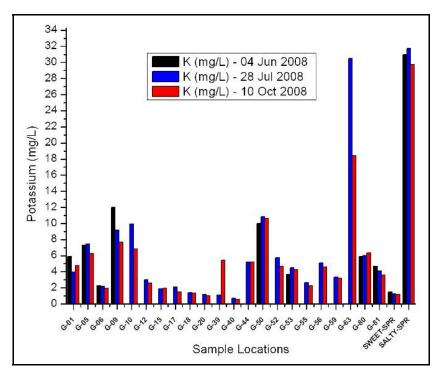


Fig. 4.74: Column graph of potassium (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.28:** Statistical analysis of potassium (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 8.43       | 6.47       | 5.67       |
| Standard Deviation | 8.57       | 8.11       | 6.39       |
| Standard Error     | 2.71       | 1.66       | 1.31       |
| Minimum Value      | 1.50       | 0.72       | 0.56       |
| Maximum Value      | 31.00      | 31.75      | 29.75      |
| Median             | 5.90       | 4.04       | 4.45       |
| Kurtosis           | 6.36       | 6.33       | 8.90       |

**Table 4.29:** Statistical analysis of potassium for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 8.43       | 8.14       | 7.65       |
| Standard Deviation | 8.57       | 8.82       | 8.24       |
| Standard Error     | 2.71       | 2.79       | 2.61       |
| Minimum Value      | 1.50       | 1.26       | 1.15       |
| Maximum Value      | 31.00      | 31.75      | 29.75      |
| Median             | 5.90       | 5.27       | 5.52       |
| Kurtosis           | 6.36       | 7.04       | 7.09       |

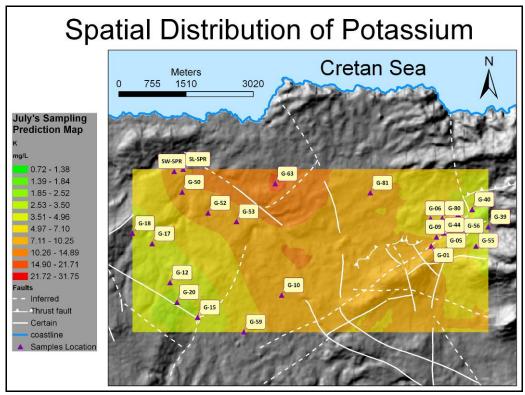


Fig. 4.75: Spatial distribution map of potassium (as mg/L) for July's 2008 sampling

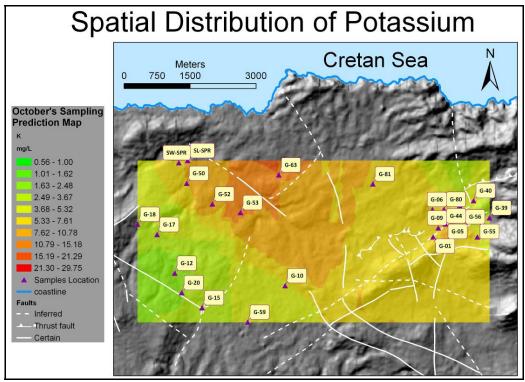


Fig. 4.76: Spatial distribution map of potassium (as mg/L) for October's 2008 sampling

### 4.7.1.3.4 Sodium (Na)

### In mg/L

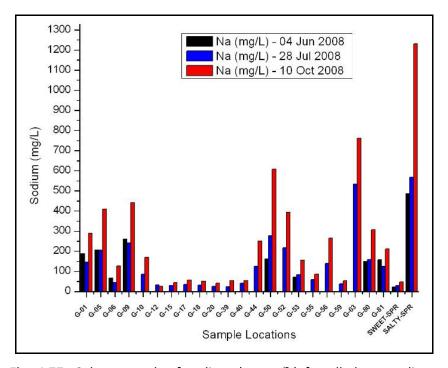


Fig. 4.77: Column graph of sodium (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.30:** Statistical analysis of sodium (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 177.30     | 137.52     | 255.82     |
| Standard Deviation | 129.9      | 148.4      | 284.9      |
| Standard Error     | 41.09      | 30.29      | 58.15      |
| Minimum Value      | 23.00      | 23.75      | 25.75      |
| Maximum Value      | 486.50     | 568.75     | 1230.00    |
| Median             | 160.00     | 84.50      | 163.38     |
| Kurtosis           | 3.336      | 3.713      | 5.155      |

**Table 4.31:** Statistical analysis of sodium for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 177.30     | 187.98     | 382.90     |
| Standard Deviation | 129.9      | 155.9      | 340.9      |
| Standard Error     | 41.09      | 49.29      | 107.8      |
| Minimum Value      | 23.00      | 30.50      | 47.50      |
| Maximum Value      | 486.50     | 568.75     | 1230.00    |
| Median             | 160.00     | 152.00     | 298.75     |
| Kurtosis           | 3.336      | 3.889      | 4.360      |

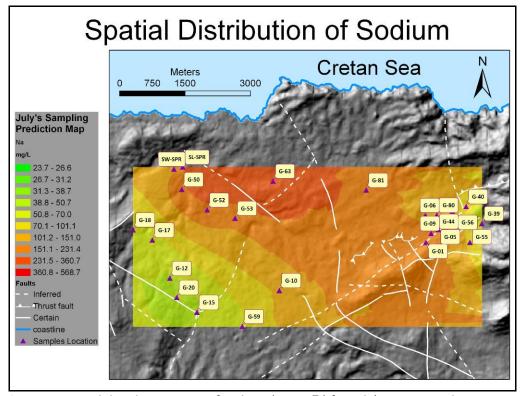


Fig. 4.78: Spatial distribution map of sodium (as mg/L) for July's 2008 sampling

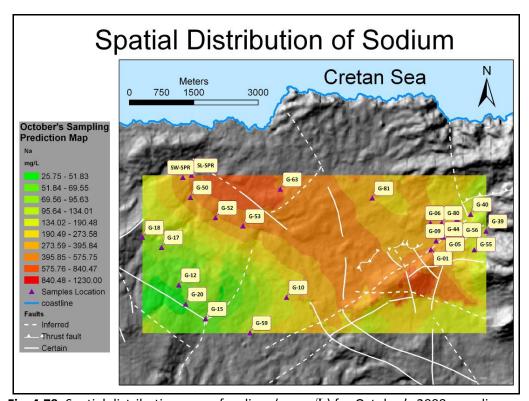


Fig. 4.79: Spatial distribution map of sodium (as mg/L) for October's 2008 sampling

### 4.7.1.3.5 Iron (Fe)

**Table 4.32:** Statistical analysis of iron (as mg/L) for all the samplings (June, July, October 2008)

| 04/06/2008 | 28/07/2008 | 01/10/2008 |
|------------|------------|------------|
| 10         | 24         | 24         |
| 0          | 0          | 0          |
|            |            |            |

### **4.7.1.4** Inorganic Nonmetallic Constituents

### 4.7.1.4.1 Boron (B)

In mg/L

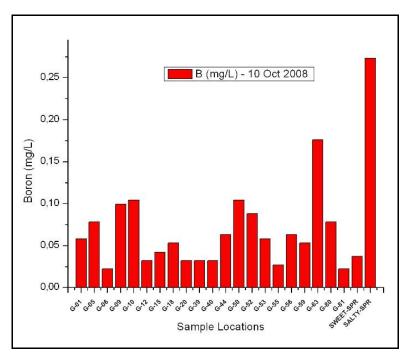


Fig. 4.80: Column graph of boron (as mg/L) for October's 2008 sampling

 $\label{eq:table 4.33:} \textbf{Table 4.33:} \ \textbf{Statistical analysis of boron (as } mg/L) \\ \textbf{for October's 2008 sampling}$ 

| DATE               | 01/10/2008 |
|--------------------|------------|
| Number of Samples  | 23         |
| Mean               | 0.07       |
| Standard Deviation | 0.06       |
| Standard Error     | 0.01       |
| Minimum Value      | 0.02       |
| Maximum Value      | 0.28       |
| Median             | 0.06       |
| Kurtosis           | 6.99       |

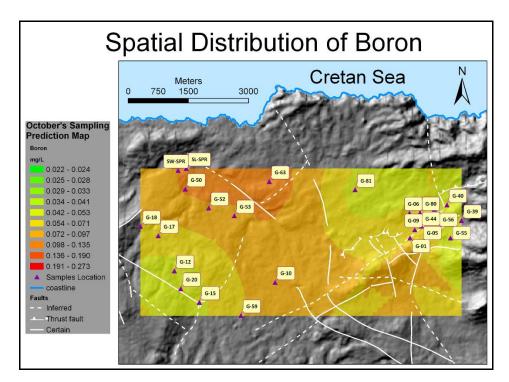
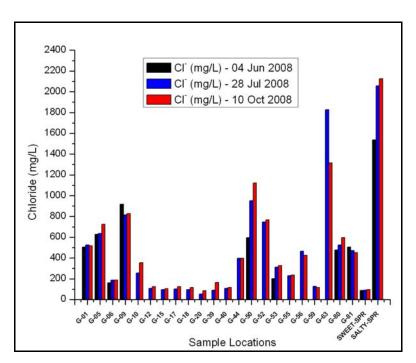


Fig. 4.81: Spatial distribution map of boron (as mg/L) for October's 2008 sampling

### 4.7.1.4.2 Chloride (Cl-)

### In mg/L



**Fig. 4.82:** Column graph of chloride (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.34:** Statistical analysis of chloride (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 561.8      | 469.9      | 475.9      |
| Standard Deviation | 423        | 523        | 488        |
| Standard Error     | 134        | 107        | 99.6       |
| Minimum Value      | 86.9       | 54.5       | 85.9       |
| Maximum Value      | 1536.5     | 2055.9     | 2125.3     |
| Median             | 506.8      | 283.9      | 340.9      |
| Kurtosis           | 2.56       | 4.11       | 4.79       |

**Table 4.35:** Statistical analysis of chloride for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 10         | 10         |
| Mean               | 561.8      | 657.3      | 696.9      |
| Standard Deviation | 423        | 557.6      | 587.0      |
| Standard Error     | 134        | 176        | 186        |
| Minimum Value      | 86.9       | 91.5       | 95.9       |
| Maximum Value      | 1536.5     | 2055.9     | 2125.3     |
| Median             | 506.8      | 526.3      | 555.8      |
| Kurtosis           | 2.56       | 4.69       | 3.78       |

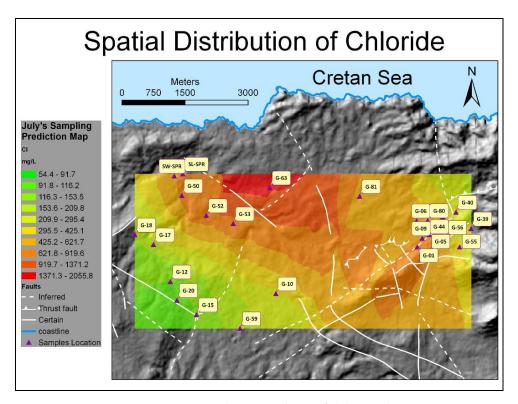


Fig. 4.83: Spatial distribution map of chloride (as mg/L) for July's 2008 sampling

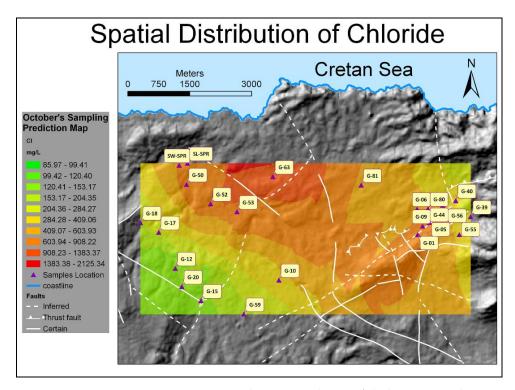
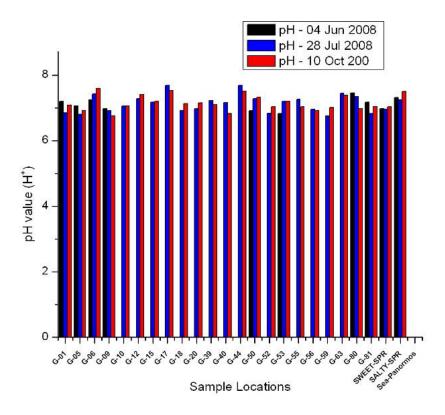


Fig. 4.84: Spatial distribution map of chloride (as mg/L) for October's 2008 sampling

# 4.7.1.4.3 pH value ( $H^+$ )



**Fig. 4.85:** Column graph of pH for all the samplings (June, July, October 2008)

Table 4.36: Statistical analysis of pH for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008             | 28/07/2008 | 01/10/2008 |  |
|--------------------|------------------------|------------|------------|--|
| Number of Samples  | 10                     | 24         | 24         |  |
| Mean               | 7.1                    | 7.1        | 7.1        |  |
| Standard Deviation | Standard Deviation 0.2 |            | 0.2        |  |
| Standard Error     | Standard Error 0.06    |            | 0.04       |  |
| Minimum Value      | 6.8                    | 6.8        | 6.8        |  |
| Maximum Value 7.5  |                        | 7.7        | 7.6        |  |
| Median             | 7.1                    | 7.2        | 7.1        |  |
| Kurtosis -0.7      |                        | -0.4       | -0.7       |  |

**Table 4.37:** Statistical analysis of pH for the same 10 samples for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008          | 28/07/2008 | 01/10/2008 |  |
|--------------------|---------------------|------------|------------|--|
| Number of Samples  | 10                  | 10         | 10         |  |
| Mean               | 7.1                 | 7.1        | 7.2        |  |
| Standard Deviation | 0.2                 | 0.2        | 0.3        |  |
| Standard Error     | Standard Error 0.06 |            | 0.08       |  |
| Minimum Value      | Minimum Value 6.8   |            | 6.8        |  |
| Maximum Value      | Maximum Value 7.5   |            | 7.6        |  |
| Median             | 7.1                 | 7.1        | 7.1        |  |
| Kurtosis -0.7      |                     | -1.9       | -0.4       |  |

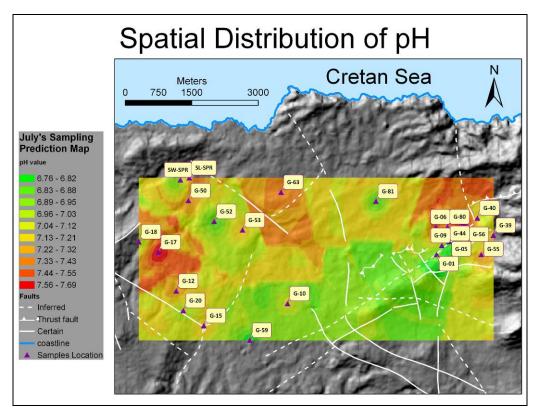


Fig. 4.86: Spatial distribution map of pH for July's 2008 sampling

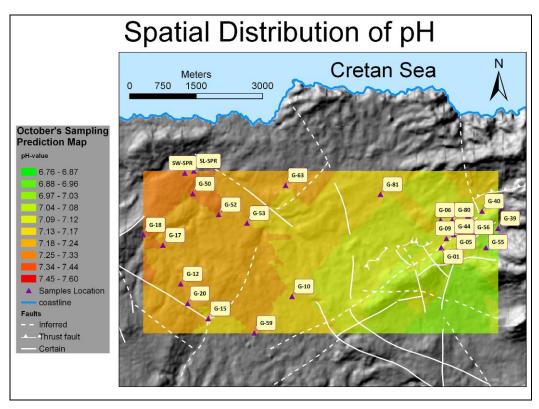


Fig. 4.87: Spatial distribution map of pH for October's 2008 sampling

# 4.7.1.4.4 Nitrogen (Nitrates, ${}^{NO_3^-}$ )

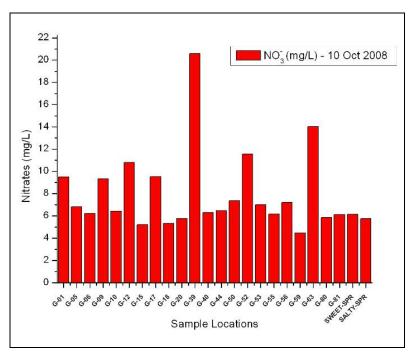


Fig. 4.88: Column graph of nitrate (as mg/L) for October's 2008 sampling

**Table 4.38:** Statistical analysis of nitrate (as mg/L) for October's 2008 sampling

| DATE               | 01/10/2008 |
|--------------------|------------|
| Number of Samples  | 23         |
| Mean               | 7.9        |
| Standard Deviation | 3.5        |
| Standard Error     | 0.7        |
| Minimum Value      | 4.5        |
| Maximum Value      | 20.6       |
| Median             | 6.5        |
| Kurtosis           | 6.6        |

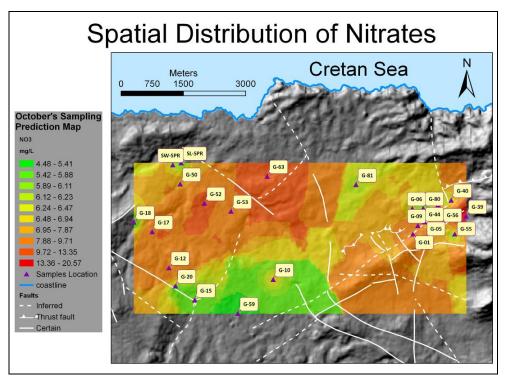


Fig. 4.89: Spatial distribution map of nitrate (as mg/L) for October's 2008 sampling

## **4.7.1.4.5** Sulfate ( $SO_4^{2-}$ )

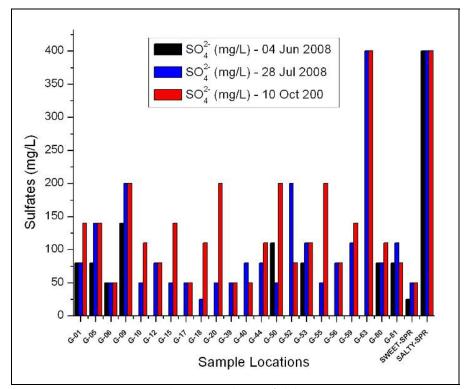


Fig. 4.90: Column graph of sulphate (as mg/L) for all the samplings (June, July, October 2008)

**Table 4.39:** Statistical analysis of sulfate (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008 | 28/07/2008 | 01/10/2008 |
|--------------------|------------|------------|------------|
| Number of Samples  | 10         | 24         | 24         |
| Mean               | 113        | 109        | 137        |
| Standard Deviation | 105        | 100        | 95         |
| Standard Error     | 33         | 20         | 19         |
| Minimum Value      | 25         | 25         | 50         |
| Maximum Value 400  |            | 400        | 400        |
| Median             | 80         | 80         | 110        |
| Kurtosis           | 7.8        | 4.8        | 3.4        |

**Table 4.40:** Statistical analysis of sulfate for the same 10 samples (as mg/L) for all the samplings (June, July, October 2008)

| DATE               | 04/06/2008             | 28/07/2008 | 01/10/2008 |  |
|--------------------|------------------------|------------|------------|--|
| Number of Samples  | 10                     | 10         | 10         |  |
| Mean               | 113                    | 127        | 148        |  |
| Standard Deviation | Standard Deviation 105 |            | 103        |  |
| Standard Error 33  |                        | 34         | 33         |  |
| Minimum Value      | 25                     | 50         | 50         |  |
| Maximum Value 400  |                        | 400        | 400        |  |
| Median             | Median 80              |            | 125        |  |
| Kurtosis           | 7.8                    | 5.2        | 3.9        |  |

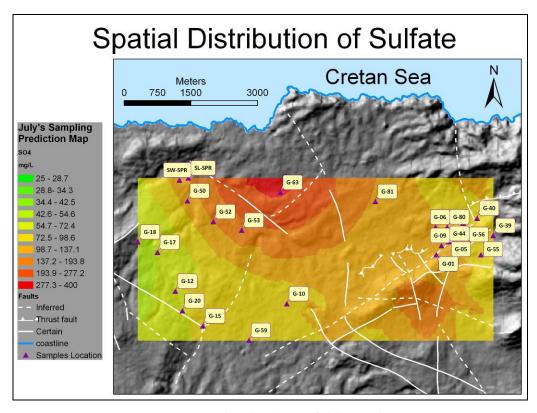


Fig. 4.91: Spatial distribution map of sulfate (as mg/L) for July's 2008 sampling

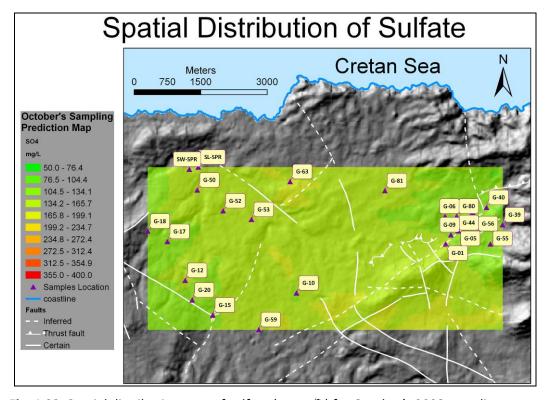


Fig. 4.92: Spatial distribution map of sulfate (as mg/L) for October's 2008 sampling

### **4.7.1.4.6** Phosphate ( $PO_4^{3-}$ )

**Table 4.41:** Statistical analysis of phosphate (as mg/L) for October 2008 sampling

| DATE                  | 01/10/2008 |
|-----------------------|------------|
| Number of Samples     | 24         |
| Concentration for all | 0.00       |
| the samples (mg/L)    | 0.00       |

#### 4.7.2 Special Interpretation of the results of the geochemical parameters

The results of the geochemical parameters were processed using graphic and statistical methods, and the results are presented in this chapter. At first place, the type of water of each sample location was characterized (based on the dominant ion), and then several diagrams, like Piper diagram, Durov diagram, dispersion diagrams etc, were constructed, and quality factors were calculated, in order to identify which is the source of contamination (seawater or halite).

#### 4.7.2.1 Ionic Concentrations of the Aegean seawater

The chemical analysis of the seawater of the study area didn't take place at the lab but concentrations of the Aegean sea-water were taken from Yalçin et al. (1997).

#### 4.7.2.2 Characterization of Groundwater

Concentrations (in mg/L) of chemical parameters as determined by various methods (**Appendix C**), were converted into me/L (milliequivalents/Litre) for characterization of groundwater according to the dominant ions (**Table 4.43**).

**Table 4.42:** Aegean seawater concentrations as derived from Yalçin et al. (1997).

| lons                          | Aegean sea-water, mg/L |
|-------------------------------|------------------------|
| Cations                       |                        |
| Na⁺                           | 11699                  |
| Mg <sup>2+</sup>              | 1337                   |
| Ca <sup>2+</sup>              | 477                    |
| K <sup>+</sup>                | 283                    |
| Anions                        |                        |
| Cl                            | 21999                  |
| SO <sub>4</sub> <sup>2-</sup> | 3016                   |
| CO <sub>3</sub> <sup>2-</sup> | 140                    |
| Br⁻                           | 60                     |
| Total                         | 39011                  |

Generally,  $Ca(HCO_3)_2$  type of water is considered as fresh water, while NaCl type of water is considered as salty. On the other hand,  $CaCl_2$  type of water is characterized as transition water type.

According to the main constituents (dominant ions), from the 24 samples, three types of groundwater determined: NaCl type (blue colour) - 13 samples, Ca(HCO<sub>3</sub>)<sub>2</sub> type (green colour) - 9 samples, and CaCl<sub>2</sub>.(red colour) - 2 samples. Spatial distributions of groundwater types for October's 2008 sampling (applying ordinary kriging) is shown in **Figure 4.93**.

**Table 4.43:** Concentrations of chemical parameters in me/L for characterization of groundwater

| Code  | e Anions         |      |                 | Cat  | 1     |      |      |                                    |
|-------|------------------|------|-----------------|------|-------|------|------|------------------------------------|
| Name  | HCO <sub>3</sub> | Cl   | SO <sub>4</sub> | К    | Na    | Са   | Mg   | Water                              |
|       | me/L             | me/L | me/L            | me/L | me/L  | me/L | me/L | Туре                               |
| G-01  | 6.7              | 14.6 | 2.9             | 0.12 | 12.62 | 5.23 | 5.66 | NaCl                               |
| G-05  | 5.6              | 20.5 | 2.9             | 0.16 | 17.84 | 5.59 | 5.81 | NaCl                               |
| G-06  | 4.8              | 5.2  | 1.0             | 0.05 | 5.52  | 2.96 | 2.35 | NaCl                               |
| G-09  | 6.2              | 23.3 | 4.2             | 0.19 | 19.25 | 5.87 | 6.41 | NaCl                               |
| G-10  | 7.7              | 10.0 | 2.3             | 0.17 | 7.43  | 7.50 | 1.92 | CaCl <sub>2</sub>                  |
| G-12  | 6.6              | 3.6  | 1.7             | 0.07 | 1.12  | 5.41 | 1.37 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-15  | 6.4              | 2.9  | 2.9             | 0.05 | 1.91  | 5.49 | 0.93 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-17  | 5.9              | 3.6  | 1.0             | 0.03 | 2.45  | 5.06 | 0.98 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-18  | 5.6              | 3.3  | 2.3             | 0.03 | 2.23  | 3.82 | 1.26 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-20  | 6.1              | 2.4  | 4.2             | 0.03 | 1.76  | 4.85 | 0.85 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-39  | 7.9              | 4.7  | 1.0             | 0.14 | 2.39  | 4.63 | 4.44 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-40  | 7.7              | 3.3  | 1.0             | 0.01 | 2.36  | 3.76 | 3.38 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-44  | 6.4              | 11.2 | 2.3             | 0.13 | 10.96 | 3.86 | 4.97 | NaCl                               |
| G-50  | 5.0              | 31.6 | 4.2             | 0.27 | 26.43 | 9.26 | 5.63 | NaCl                               |
| G-52  | 5.5              | 21.6 | 1.7             | 0.12 | 17.18 | 9.32 | 3.39 | NaCl                               |
| G-53  | 5.5              | 9.2  | 2.3             | 0.11 | 6.79  | 6.10 | 1.94 | NaCl                               |
| G-55  | 6.4              | 6.7  | 4.2             | 0.06 | 3.69  | 3.83 | 3.66 | CaCl <sub>2</sub>                  |
| G-56  | 6.3              | 12.0 | 1.7             | 0.12 | 11.57 | 5.03 | 5.09 | NaCl                               |
| G-59  | 6.4              | 3.3  | 2.9             | 0.08 | 2.33  | 6.35 | 1.22 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| G-63  | 4.6              | 37.1 | 8.3             | 0.47 | 33.13 | 7.39 | 7.26 | NaCl                               |
| G-80  | 5.2              | 16.8 | 2.3             | 0.16 | 13.38 | 4.85 | 4.53 | NaCl                               |
| G-81  | 5.1              | 12.7 | 1.7             | 0.09 | 9.18  | 5.70 | 2.32 | NaCl                               |
| SW-SP | 5.9              | 2.7  | 1.0             | 0.03 | 2.07  | 4.63 | 0.96 | Ca(HCO <sub>3</sub> ) <sub>2</sub> |
| SL-SP | 4.0              | 59.9 | 8.3             | 0.76 | 53.51 | 7.42 | 9.38 | NaCl                               |

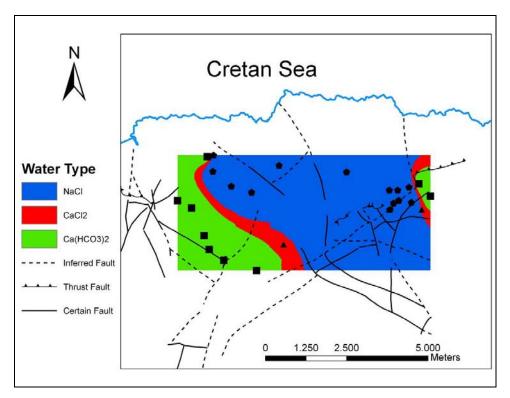


Fig. 4.93: Spatial distributions of groundwater types for October's 2008 sampling. Rectangulars: Ca(HCO<sub>3</sub>)<sub>2</sub> type, Triangles: CaCl<sub>2</sub> type, and pentagons: NaCl type.

### 4.7.2.3 Ternary Diagrams

Two ternary (tri-lateral) diagrams were generated for dominant anions and dominant cations respectively based on the previous **section 4.7.3.2**. Each diagram is based on three columns of data for depicting the proportions of the main cations or anions, expressed in milliequivalents per litre (me/L).

For anions, the diagram has 100%  $Cl^-$  to the left corner, bicarbonate to the right and  $SO_4^{2^-}$  on top. For cations, the diagram has 100%  $Ca^{2^+}$  in the left corner, 100%  $Mg^{2^+}$  towards the right, and 100%  $Na^+$  upwards.

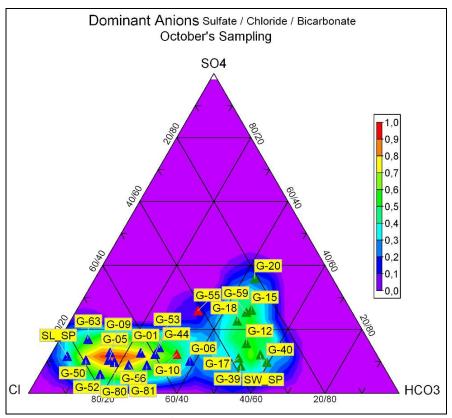


Fig. 4.94: Ternary diagram of major anions

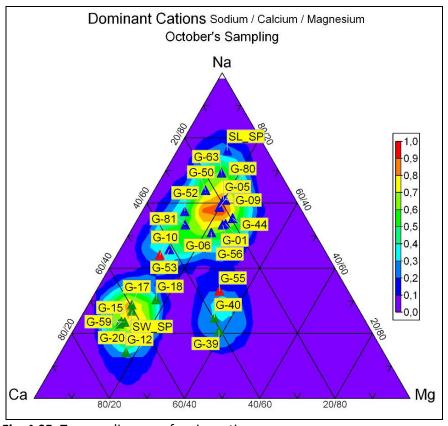
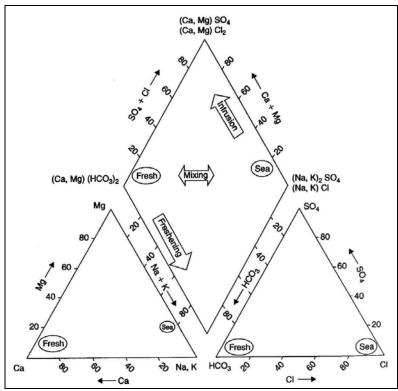


Fig. 4.95: Ternary diagram of major cations

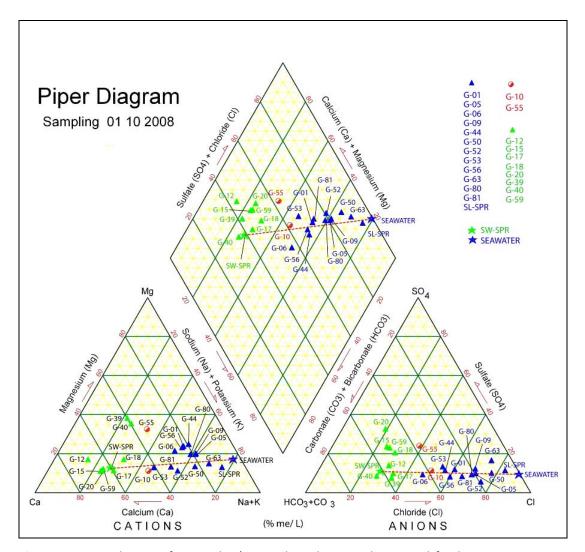
#### 4.7.2.4 Piper Diagram

A very useful way for compiling a large number of chemical analyses is by constructing the so-called Piper diagram. This diagram contains two triangular charts for illustrating the proportions of cations and anions (expressed in milliequivalents /Litre (me/L)). At the left is situated the triangle for cations ( $Ca^{2+}$ ,  $Na^+$  +  $K^+$ ,  $Mg^{2+}$ ), while at the right the triangle for anions (carbonate,  $Cl^-$ ,  $SO_4^{2-}$ ) (**Fig. 4.96**).

The triangle for cations has 100% of  $Ca^{2+}$ ,  $Na^+ + K^+$  and  $Mg^{2+}$  in the left, the right, and on top corner respectively. The sum of their concentrations (in me/L) is recalculated to 100% and the relative composition is plotted in the triangle. Similarly, for anions, the triangle has 100% carbonate,  $CI^-$  and  $SO_4^{2-}$  to the left, to the right and on top corner respectively. The two data points in the triangles (cation and anion triangles) are united by drawing lines parallel to the outside boundary until they join in the middle diamond shape (**Fig. 4.96**). Therefore, a single point indicates the relative chemical composition of the groundwater (Appelo and Postma, 2005).



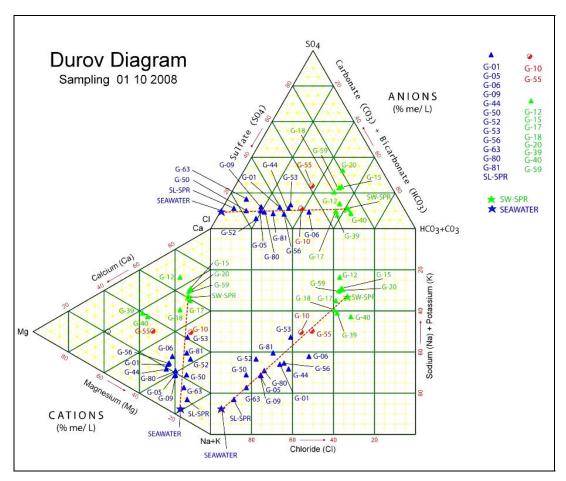
**Fig. 4.96:** Piper plot showing average composition of fresh water and seawater (Appelo and Postma, 2005).



**Fig. 4.97:** Piper diagram for October's sampling showing theoretical fresh-seawater mixing line: Red dotted line is the mixing line between fresh (sweet spring) and seawater

#### 4.7.2.5 Durov Diagram

The Durov diagram plots the major ions as percentages of milli-equivalents (me) in two triangles, while the total anions and the total cations are equal to 100%. The data points (in the two triangles) are projected onto a square grid which lies perpendicular to the third axis in each triangle (Fig. 4.98). (Rockworks 14 Help, 2008).



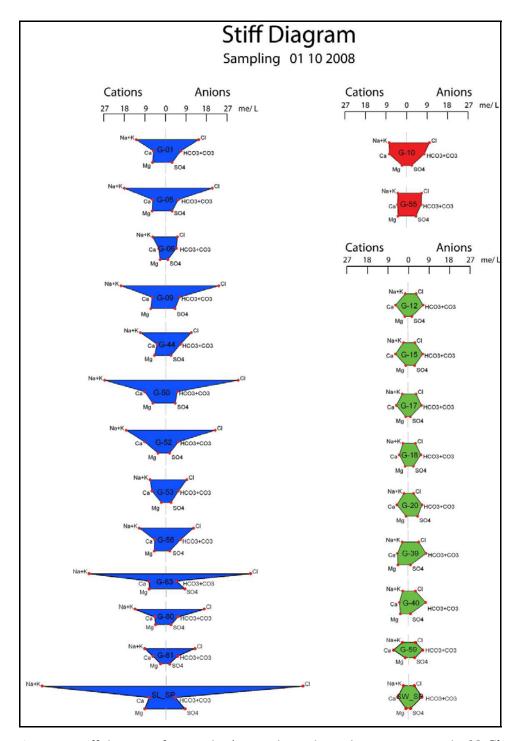
**Fig. 4.98:** Durov diagram for October's sampling. Red dotted line is the mixing line between fresh (sweet spring) and seawater

### 4.7.2.6 Stiff Diagrams - Stiff Map

The Stiff diagrams are plotted for individual samples as a method of graphically comparing the concentration of selected anions and cations for several individual samples. The shape formed by the Stiff diagrams identifies samples that have similar compositions and are useful when used as map symbols (**Fig. 4.99 & 4.100**) (Rockworks 14 Help, 2008).

A stiff diagram consists of three horizontal axes displaying selected components. On each axis a cation is plotted to the left and an anion to the right, again in me/L. The uppermost axis has  $Na^+$  to the left and  $Cl^-$  to the right and reflects a possible marine influence since in seawater NaCl is the dominant salt. The second axis has  $Ca^{2+}$  to the left and  $HCO_3^-$  to the right and this axis is meant to display the dissolution of  $CaCO_3$ . The third axis has  $Mg^{2+}$  to the left and

 $SO_4^{2-}$  to the right, presenting the remaining two major components in most waters (Appelo and Postma, 2005).



**Fig. 4.99:** Stiff diagrams for October's sampling. Blue colour represents the NaCl water type, red represents the  $CaCl_2$  water type, and green represents the  $Ca(HCO_3)_2$  type (according to section **4.7.3.2**).

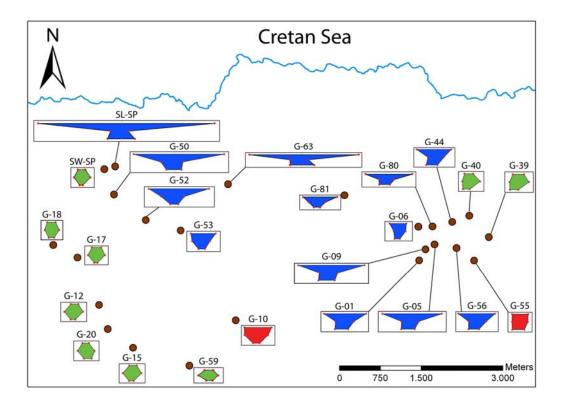


Fig. 4.100: Stiff map: Spatial distribution of Stiff diagrams for October's sampling

### 4.7.2.7 Sodium Absorption Ratio (SAR)

High sodium concentrations in irrigation water affect the permeability of soil and cause infiltration problems, and finally results in breakdown of soil aggregates (Kallergis, 2001).

Geochemists often use the Sodium Absorption Ratio (SAR) of water to estimate the appropriateness of irrigation water, as proposed first from Ayer in 1975. SAR is defined by the following equation:

$$SAR = \frac{Na}{\sqrt{(Ca + Mg)/2}} \text{, where Na, Ca, Mg in me/L}$$

The SAR hazard classification is shown in **Figure 4.101**, where values below 6 indicate no problem concerning the irrigation water, between 6 to nine the SAR hazard is moderate, and above 9 the hazard is acute, and the water is unsuitable for any kind of crops (Kallergis, 2001).

The SAR hazard map of the study area, which was extracted in GIS environment for October's sampling (where sodium was increased greatly), using ordinary Kriging interpolator, is presented below (Fig. 4.101).

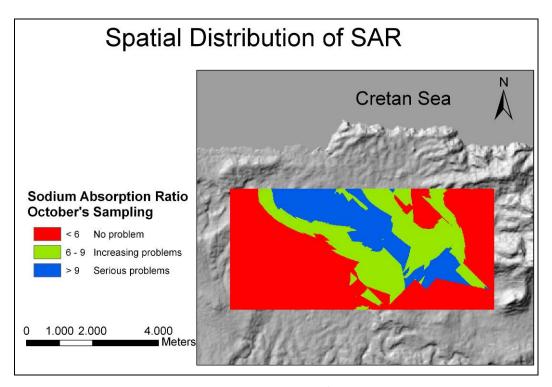


Fig. 4.101: SAR hazard map of the study area.

#### 4.7.2.8 Wilcox Plot

Using SAR and electrical conductivity values, an easy way that can be used to determine easily the viability of irrigation water is the Wilcox plot.

The Wilcox diagram is a simple scatter plot of SAR on the Y-axis vs. electrical conductivity on the X-axis (in log scale). The plot was created in AquaChem software 5.1 Version by Rockworks. The categories that the software divides the sodium (SAR) and salinity hazard (EC) are giving in **Table 4.44**.

| Cor | Conductivity (μs/cm) |           |  | SA        | R <sup>*</sup> |
|-----|----------------------|-----------|--|-----------|----------------|
| C1  | Low                  | 0-249     |  | <b>S1</b> | Low            |
| C2  | Medium               | 250-749   |  | S2        | Medium         |
| С3  | High                 | 750-2249  |  | \$3       | High           |
| C4  | Very High            | 2250-5000 |  | <b>S4</b> | Very High      |

Table 4.44: Categories of SAR and EC used for Wilcox diagram construction

**S1**: Line equation: y = -1.5816e - 3x + 10.15816

**S2**: Line equation: y= -2.2959e-3x + 18.22959

**S3**: Line equation: y = -3.0102e - 3x + 26.30102

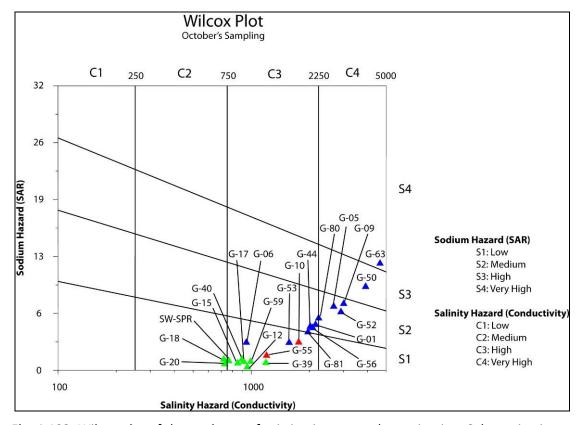


Fig. 4.102: Wilcox plot of the study area for irrigation water determination. Salty spring is not included (out of range (EC>5,000 $\mu$ S/cm))

<sup>\*</sup> The locations of the SAR lines are determined by the following equations (AquaChem Help, 2008):

The Wilcox plot for the study area for October's sampling (where sodium was increased greatly), is presented below (**Fig. 4.102**). Note that only 23 of the 24 sample locations are depicted, because the electrical conductivity of Salty Spring was out of range (above  $5,000\mu s/cm$  - very high salinity hazard), so this sample location is not included in the Wilcox plot.

#### 4.7.2.9 Dispersion Diagrams

Dispersion diagrams were created in order to find if the water from each borehole has the same source of contamination. This fact was checked by the correlation coefficient R (known as Pearson's R) which is used in statistics for indicating the strength and direction of a linear relationship between two random variables (Rodgers & Nicewander, 1988).

Several authors have offered guidelines for the classification of a correlation coefficient R (e.g. Lomax, 2007; Cohen, 1988), as the interpretation of a correlation coefficient depends on the purposes. For the interpretation of the size of correlation of the chemical parameters, the classification presented in **Table 4.45** was used:

| Correlation | R         |
|-------------|-----------|
| None        | ≈0        |
| Weak        | <0.50     |
| Medium      | 0.50-0.80 |
| Strong      | >0.80     |
| Perfect     | 1         |

**Table 4.45:** Classification of correlation coefficient which used for the chemical parameters

So, only when the data points all lie exactly on a straight line (with positive slope) a perfect correlation of 1 occurs. A correlation bigger than 0.8 is usually described as strong, while a correlation less than 0.5 is described as weak. No linear correlation for R close to 0.

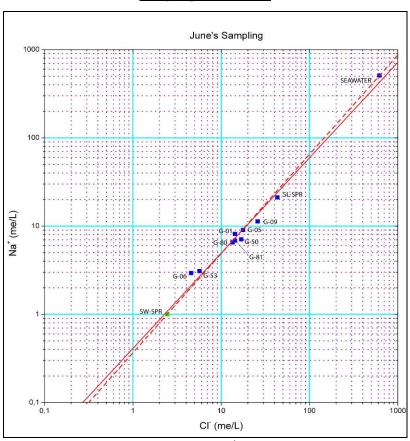
Five kinds of dispersion diagrams were constructed for all the samplings (June, July, August 2008), where various major elements are plotted in relation to Cl<sup>-</sup> concentration: Na-Cl, Ca-Cl, K-Cl, Mg-Cl, and SO<sub>4</sub>-Cl. The solid line represents the regression line of each diagram, drawn

according to the least-square method, while, the dotted line is the marine composition line (mixing line), joining the end-members - fresh water (sweet spring) and Aegean seawater.

All cross-plots have very high correlation coefficients (R) of their concentrations (0.91-0.98), and a few close to 0.8.

### 4.7.2.9.1 Na-Cl

### Sampling 4 June 2008

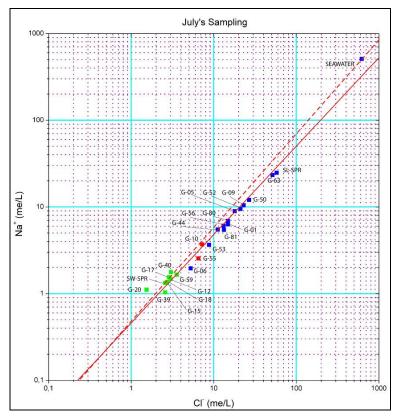


**Fig. 4.103:** Dispersion Diagram of Na<sup>+</sup> in relation to Cl<sup>-</sup> for June's sampling

| Yscale(Y) = A + B * xscale(X) |  |  |  |
|-------------------------------|--|--|--|
| Parameter Value Error         |  |  |  |
| A -0.38548 0.05289            |  |  |  |
| <b>B</b> 1.08035 0.03861      |  |  |  |

| R-Value | Standard<br>Deviation | N  | P value |
|---------|-----------------------|----|---------|
| 0.99    | 0.08                  | 11 | <0.0001 |

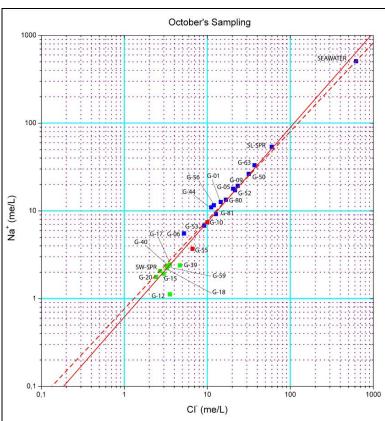
### Sampling 28 July 2008



**Fig. 4.104:** Dispersion Diagram of Na<sup>+</sup> in relation to Cl<sup>-</sup> for July's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| A -0.33832 0.03102            |  |  |  |  |
| <b>B</b> 1.01972 0.02743      |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.99    | 0.08                  | 25 | <0.0001 |



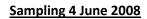
### Sampling 10 October 2008

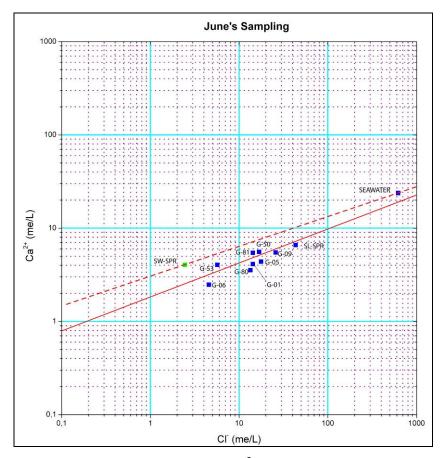
**Fig. 4.105:** Dispersion Diagram of  $\mathrm{Na}^+$  in relation to  $\mathrm{Cl}^-$  for October's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| A -0.20887 0.04235            |  |  |  |  |
| <b>B</b> 1.08001 0.0369       |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.99    | 0.09                  | 25 | <0.0001 |

### 4.7.2.9.2 Ca-Cl



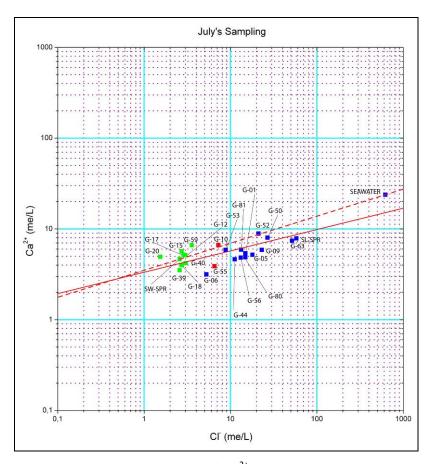


**Fig. 4.106:** Dispersion Diagram of Ca<sup>2+</sup> in relation to Cl<sup>-</sup> for June's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| <b>A</b> 0.26208 0.07304      |  |  |  |  |
| <b>B</b> 0.36441 0.05333      |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.92    | 0.11                  | 11 | <0.0001 |

### Sampling 28 July 2008

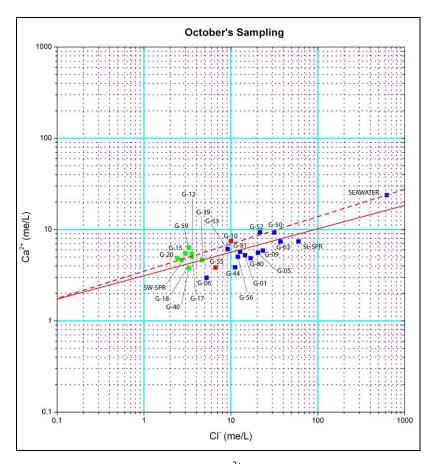


**Fig. 4.107:** Dispersion Diagram of Ca<sup>2+</sup> in relation to Cl<sup>-</sup> for July's sampling

| yscale(Y) = A + B * xscale(X) |                          |  |  |  |  |
|-------------------------------|--------------------------|--|--|--|--|
| Parameter Value Error         |                          |  |  |  |  |
| <b>A</b> 0.52269 0.04225      |                          |  |  |  |  |
| В                             | <b>B</b> 0.23525 0.03737 |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.80    | 0.11                  | 25 | <0.0001 |

### Sampling 10 October 2008

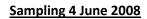


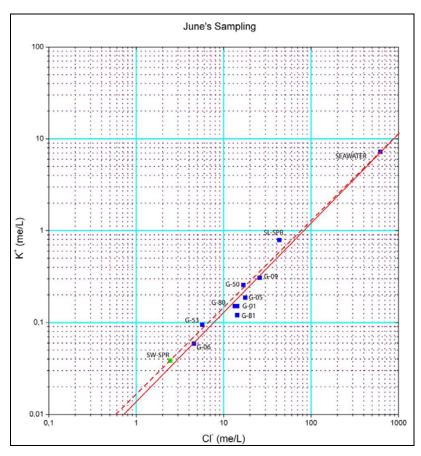
**Fig. 4.108:** Dispersion Diagram of Ca<sup>2+</sup> in relation to Cl<sup>-</sup> for October's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| <b>A</b> 0.49422 0.04762      |  |  |  |  |
| B 0.25722 0.0415              |  |  |  |  |

| R-Value | Standard  | N  | Р       |
|---------|-----------|----|---------|
|         | Deviation |    |         |
| 0.79    | 0.11      | 25 | <0.0001 |

### 4.7.2.9.3 K-Cl



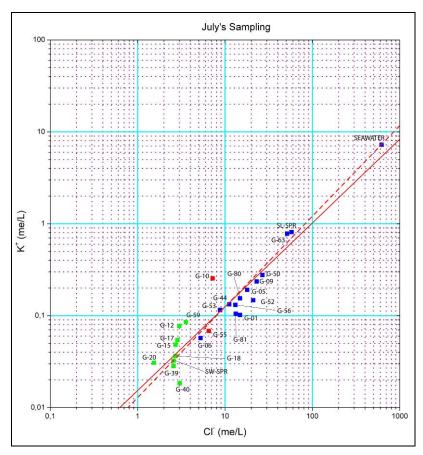


**Fig. 4.109:** Dispersion Diagram of  $K^+$  in relation to  $Cl^-$  for June's sampling

| yscale(Y) = A + B * xscale(X) |         |         |  |
|-------------------------------|---------|---------|--|
| Parameter Value Error         |         |         |  |
| Α                             | -1.8624 | 0.07292 |  |
| В                             | 0.97183 | 0.05324 |  |

| R-Value | Standard  | N  | Р       |
|---------|-----------|----|---------|
|         | Deviation |    |         |
| 0.99    | 0.11      | 11 | <0.0001 |

### Sampling 28 July 2008

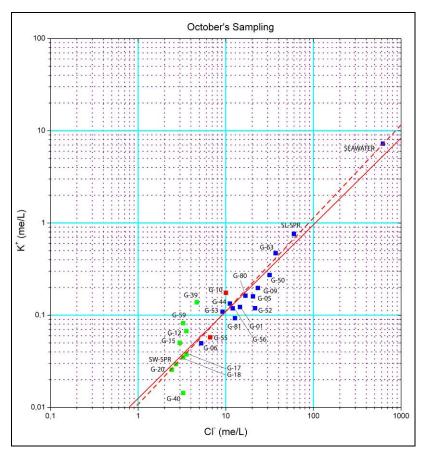


**Fig. 4.110:** Dispersion Diagram of K<sup>+</sup> in relation to Cl<sup>-</sup> for July's sampling

| yscale(Y) = A + B * xscale(X) |          |         |  |
|-------------------------------|----------|---------|--|
| Parameter Value Error         |          |         |  |
| Α                             | -1.81384 | 0.07173 |  |
| В                             | 0.91152  | 0.06344 |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.95    | 0.18                  | 25 | <0.0001 |

### Sampling 10 October 2008



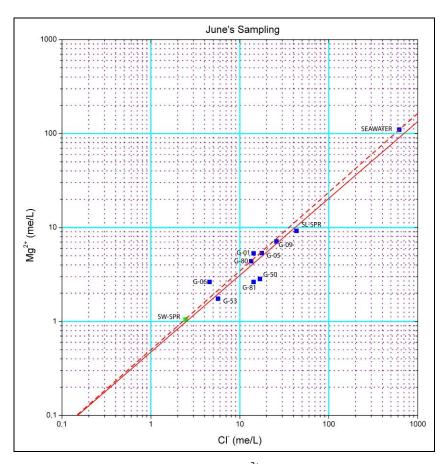
**Fig. 4.111:** Dispersion Diagram of  $K^+$  in relation to  $Cl^-$  for October's sampling

| yscale(Y) = A + B * xscale(X) |          |         |  |
|-------------------------------|----------|---------|--|
| Parameter Value Error         |          |         |  |
| Α                             | -1.90143 | 0.07959 |  |
| В                             | 0.94085  | 0.06936 |  |

| R-Value | Standard  | N  | Р       |
|---------|-----------|----|---------|
|         | Deviation |    |         |
| 0.94    | 0.18      | 25 | <0.0001 |

### 4.7.2.9.4 Mg-Cl

### Sampling 4 June 2008

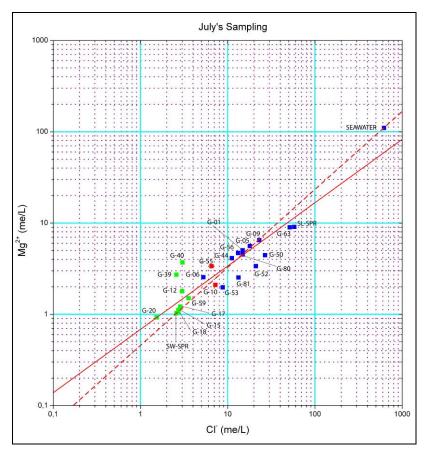


**Fig. 4.112:** Dispersion Diagram of  ${\rm Mg}^{2^+}$  in relation to  ${\rm Cl}^-$  for June's sampling

| yscale(Y) = A + B * xscale(X) |          |         |  |
|-------------------------------|----------|---------|--|
| Parameter Value Error         |          |         |  |
| Α                             | -0.32552 | 0.09213 |  |
| В                             | 0.81792  | 0.06726 |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.97    | 0.13                  | 11 | <0.0001 |

### Sampling 28 July 2008



**Fig. 4.113:** Dispersion Diagram of Mg<sup>2+</sup> in relation to Cl<sup>-</sup> for June's sampling

| yscale(Y) = A + B * xscale(X) |         |         |  |
|-------------------------------|---------|---------|--|
| Parameter                     | Value   | Error   |  |
| Α                             | -0.1643 | 0.06447 |  |
| В                             | 0.69353 | 0.05702 |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.93    | 0.16                  | 25 | <0.0001 |

## October's Sampling 1000 SEAWATER 1000 SEAWATER 1000 G-55 G-55 G-44 G-15 G-55 G-55 G-55 G-55 G-55 G-55 G-55 G-55 G-57 G-55 G-55 G-57 G-55 G-57 G-57

### Sampling 10 October 2008

**Fig. 4.114:** Dispersion Diagram of  $Mg^{2+}$  in relation to  $Cl^-$  for June's sampling

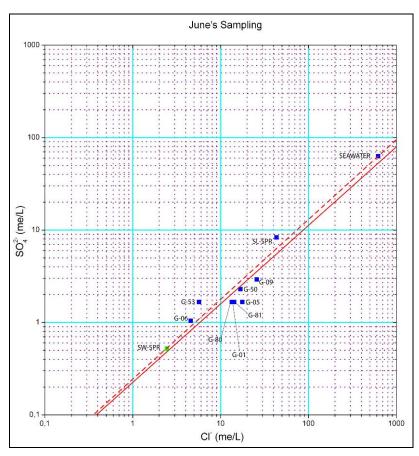
Cl (me/L)

| yscale(Y) = A + B * xscale(X) |         |         |  |
|-------------------------------|---------|---------|--|
| Parameter Value Error         |         |         |  |
| Α                             | -0.2608 | 0.07702 |  |
| В                             | 0.76055 | 0.06712 |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.92    | 0.18                  | 25 | <0.0001 |

### 4.7.2.9.5 SO<sub>4</sub>-Cl

### Sampling 4 June 2008

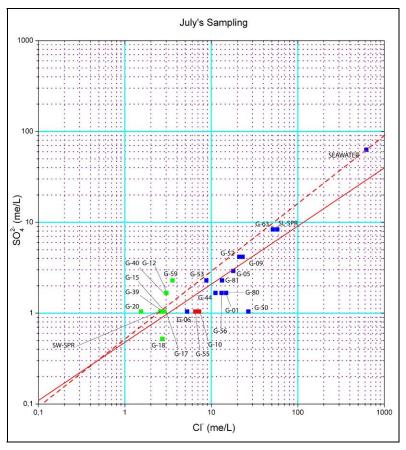


**Fig. 4.115:** Dispersion Diagram of  $SO_4^{2-}$  in relation to Cl<sup>-</sup> for June's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| <b>A</b> -0.64808 0.09758     |  |  |  |  |
| <b>B</b> 0.84905 0.07124      |  |  |  |  |

| R-Value | Standard  | N  | Р       |
|---------|-----------|----|---------|
|         | Deviation |    |         |
| 0.97    | 0.14      | 11 | <0.0001 |

### Sampling 28 July 2008



**Fig. 4.116:** Dispersion Diagram of  $SO_4^{2-}$  in relation to  $Cl^-$  for July's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| A -0.32093 0.08581            |  |  |  |  |
| <b>B</b> 0.63981 0.07589      |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.87    | 0.22                  | 25 | <0.0001 |

# October's Sampling 1000 SEAWATER SEAWATER G-59 G-59 G-59 G-50 G-15 G-18 G-80 SW-SPR G-12 G-56 G-81 G-56 G-81 G-56 G-81 G-56 G-81 G-56 G-81

### Sampling 10 October 2008

Fig. 4.117: Dispersion Diagram of  ${\rm SO_4}^{2^-}$  in relation to  ${\rm Cl}^-$  for October's sampling

Cl (me/L)

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| <b>A</b> -0.13717 0.10319     |  |  |  |  |
| <b>B</b> 0.55836 0.08992      |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.79    | 0.24                  | 25 | <0.0001 |

100

### **4.7.2.10** Factors controlling Groundwater quality (Indications of seawater intrusion)

Effects of seawater intrusion have been evaluated by series of ionic ratios. For this thesis four molar ratios were calculated:  $Na^+:Cl^-,Ca^{2+}:Mg^2,Cl^-:HCO_3^-,SO_4^-:Cl^-$ , and then they were showed versus  $Cl^-$  concentrations (except  $Ca^{2+}:Mg^{2+}$ ).

### 4.7.2.10.1 Ranges of hydrochemical ratios

**Table 4.46:** Ranges of geochemical ratios (modified from Rao et al., 2005)

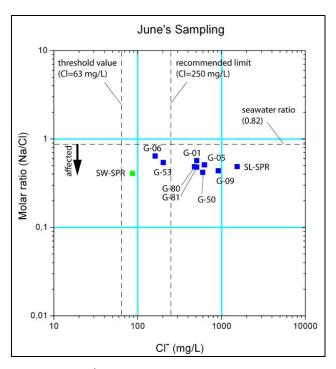
| .003)                               |           |  |
|-------------------------------------|-----------|--|
| Hydrochemical ratio                 | Range     | Remarks with the reference to the seawater |
|                                     | <0.82     | Contamination                              |
| Na <sup>+</sup> : Cl <sup>-</sup>   | ≈0.82     | Recent contamination                       |
|                                     | >0.82     | Non-contamination                          |
| Ca <sup>2+</sup> : Mg <sup>2+</sup> | <1        | Contamination                              |
|                                     | >1        | Non-contamination                          |
| CI. • HCO .                         | <1        | Non-contamination                          |
| Cl : HCO <sub>3</sub>               | >1        | Contamination                              |
| CO : . CI:                          | ≈ or <0.1 | Contamination                              |
| SO <sub>4</sub> : Cl                | >0.1      | Non-contamination                          |

### 4.7.2.10.2 Molar Ratio of Na<sup>+</sup> : Cl<sup>-</sup>

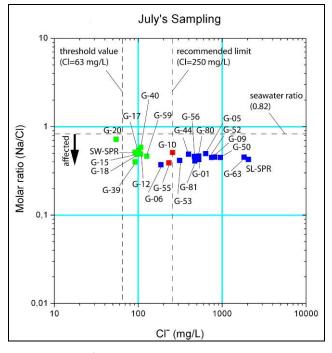
**Table 4.47**: Na<sup>+</sup> : Cl<sup>-</sup> molar ratio results for all the samplings (June, July, October).

| Code Name | Na : Cl (June) | Na : Cl (July) | Na : Cl (October) |
|-----------|----------------|----------------|-------------------|
| G-01      | 0.57           | 0.42           | 0.87              |
| G-05      | 0.51           | 0.50           | 0.87              |
| G-06      | 0.64           | 0.37           | 1.05              |
| G-09      | 0.44           | 0.45           | 0.83              |
| G-10      | -              | 0.51           | 0.74              |
| G-12      | -              | 0.49           | 0.32              |
| G-15      | -              | 0.49           | 0.64              |
| G-17      | -              | 0.54           | 0.69              |
| G-18      | -              | 0.50           | 0.68              |
| G-20      | -              | 0.72           | 0.73              |
| G-39      | -              | 0.40           | 0.51              |
| G-40      | -              | 0.58           | 0.72              |
| G-44      | -              | 0.49           | 0.98              |
| G-50      | 0.42           | 0.45           | 0.83              |
| G-52      | -              | 0.45           | 0.80              |
| G-53      | 0.54           | 0.42           | 0.74              |
| G-55      | 1              | 0.39           | 0.56              |
| G-56      | -              | 0.46           | 0.96              |
| G-59      | -              | 0.46           | 0.71              |
| G-63      | -              | 0.45           | 0.89              |
| G-80      | 0.49           | 0.47           | 0.80              |
| G-81      | 0.48           | 0.41           | 0.72              |
| SWEET-SPR | 0.40           | 0.51           | 0.76              |
| SALTY-SPR | 0.49           | 0.43           | 0.89              |

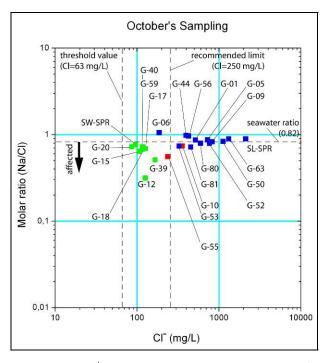
### Molar Ratio of Na<sup>+</sup>: Cl<sup>-</sup> versus Cl<sup>-</sup>



**Fig. 4.118:** Na<sup>+</sup> : Cl<sup>-</sup> molar ratio versus Cl<sup>-</sup> for June's sampling



**Fig. 4.119:**  $Na^+$  :  $Cl^-$  molar ratio versus  $Cl^-$  for July's sampling



**Fig. 4.120:** Na<sup>+</sup> : Cl<sup>-</sup> molar ratio versus Cl<sup>-</sup> for October's sampling

### 4.7.2.10.3 Molar Ratio Ca<sup>2+</sup> : Mg<sup>2+</sup>

**Table 4.48**: Ca<sup>2+</sup> : Cl<sup>-</sup> molar ratio results for all the samplings (June, July, October).

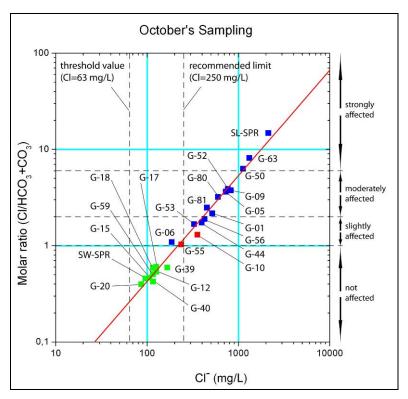
| Code Name | Ca : Mg (June) | Ca : Mg (July) | Ca : Mg (October) |
|-----------|----------------|----------------|-------------------|
| G-01      | 0.78           | 1.07           | 0.92              |
| G-05      | 0.82           | 0.93           | 0.96              |
| G-06      | 0.94           | 1.24           | 1.26              |
| G-09      | 0.77           | 0.90           | 0.92              |
| G-10      | -              | 3.17           | 3.91              |
| G-12      | -              | 2.86           | 3.95              |
| G-15      | -              | 5.10           | 5.88              |
| G-17      | -              | 4.28           | 5.15              |
| G-18      | -              | 3.73           | 3.03              |
| G-20      | -              | 5.32           | 5.68              |
| G-39      | -              | 1.29           | 1.04              |
| G-40      | -              | 1.13           | 1.11              |
| G-44      | -              | 1.12           | 0.776             |
| G-50      | 1.96           | 1.80           | 1.65              |
| G-52      | -              | 2.63           | 2.74              |
| G-53      | 2.31           | 2.98           | 3.14              |
| G-55      | -              | 1.15           | 1.05              |
| G-56      | -              | 1.03           | 0.99              |
| G-59      | -              | 4.40           | 5.19              |
| G-63      | -              | 0.83           | 1.02              |
| G-80      | 0.81           | 1.08           | 1.07              |
| G-81      | 2.07           | 2.33           | 2.45              |
| SW-SP     | 3.85           | 4.51           | 4.81              |
| SL-SP     | 0.71           | 0.87           | 0.79              |

### 4.7.2.10.4 Molar Ratio Cl : HCO<sub>3</sub> +CO<sub>3</sub>

**Table 4.49**: Cl<sup>-</sup> : HCO<sub>3</sub><sup>-</sup>+CO<sub>3</sub> molar ratio results for October's sampling

| Code Name | CI : HCO3 |
|-----------|-----------|
| Code Name | (October) |
| G-01      | 2.2       |
| G-05      | 3.6       |
| G-06      | 1.1       |
| G-09      | 3.8       |
| G-10      | 1.3       |
| G-12      | 0.5       |
| G-15      | 0.5       |
| G-17      | 0.6       |
| G-18      | 0.6       |
| G-20      | 0.4       |
| G-39      | 0.6       |
| G-40      | 0.4       |
| G-44      | 1.7       |
| G-50      | 6.3       |
| G-52      | 3.9       |
| G-53      | 1.7       |
| G-55      | 1.0       |
| G-56      | 1.9       |
| G-59      | 0.5       |
| G-63      | 8.2       |
| G-80      | 3.2       |
| G-81      | 2.5       |
| SWEET-SPR | 0.5       |
| SALTY-SPR | 15        |

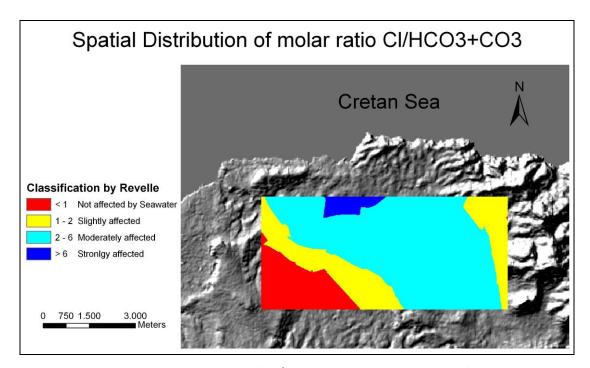
### Molar Ratio Cl : HCO<sub>3</sub> +CO<sub>3</sub> versus Cl



**Fig. 4.121:** Cl<sup>-</sup>: HCO<sub>3</sub><sup>-</sup>+CO<sub>3</sub> molar ratio versus Cl<sup>-</sup> for October's sampling

| yscale(Y) = A + B * xscale(X) |  |  |  |  |
|-------------------------------|--|--|--|--|
| Parameter Value Error         |  |  |  |  |
| A -2.56329 0.07812            |  |  |  |  |
| <b>B</b> 1.09704 0.03096      |  |  |  |  |

| R-Value | Standard<br>Deviation | N  | Р       |
|---------|-----------------------|----|---------|
| 0.99    | 0.06                  | 24 | <0.0001 |



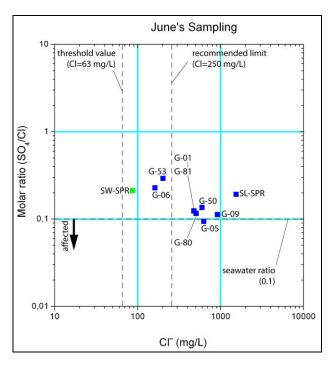
**Fig. 4.122:** Spatial distribution map of Cl/HCO<sub>3</sub>+CO<sub>3</sub> molar ratio. Classification by Revelle (Kallergis, 2001).

### 4.7.2.10.5 Molar Ratio SO<sub>4</sub>: Cl

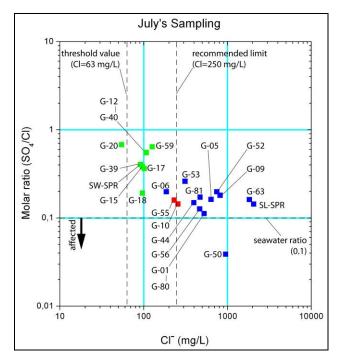
**Table 4.50**:  $SO_4^-$ :  $Cl^-$  molar ratio results for all the samplings (June, July, October).

| Code Name | SO <sub>4</sub> : Cl (June) | SO <sub>4</sub> : Cl (July) | SO <sub>4</sub> : Cl (October) |
|-----------|-----------------------------|-----------------------------|--------------------------------|
| G-01      | 0.12                        | 0.11                        | 0.20                           |
| G-05      | 0.09                        | 0.16238                     | 0.14                           |
| G-06      | 0.23                        | 0.19                        | 0.19                           |
| G-09      | 0.11                        | 0.18                        | 0.18                           |
| G-10      | -                           | 0.14                        | 0.23                           |
| G-12      | -                           | 0.55                        | 0.47                           |
| G-15      | -                           | 0.38                        | 0.98                           |
| G-17      | -                           | 0.36                        | 0.29                           |
| G-18      | -                           | 0.19                        | 0.70                           |
| G-20      | -                           | 0.68                        | 1.72                           |
| G-39      | -                           | 0.40                        | 0.22                           |
| G-40      | -                           | 0.55                        | 0.32                           |
| G-44      | -                           | 0.15                        | 0.21                           |
| G-50      | 0.14                        | 0.04                        | 0.13                           |
| G-52      | 1                           | 0.19                        | 0.08                           |
| G-53      | 0.29                        | 0.26                        | 0.25                           |
| G-55      | -                           | 0.16                        | 0.63                           |
| G-56      | -                           | 0.13                        | 0.14                           |
| G-59      | -                           | 0.64                        | 0.89                           |
| G-63      | -                           | 0.16                        | 0.22                           |
| G-80      | 0.12                        | 0.11                        | 0.14                           |
| G-81      | 0.12                        | 0.18                        | 0.13                           |
| SWEET-SPR | 0.21                        | 0.40                        | 0.38                           |
| SALTY-SPR | 0.19                        | 0.14                        | 0.14                           |

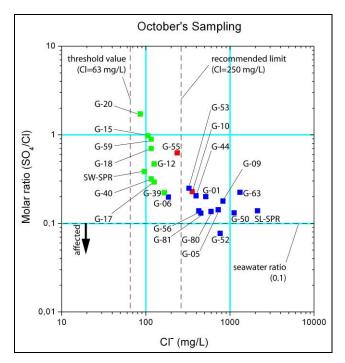
### Molar Ratio SO<sub>4</sub> : Cl versus Cl



**Fig. 4.123:** SO<sub>4</sub> : Cl molar ratio versus Cl for June's sampling



**Fig. 4.124:**  $SO_4^-$ :  $Cl^-$  molar ratio versus  $Cl^-$  for July's sampling



**Fig. 4.125:** SO<sub>4</sub> : Cl<sup>-</sup> mzolar ratio versus Cl<sup>-</sup> for October's sampling

### **4.7.2.11** Quality Maps

Two different approaches were used for the production of groundwater quality maps. These maps were created in a GIS environment in order to determine the quality of the waters of the study area based on different groups of geochemical parameters. The first groundwater quality map, takes into account conductivity, total hardness, chloride, sulfate, and nitrate, and it is commonly used in urban areas for groundwater assessment (Ducci, 1999; Nas & Berktay, 2008) based on Civita et al (1993) classification. Whereas, the second one, known as Groundwater Quality Index (GQI) links different water quality data (calcium, magnesium, sodium, chloride, sulfate, TDS and nitrate) concentrations to the WHO's guidelines (**Table 3.6** of *Chapter 3*).

### 4.7.2.11.1 Groundwater Quality Map (based on Civita et al., 1993)

A groundwater quality map was generated following the classification shown in **Table 4.51**. That classification was firstly suggested by Civita et al. (1993) and it is based mainly on European Council's guidelines. The production of the groundwater quality map was carried out through the overlapping of the thematic maps, which thematic maps are produced as a result of ordinary kriging interpolations as has already been presented at **section 4.7.2** of this chapter. ArcGIS Spatial Analyst extension was used for the creation of this map which was made only for October's data, because nitrate data was available only for that sampling.

For the total hardness, all the proposed classes of water quality (A, B, C) (**Table 4.51**) were existed at the water samples. Though, for the conductivity and chloride the B and C class existed, for the nitrate the A and B class, and finally for the sulfate only the B class. At last, after the above outputs manipulation, the derived groundwater quality map classifies the study area into 9 classes (**Fig. 4.126**).

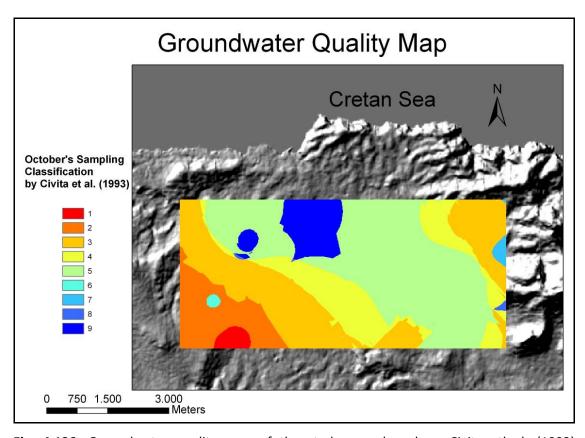
**Table 4.51:** Groundwater quality classification (Civita et al., 1993) (Total hardness units were transformed from mg  $CaCO_3/L$  to French units (°F =  $10mg\ CaCO_3$  per 1L water))

| Quality | Class | Total<br>Hardness | Conductivity | SO <sub>4</sub> <sup>2</sup> - | Cl <sup>-</sup> , | $\mathbf{NO}_3^-$ |
|---------|-------|-------------------|--------------|--------------------------------|-------------------|-------------------|
|         |       | (°F)              | μS/cm        | (mg/L)                         | (mg/L)            | (mg/L)            |
| Optimum | Α     | <30               | <1000        | <50                            | <50               | <10               |
| Medium  | В     | 30-50             | 1000-2000    | 50-250                         | 50-200            | 10-50             |
| Poor    | С     | >50               | >2000        | >250                           | >200              | >50               |

### 4.7.2.11.2 Ground Quality Index (GQI)

As already mentioned, the GQI was developed using seven chemical parameters ( $Ca^{2+}$ ,  $Mg^{2+}$ ,  $Na^+$ ,  $Cl^-$ ,  $SO_4^{2-}$ ,  $NO_3^-$ , and TDS). First Babiker et al (2007) applied the proposed index to Nesuno basin in Japan with great success, while next many applications globally were based on this index. In Crete, Kouli et al. (2008) applied GQI in Keritis river basin in the western part

of the island characterising the groundwater quality of the area, combining the same geochemical parameters.



**Fig. 4.126:** Groundwater quality map of the study area based on Civita etl al. (1993) classification (see **Table 4.51**)

Initially, "primary map I" (representing the seven concentration maps from **section 4.7.2** of this chapter) was used. Then, the measured concentration, X', of every pixel in the "primary map I" was associated with its corresponding WHO guideline value, X (**Table 3.6** of *Chapter 3*), by the following formula:

$$C = \frac{X' - X}{X' + X}$$
 Babiker et al (2007)

The "primary map II" (outputs derived as described above) display for each pixel contamination index values ranging from -1 to 1.

Next, primary map II was rated between 1 and 10 in order to generate the "rank map" using the following polynomial function:

$$r = 0.5*C^2+4.5*C+5$$
 Babiker et al (2007)

where, C represents the contamination index value for each pixel and r represents the corresponding rank value.

Afterwards, the relative weight (w) of each parameter had to be calculated as the mean value (r: 1–10) of the corresponding rank map and the "mean r + 2" ( $r \le 8$ ) for the parameter that has potential health effects, i.e. nitrate (**Table 4.52**).

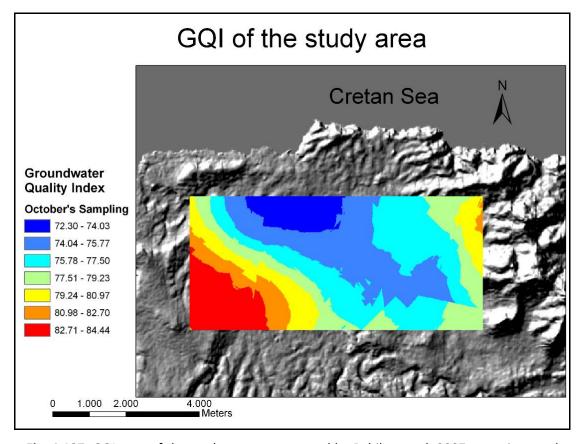
Finally, the GQI map (**Fig. 4.127**) concerning the seven chemical parameters was premeditated as follows:

$$GQI = 100 - \left(\frac{r_1 w_1 + r_2 w_2 + ... + r_7 w_7}{7}\right)$$
 Babiker et al (2007)

**Figure 4.127** shows the groundwater quality of the study area, created as described above. The extracted map gave groundwater quality values between 72.30 and 84.44. These values were classified into seven equal classes. Hot colours indicate the bad water quality, while the cold colours indicate the good water quality (maximum groundwater quality=100).

**Table 4.52:** Statistics of the seven parameters of groundwater quality from the study area for October's sampling

| and the state of t |      |      |                 |  |  |  |  |
|--|------|------|-----------------|--|--|--|--|
| Parameters   | Min  | Max  | Mean            |  |  |  |  |
| Calcium  | 2.66 | 3.55 | 3.16            |  |  |  |  |
| Magnesium  | 1.22 | 3.20 | 1.87            |  |  |  |  |
| Sodium   | 2.30 | 7.93 | 5.38            |  |  |  |  |
| Chloride   | 4.09 | 8.78 | 6.77            |  |  |  |  |
| Nitrate*   | 1.59 | 3.21 | 1.99 + 2 = 3.99 |  |  |  |  |
| Sulfate  | 3.09 | 4.41 | 3.83            |  |  |  |  |
| TDS*   | 5.19 | 7.79 | 6.71            |  |  |  |  |



**Fig. 4.127:** GQI map of the study area as proposed by Babiker et al. 2007, superimposed to the DEM. Hot colours indicate the bad water quality, while the cold colours indicate the good water quality (maximum groundwater quality=100).

### 4.7.3 Ion exchange

During seawater intrusion in a coastal aquifer two kinds of hydrochemical processes take place between fresh water and seawater and the aquifer, which influence the chemical composition of groundwater: a) mixing processes and b) ion exchange phenomena.

Mixing models have already graphically presented in previous sections. In Piper diagram (section 4.7.2.5 of this chapter), in Durov diagram (section 4.7.2.6 of this chapter), and in the dispersion diagrams (section 4.7.2.10 of this chapter), the mixing line has been drawn, joining the end members - fresh water ("sweet spring" sample location) and Aegean seawater.

On the other hand, apart from the simple mixing, the groundwater from coastal aquifers during seawater intrusion is strongly affected by cation exchange reactions. The type of unaffected fresh groundwater is  $Ca(HCO_3)_2$  while seawater is dominated by  $Na^+$  and  $Cl^-$  ions (NaCl type). When seawater intrudes into a coastal aquifer (containing fresh water), an exchange of cations takes place:

$$Na^{+} + \frac{1}{2}Ca-X_{2} \rightarrow Na-X + \frac{1}{2}Ca^{2+}$$

where X indicates the soil exchanger. The reaction shows that  $Na^+$  is received by the exchanger and  $Ca^{2^+}$  is released, while the dominant anion  $Cl^-$  remains the same. The reverse process takes place during freshening (Appelo and Postma book, 2005).

### 4.8 Summary

In this chapter, all the results that derived after the application of methodologies described at previous chapter were presented. Geomorphological and hydrological features (DEM derivatives) were presented first and preliminary results of RS analysis followed next. Then geophysical raw data (TEM and VES) were presented, and their processing, analysis and modelling were followed (1D modelling, 2D & 3D imaging). All the 15 geochemical parameters of the 3 water samplings were calculated as well, while statistical analysis tables, column graphs, and maps for each parameter were created. At the end, special interpretation of geochemical data took place (Piper, Durov, Stiff, Dispersion diagrams, molar ratios, quality maps, etc) for saline waters origin determination. The discussion chapter comes next, where an assessment of the relationship between all the results is given.

## [DISCUSSION]

### **Chapter Contents**

- Introduction to the discussion
- ► An assessment of the relationship between the geomorphology, rock types and structure
- ► An assessment of the water quality in relation to the physical characteristics of geomorphology and geology
  - Groundwaters Characterisation
  - Geochemical Processes
  - Quality Maps
- ► An assessment of the relationship between the physical & geochemical characters of the area and the geophysical surveys
  - o AB, CD, EF, FG, HI cross-sections
  - VES soundings
  - 3D TEM imaging + Groundwater Quality Maps
  - o Simple Hydrogeological Model
- **▶** Summary

### 5.1 Introduction to the discussion

The overall purpose of this thesis is stated in *Chapter 1* and repeated here for clarity:

The purpose is to apply geophysical and geochemical methods to a poorly understood area of limited groundwater resources, in order to determine the status of those resources used by an increasing local population.

This discussion is based around the objectives of the thesis and is arranged in subsections according to the primary questions stated in *Chapter 1*. These primary questions are repeated here for clarity:

- What is the relationship between the geomorphology, rock types and structure?
- What is the relationship between the water quality and the physical characteristics of geomorphology and geology?
- What is the relationship between the physical & geochemical characters of the area and the geophysical surveys?

## 5.2 An assessment of the relationship between the geomorphology, rock types and structure

Data provided in *Chapter 1-4* demonstrate the variable geomorphology of northern Crete, whereby the study area is downslope from the mountains, and therefore the Geropotamos River is fed by rainfall. However, beneath the surface, subterranean water flow to the north in the karstic system, carries freshwater to the aquifers on the northern coastal area. Since salination is an established fact of the geochemical measurements from *Chapter 4*, and is variable throughout the year, there must be an interplay of water pressure from the mountains and from the sea. Therefore, it is necessary to assess the relationship between the water flow from land and sea, in the context of the geomorphology, lithology and geological structure. An integral component of this is the potential impact of evaporite deposits in the study area, discussed below, along with the geological and geomorphological aspects.

It has previously suggested that evaporites (halites) were present in the study area (Knithakis, 1995; Region, 1999). There is the potential that salination of groundwater in part of the study area could be due to buried evaporites. However, the reason this was suggested derives from Lambrakis and Marinos (Lambrakis & Marinos, 2003) who drew attention to the presence to the Neogene evaporites in Greece. However, their work did not specifically include the study area. More focused work in the study area has revealed the following information:

- IGME report (Knithakis, 1995) records the presence of evaporites (halites) in the Neogene sediments only (section 2.3 of *Chapter 2*). From the theory, evaporites are created in basins, and cretan evaporites were due to Mediterranean salinity crisis during the Messinian Stage of the Tertiary Period (section 2.4.2 of *Chapter 2*).
- There is also a problem with the groundwater quality in the north-eastern part of the area too, consisting of dolomitic limestones and dolomites. Although dolomite is well known to be associated with the formational processes of evaporites in some modern environments (such as the Coorong in Australia), in most cases dolomite is a later alteration product of limestones, unrelated to the surface environments where Neogene evaporites form (Tucker and Wright, 1990). Therefore, water quality problems related to dolomite are more likely linked to diagenesis of limestones later in geological history, not controlled by the Earth surface environments where evaporites develop.
- All the evaporites found in Crete are gypsum, the other major evaporite minerals
  often associate with gypsum have never been found. It is possible that halite was
  dissolved out of the rock formations, and removed from the system.
- All the data that have been collected in this study (data from borehole logs) have not revealed the presence of evaporites in any of the boreholes.
- The locations in the Neogene sediments which do have salt water are located near the sea or close to the major faults in the eastern part of the study area.
- In the SW of the study area the Neogene sediments yield very good quality water from those sediments.

There are 3 possible scenarios to explain the pattern of the saline water in the study area:

**Scenario 1**: seawater intrusion, **Scenario 2**: evaporites (halites), **Scenario 3**: combination of seawater Intrusion and evaporites.

The sum of these points shows that the only places that saline water affects the aquifer is the northern part of Geropotamos basin where seawater could be intruding. The lack of evaporites in the Neogene sediments in the southern part of the basin is strong evidence that evaporites do not exist in the study area. Note however that evaporites (gypsum) exist in the neighbouring basin west of the study area shown on **Figure 2.10** of **Chapter 2**. Overall, this analysis leads to the deduction that there is good evidence that saline water problems in the aquifer are due to seawater intrusion and not due to evaporite dissolution and therefore considered the most likely.

As described above the most likely scenario is the seawater intrusion rather than evaporite existence, due to the reasons that described previously. In this section, five kinds of datasets are cross-compared in order to test this deduction. IGME geological map, data that collected through field geological observations, information from the available borehole logs, hydro-lithological map, and lineaments extracted after remote sensing analysis are combined to lead to the conclusion that salt water is entering the aquifer from faults that extend inland from the coastline.

Geological map of IGME, that was the only available source of knowledge concerning the geology of the study area, gave valuable information about the rock types and structure. As described in **section 2.2.4** of *Chapter 2*, the northern part of Geropotamos basin consists mainly of dolomitic limestones and stromatolites (Plattenkalk nappe), and phyllites/quartzites (Phyllite/Quartzite nappe) covered by Neogene and Quaternary sediments, while the tectonic setting is characterised by NW-SE and NE-SW direction faults and thrusts.

The information derived from IGME map (see previous paragraph), and particularly the main units and the major thrust fault between plattenkalk and phyllite/quartzite nappes at the north-eastern part of the study area, was verified after the short geological fieldwork in February of 2008 (section 4.5 of *Chapter 4*).

Borehole log information that was provided by local authorities gave valuable data about the lithology of the study area, which was also used for geological cross-sections construction (section 4.5 of *Chapter 4*). Apart from that, those borehole registration forms included information about the static water level and pumping level of most of the boreholes (*Appendix A*).

Hydrolithological classification of the geological units based on permeability was based on previous study from Regional Governor of Crete (1999) as described on **section 2.3** of *Chapter 2*. So, along with that classification the northern part of Geropotamos basin (where the phyllite/quartzite nappe lies) is characterised as almost impermeable formation (I2), whereas the eastern and southern part (dolomitic limestones and stromatolites) of the area showed to consists of permeable formations (K1).

To sum up, the previous data show that there is an impermeable formation along the coastline (phyllite/quartzite nappe) which probably consists a barrier to seawater to come inland. This option seems to be in contrary with the seawater intrusion scenario that seemed to be the most likely. Tectonic setting is a very important factor that supports the scenario of seawater intrusion, where the faults are identified as the major potential conduits of water flow into the aguifer.

Hence, as the tectonic features seem to be the key point, remote sensing analysis was attempted for photolineaments detection, indicating possible faults (section 4.4 of *Chapter* 4). The lineaments detected in the Landsat-ETM band 5 image (after filtering) can be correlated with the tectonic setting of the study area as described at previous section and some of them correspond to faults documented in the IGME geological map, while some others are presented in this thesis for the first time. The preliminary structural patterns obtained by remote sensing analysis, seems to reflect the actual distribution and orientation of the major tectonic features in the study area since they do not coincide with the road network. However, this is a preliminary work and in order to certify these assumptions, identification of these possible faults in the field is needed in the future.

Consequently, the apparent section showed the close relationship between the geomorphology, rock types and structure, and at the same time the uncertainty of **scenario 1** was decreased, and it seems to be the most probable.

# 5.3 An assessment of the water quality in relation to the physical characteristics of geomorphology and geology

Three water samplings (June, July, and October 2008) accomplished in 24 sample locations (22 boreholes and 2 springs within the study area), as described in **section 4.7** of *Chapter 4*, and 15 chemical quality parameters were measured in order to check the quality of the waters and to identify their contaminator. Geomorphological and geological information (physical characteristics) showed so far that scenario 1 (see **section 5.2**) is the most possible. Further down follows a detailed description that proves the excellent relationship between the geochemical analysis and physical characteristics, and provide evidence that seawater intrusion is the contaminator of northern Geropotamos basin.

Initially, chemical parameters will be discussed first and then special chemical interpretation follows (special diagrams, quality factors, etc). For each parameter column graphs, tables of statistical analyses and spatial distribution maps were constructed (section 4.7.1 of *Chapter 4*). Note that June's sampling was a pilot sampling and only 10 samples were analysed. Therefore, due to the low number of available data distribution maps were not extracted. Moreover, two tables of statistical analyses exist (one including all the samples of each sampling) and a second one including just the same 10 samples for direct comparison of the statistics for each sampling.

Values of parameters strongly related to seawater presence, such as Electrical Conductivity (EC), Total Dissolved Solids (TDS), and Sodium concentrations, show a relatively high correlation as can be seen in **section 4.7.1** of *Chapter 4*. The increasing values of those parameters in our samples strongly support the hypothesis of seawater intrusion in the study area (**Fig. 5.1**). Other parameters such as Potassium, Chloride, Boron concentrations in general follow the special spatial distribution of the aforementioned parameters and their values in the samples we analysed are in correlation with them and they support the

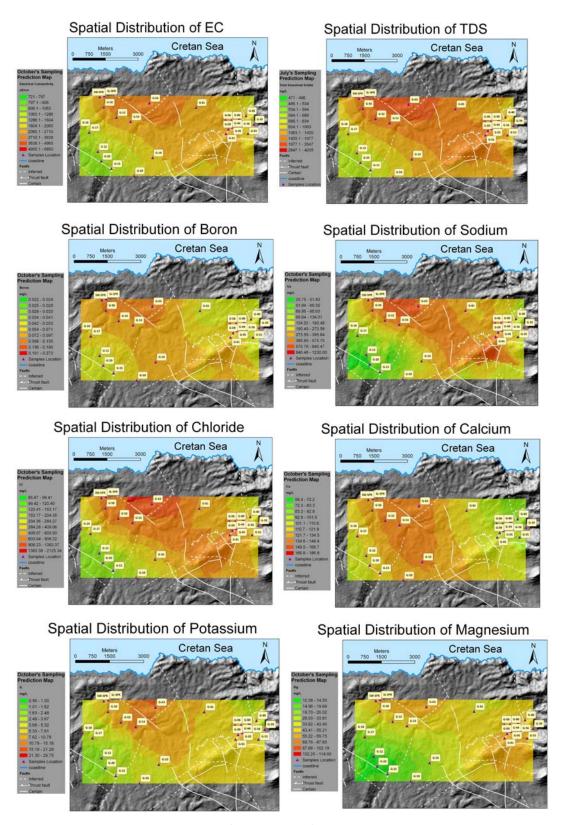
hypothesis of seawater intrusion too (**Fig. 5.1**). It is not worthy mention that we didn't observe values of the above-mentioned parameters in any of our samples which oppose this hypothesis. The values of the parameters analysed are not affected from any substantial anthropogenic activities (e.g. fertilizers, animal stock production), since sensitive parameters such as Nitrate and Phosphate concentrations show low and zero values respectively.

#### **Groundwaters characterisation**

Groundwaters of the study area were classified according to their geochemical characteristics based on the dominant ions (cations and anions) as listed in **Table 4.4.3** on **section 4.7.2.2** of **Chapter 4** and based on ternary diagrams of **section 4.7.2.3** of **Chapter 4**. Three groundwater types are recognised: NaCl, CaCl<sub>2</sub> and Ca(HCO<sub>3</sub>)<sub>2</sub>, and their spatial distribution is shown in **Figure 5.2** (Kriging water types). The SO<sub>4</sub> and Mg concentrations are normally very low. Stiff diagrams and map is a good way to visualise this information (**Fig. 5.2**).

Therefore, groundwaters in the north-central part of the study area near the coastline belongs to NaCl, which are under the influence of seawater intrusion, while groundwaters in western and eastern part belong to Ca(HCO<sub>3</sub>)<sub>2</sub> type, which it is considered as the fresh waters of the area. Between the two zones, a thin region of CaCl<sub>2</sub> type groundwater exists which is considered as the transition zone and it is probably produced from cation exchange as it will be discussed later.

As mentioned above, boreholes containing NaCl type of water are situated at the north-central part of the study area and close to seashore. These are the same boreholes which showed high EC values, and salinity, TDS, and calcium concentrations, which resulted from seawater intrusion (Fig. 5.1).



**Fig. 5.1:** Six chemical parameters from October's sampling showing seawater intrusion as the most likely contaminator of the study area groundwaters

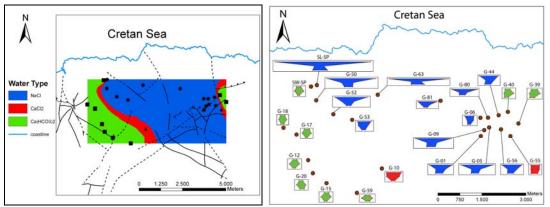


Fig. 5.2: a) Spatial distribution of groundwaters of the area after Kriging, and b) stiff map, for October's sampling

#### **Geochemical Processes**

As mentioned in **section 4.7.3** of **Chapter 4**, during seawater intrusion in coastal aquifers two kinds of hydrochemical processes take place between fresh water and seawater and the aquifer: a) mixing processes and b) ion exchange phenomena.

#### - Mixing Processes

The mixing between the fresh and seawater in the northern Geropotamos aquifer system is reflected initially in the Piper and Durov diagrams for October's sampling. Then 5 kinds of dispersion diagrams (Na-Cl, Ca-Cl, K-Cl, Mg-Cl, SO<sub>4</sub>-Cl) were constructed and finally 4 quality factors (Na:Cl, Ca:Mg, Cl:HCO<sub>3</sub>, SO<sub>4</sub>:Cl) were applied for all the samplings (except Cl:HCO<sub>3</sub>). For all the aforementioned calculations, sample from the sweet spring was used as the representative freshwater end-member, and seawater from Aegean Sea was used as seawater end-member (section 4.7.2.1 of *Chapter 4*) for representative results.

Piper diagram (Fig. 4.97 of *Chapter 4*) is in agreement with the theoretical image from Appelo and Postma (2005) (Fig. 4.96) which gives an average composition of fresh water and seawater. It shows all 24 samples as well as the theoretical freshwater-seawater line of mixing. All the samples lie very close to the mixing line, with only minor deviations.

Additionally, the Durov diagram (**Fig. 4.98** of **Chapter 4**) undoubtedly shows also a trend of samples to plot diagonally of the diagram, indicating the mixing phenomena between endmembers.

So, it is deduced from the Piper and Durov diagrams that the most important hydrochemical process in the groundwaters is the mixing. This is confirmed next as concentrations of various cations (Na $^+$ , Ca $^{2+}$ , K $^+$ , Mg $^{2+}$ ) and SO $_4^-$  are presented as a function of the chloride (dispersion diagrams). Cl $^-$  is regarded as a conservative ion, and therefore represents the proportion of the mixture (section 4.7.2.9 of Chapter 4). Almost all samples showed strong correlation coefficient R (0.80-1) of regression lines (red solid lines), and all seem to coincide well with the freshwater-seawater mixing lines (red dotted lines), proving their common origin (seawater).

**Figures 4.103, 4.104** & **4.105** demonstrate that there is seawater influence of the waters with respect with sodium for all samplings (June, July, October), as the correlation factor R has a value about 0.99 (almost perfect correlation). The same for all the samplings of potassium and magnesium (R values about 0.95) (**Figs. 4.109 - 4.114**).  $SO_4^-$ -Cl dispersion diagrams (**Figs. 4.115, 4.116** & **4.117**) of all samplings show also that ions have the same origin (R=, however small declinations from the mixing line perhaps are due to redox processes of  $SO_4^-$  ions (Panagopoulos, 2008). Therefore, all the aforementioned elements derive from mixing processes of the end members (freshwaters-seawater), while the ion exchange phenomena are not so intensive.

Factors controlling groundwater quality (ionic ratios:  $Na^+: Cl^-, Ca^{2+}: Mg^{2+}, Cl^-: HCO_3^-, SO_4^{2-}: Cl^-)$  with respect to the influence of seawater were also applied and their ranges are shown in **Table 4.46** (section **4.7.2.10.1** of *Chapter 4*). Then the calculated above-mentioned molar ratios were graphically presented versus  $Cl^-$  concentrations (except  $Ca^{2+}: Mg^{2+}$ ).

**Table 4.46** shows that Na<sup>+</sup>: Cl<sup>-</sup> ratio values less than 0.82 (seawater ratio) indicate fresh water contamination by seawater. For June's and July's samplings **all** Na<sup>+</sup>: Cl<sup>-</sup> ratios have values below that threshold, which indicates the high influence of seawater in the groundwaters (even for good quality waters) (**Table. 4.47**). However, in October's sampling, sodium concentrations were increased very much, while chloride concentrations were remained almost the same in comparison with June and July (**Table. 4.47**). This fact had as a result the jump of the molar ratios for that sampling, with values near the seawater ratio, 0.82 (about ±10%). The key point here is that on October the simple mixing between

groundwaters with seawater was very recent (Mercado, 1985; Lee and Song, 2007), which influenced all the sample locations.

#### - Cation exchange phenomena

As described in **section 4.7.3** of *Chapter 4*, when seawater intrusion takes place, due to cation exchange, Ca<sup>2+</sup> are released, while Na<sup>+</sup> are received by the soil exchanger. Nevertheless, increase in Na<sup>+</sup> concentrations took place in October, as mentioned above which is normal as the groundwaters molar ratios reach the seawater ratio (0.82) and indicate the recent water intrusion into the area. This seawater encroachment is so recent that no extended cation exchange phenomena have taken place yet along with mixing processes (as occurred in June and July). This also supports the hypothesis that seawater is the contaminator in the study area because in October the aquifer is expected to be in its most stressed condition due to extended dry season and high water pumping rates, especially for irrigation purposes. So, the seawater intrusion should be very recent for that period.

#### **Quality maps**

Quality maps showed great relationship between physical characteristics and geochemical analyses as well. Both approaches of groundwater quality maps, one based on Civita et al. (1993) classification and the other based on WHO guidelines, locate the northern-central part of the area near the seashore as contaminated, which it is also in agreement with scenario 1. The same maps will be discussed again later for comparison with the TEM 3D imaging maps. To sum up, geochemical approach decrease much more the uncertainty of which is the contaminator in the northern part of Geropotamos basin, and complements scenario 1, which regards seawater as the only source of contamination.

# 5.4 An assessment of the relationship between the physical & geochemical characters of the area and the geophysical surveys

In **sections 5.2** evaluation of all the available data, concerning the physical characteristics of geomorphology and geology of the study area, was accomplished, while in **section 5.3** the correlation between those characteristics with chemical results is described. The majority

of the data lead to the interpretation that seawater encroachment takes place at the northern part of Geropotamos and contaminates the fresh groundwater of the area. Of course all this information is surfacial information, while data from boreholes (lithology and chemical analyses) are relatively not many and not very good distributed. Geophysical survey, which comprises from a dense grid of TEM soundings covering all the area under study, and some VES soundings taken in selective places, was used as a tool in order to give information for the deeper geology (rock types, tectonics) and hydrogeology (aquifer characteristics) of Geropotamos area. Description of TEM and VES results and their good relationship with the previously discussed results follows, attesting that seawater intrudes, through faults that extend inland, and contaminates the groundwater.

Although TEM and VES geophysical techniques are considered as very innovative and capable for deep investigations, it is necessary their results to be combined with other data, such as chemical and geological/geomorphological (section 5.3). Note that, because the area is very complex, for better understanding, only 2D and 3D TEM extracted geoelectrical graph models are discussed. It is reminded that for the construction of those 2 kinds of models, only 1D inversion results were used (section 4.6.1.3 of *Chapter 4*).

#### AB, CD, EF, FG, HI cross-sections

Five geological cross-sections were constructed (**section 4.5** of **chapter 4**), while at the same positions five TEM profiles were created having the same 3x exaggeration and the same length for easier comparison between them. However, some differences in relief maybe appear due to the fact that for geological cross-sections construction a straight line on the surface was chosen using dense information from DEM, but for the TEM profiles the scarce elevation information from each sounding (from GPS) only was used for the relief. In addition each 2D geoelectrical model is a crooked line (**Fig. 4.33** of **Chapter 4**) and not a straight line like each geological cross-section.

As it is presented below, 2D geoelectrical models are in good correlation with the geological cross-sections concerning the recognition of the nappes (especially phyllite/quartzite nappe with plattenkalk nappe) and confirmation of faults. In addition, 2D geoelectrical models

give information about the permeability of the rocks (conclusively phyllite/quartzite nappe is not impermeable) and the aquifer characteristics (saturation, water table depth and contamination). AB and HI cross-section examples are described next in more detail since they are the most representative.

AB cross-section is 9 km long and has NW-SE direction and it comprises the two major units (Plattenkalk and phyllite/quartzite nappes) covered by the Neogene and Quaternaty sediments. Plattenkalk unit (presented in purple colour) is recognised at the south-eastern part of the profile (Fig 5.3) with resistivities greater than 1000 ohm.m (as expected). Phyllite/quartzite nappe is defined very well in the north-western and central part of the profile with resistivities generally about 100 ohm.m and sometimes in places up to 300 ohm.m, when the nappe is rich in quartzite. Sediments which are composed by marly limestones, marine and alluvial deposits, clays, etc have resistivities ranging from 100 to 500 ohm.m, and occasionally, when Neogene limestones are more cohesive and stiff, the resistivities are even more increased up to 1000 ohm.m. Generally, the sediments are not recognised clearly over phyllite/quartzite nappe (Fig. 5.3), since the resistivity values overlap (Table 5.1).

The thrust fault between phyllite/quartzite nappe and plattenkalk nappe is observed in AB geoelectrical model, which its position and direction are verified by the geological cross-section. Additionally, the transition zone between them is recognised with resistivity values between the values of the two nappes (Fig. 5.3).

As already mentioned, phyllite/quartzite nappe is considered almost impermeable, except if faults then these could be major potential conduits of water flow inland. The northwestern part of AB 2D geoelectrical model (**Fig. 5.3**) shows undoubtedly the seawater encroachment and complements scenario 1 (**section 5.2**). It illustrates the low resistivity values (blue colour) situated into the phyllites/quartzite nappes 20m under the surface extending up to 1.7 km inland and it is considered as the strongest evidence for scenario 1.

Two different types of aquifer expected based on rock types. Sediments are expected to host a phreatic aquifer (G-63 and G-81 are evidence) which lie above phyllite/quartzite unit.

The problem is that resistivity values overlap (**Table 5.1**) and it is hard to separate them, which is part of the limitation of geophysics. Deeper aquifer is expected to be found in discontinuities (fracture zone in Phyllite/quartzite nappe or karst in plattenkalk unit). A fracture zone ( $1^{st}$  left black colour ellipse) seems to appear which probably acts as a conduit (e.g. a fault) for seawater encroachment into aquifer. The  $2^{nd}$  ellipse in the middle most likely represents the seawater intrusion through the thrust zone. The deeper aquifer (maybe a little influenced by seawater) is recognised in the dolomites with resistivity values greater than 10 ohm.m, while underneath there is brackish water ( $\approx 1$  ohm.m) probably originating from seawater which intrudes though faults from the north-eastern part of the seashore ( $3^{rd}$  ellipsis). Many boreholes through the Plattenkalk nappe with relatively high pumping rate (**Appendix A**) confirm the existence and the amount of groundwater.

In order to show that the low resistivities that appear (indicated by the three ellipses) are not artefacts but good quality data, resistivity curves and 1D inversion models are illustrated only for those soundings (Fig. 5.3). All models (low rms) present that conductive layers ( $\approx 1$  ohm.m) lie below, which complement scenario 1. Note that 0264 and 0246 TEM soundings, were measured in different units (phyllite/quartzite nappe and plattenkalk nappe respectively), and the difference in their responses (different resistivity values for the upper layers) permits recognition of different rock formations. However, both measurements recognised groundwater existence (low resistivity values), as well as its different quality characteristics (brackish water underneath fresh water).

CD, EF and FG geological cross-sections cross mainly above sediments, superimposed to phyllite/quartzite nappe, which their thickness has approximately estimated by the available data (geological map and borehole logs). CD and EF are 4 km long, while FG cross-section is 7 km long having NW-SE, NNW-SSE and SSW-NNE directions respectively. Their 2D geoelectrical models (juxtaposed 1D inversion models) (Fig. 4.35f, 4.36f & 4.37f) demonstrate that the resistivity values of these sediments vary depending on the rock types from 100 to 500 ohm.m (Neogene limestone, clays, gravels, etc); however when Neo-

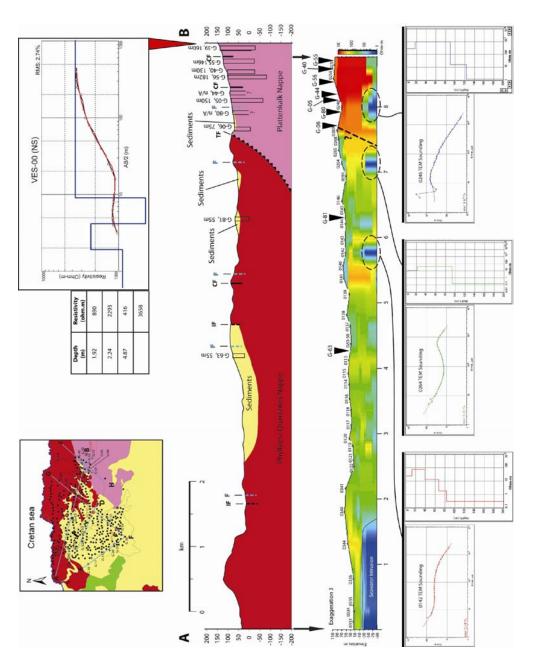


Fig. 5.3: AB geological cross-section in comparison with the 2D geoelectrical model and VES-00 sounding

gene limestones are more cohesive and stiff, the resistivity values are even more increased up to 1000 ohm.m. Generally, due to resistivity values overlapping between phyllite/quartzite nappe and sediments, it is hard to distinguish them. Boreholes confirm that there is groundwater in sediments, which is confirmed by TEM data, where the recharge zone is defined with resistivity values 10-40 ohm.m. Low resistivity areas at deeper layers are evidence for fracture zones in the phyllite/quartzite nappe. These zones are conduits for seawater intrusion, and consequently contamination of the groundwater (low resistivity areas shown with blue colour).

Finally, the HI geoelectrical model is a small part (4 km long) of *HI* geological *cross-section* and crosses only the plattenkalk nappe, which is obvious from the high resistivity values which indicate the dolomites and dolomitic limestones. TEM technique is very good for identifying conductive zones underneath more resistive layers (in contrary with VES soundings). The aquifer system is clearly identified. The water table (60m-100m from the surface) and the interface (mixing zone) between fresh and brackish waters (beginning from 110m) are depicted in Figure 5.4 (black thick dashed lines). The aforementioned hydrogeological status is supported by the big number of boreholes with high pumping rate (greater than 100 m³/h, *Appendix A*). Since the depth of the boreholes is close to mixing zone (as described above) the quality of their waters appears slightly affected (section 5.3). Specifically, the contamination zone is situated lower, mainly below G-44. Based on this interpretation, this particular borehole is considered the most vulnerable to saline intrusion problems.

The resistivity curves and 1D inversion models of three TEM soundings (0254, 0253 and 0244) are given (as we did for cross-section AB) in order to enforce the hydrogeological model that assumed previously. Specifically, these three TEM soundings were presented in order to show the good quality of data (low rms), as well as the similarity between their resistivity values. The depth models of each sounding appear slight differences between them, where the aquifer system is mapped (see text above). For that reason, TEM technique can be used as an effective tool for monitoring of the seasonal changes of the aquifer system (seawater intrusion) by applying time lapse measurements.

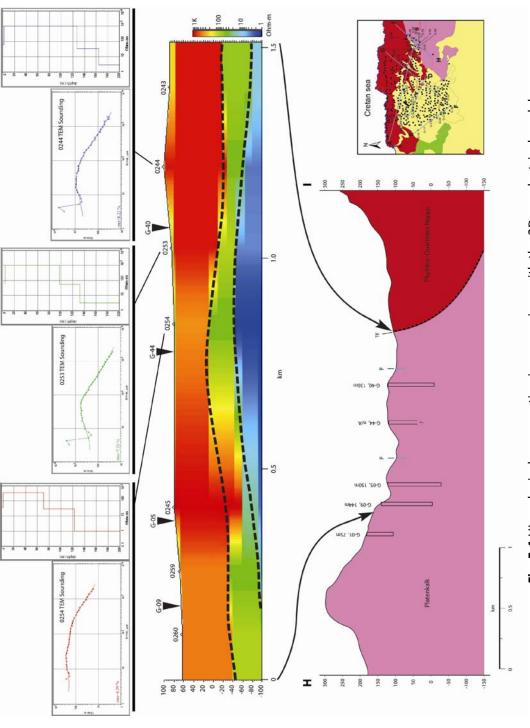


Fig. 5.4 HI geological cross-section in comparison with the 2D geoelectrical model

#### **VES** soundings

In **section 4.6.2** of **Chapter 4**, resistivity data acquisition was described, where 3 VES soundings took place in three different environments: a) VES-00, on plattenkalk nappe (dolomitic limestones), b) VES-01, on sediments, and c) VES-02 on the contact between sediments and Phyllite/quartzite nappe. For VES-01 and VES-02 multidirectional measurements took place (NS and WE direction), whereas two small TEM profiles (25 x 25 m loop size for better resolution near surface) are created as well crossing through VES soundings for direct correlation. The results of each sounding are discussed next.

**VES-00 sounding** is situated at the end of AB cross-section (**Fig. 5.3**). This means that it took place on dolomitic limestones at Maniaki area, where TEM technique had SPM effect and no reliable data were acquired (**section 4.6.1.2** of **Chapter 4**). Moreover, no multidirectional measurements accomplished (only NS direction), because there was not enough space in the WE direction. As shown in **Figure 5.3**, the first thin layer (2m thick), with resistivity about 800 ohm.m, represents the weathered surface. This is probably the "terra rossa", which was referred to in **section 4.6.1.2** of **Chapter 4** and probably, due to the fat that it is rich in magnetite material, creates the SPM effect in TEM data. The next layer represents dolomitic limestones, which has values varying from 2293 to 2650 ohm.m. Note that a probable fracture zone lies at 5 meters depth with resistivity 416 ohm.m, as it contains groundwater.

**VES-01** is situated at the southern part of FG cross-section (**Fig. 4.26** of **Chapter 4**) on the sediments. Measurements in both directions (NS and EW) showed similar results: the first very thin layer (1.6 m thick) is followed by a less resistive layer (up to about 20m depth), which finally is followed by a resistive layer (**Fig. 4.43** & **4.44** of **Chapter 4**). The small TEM profile with WE direction (**Fig. 4.45** of **Chapter 4**) showed exactly the same results, that is the phreatic aquifer.

**VES-02** is situated at the eastern part of CD cross-section (**Fig. 4.26** of **Chapter 4**). This site is on sediments, very close to the contact between phyllite/quartzite nappe with sediments. It was chosen in purpose and multidirectional measurements took place. VES-02 with NS

direction had good results. In the contrary, the resistivity curve of VES-02 (with WE direction), is problematic as the last measurement points (when during measurement the eastern electrodes was very close to phyllite/quartzite nappe) showed extremely big values (Fig. 4.47). When these points removed, the model showed similar results with VES-02 with NS direction. Small TEM profile (Fig. 4.48 of *Chapter 4*) with WE direction shows clearly the contact.

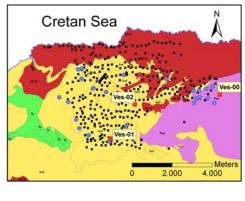
**Table 5.1:** Values of resistivity for different geological materials and groundwaters of the study area as concluded after geophysical data interpretation (TEM and VES)

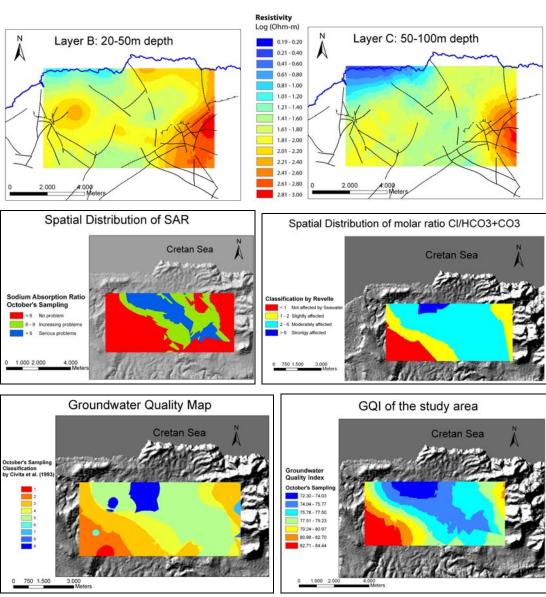
|                          | Rock Material  | Resistivity<br>(ohm.m) |
|--------------------------|--|------------------------|
| Quaternary sediments     | - Alluvial deposits (Q2)<br>- Marine deposits (N2-Q1)<br>- Limestones, Marls, Clays, Conglomerates (N1-N2) | 100-500                |
| Neogene sediments        |  |                        |
| Phyllite-Quartzite nappe | - Phyllites, quartzites and orthorocks (C3-T3)   | 100-300                |
| Plattenkalk nappe        | - Dolomites and dolomitic limestones (T3-J1) - Banded recrystallized olomitic stromatolites (C3-T3)        | >1000                  |

|                | Resistivity (ohm.m) |
|----------------|---------------------|
| Fresh water    | 10-40               |
| Brackish water | 0.1-10              |

#### 3D TEM imaging + Groundwater Quality Maps

In previous paragraphs, 2D geoelectrical models were discussed, where information about rock types, tectonics and aquifer characteristics were successfully identified. As described on **section 4.6.1.3.3** of *Chapter 4*, four 3D geoelectrical resistivity layers were constructed: Layer A (0-20m depth), layer B (20-50m depth), Layer C (50-100m depth) and Layer D (100-200m depth) in order to give some extra information about the surficial geology (rock types and general tectonic regime) and aquifer characteristics as well. Therefore, the upper Layer A can be correlated with the surficial geological setting, that's why a layer with the geology is overlain. Layers B and C are compared with the geochemical data (as 20-100m is the depth which boreholes mainly pump from), and Layer D shows clearly the contamination. Note that all chemical maps cover a smaller area than TEM resistivity maps.





**Fig. 5.5**: Layers B and C (upper images) are compared with the four chemical maps, extracted as described in *Chapter 4* (lower images), showing the same results (see text for details).

**Figure 4.39a** of *Chapter 4* depicts Layer A with geology, in which they are in great agreement. At the eastern part, high resistivity plattenkalk nappe is shown, while sediments and phyllite/quartzite nappe have almost the same resistivity values. There is no evidence of contamination, but in the contrary the phreatic aquifer is shown in the central and southern part (Quaternary deposits and Neogene limestones, respectively). This is in agreement with the information from locals saying that at that at those specific areas there are plenty of shallow wells with good quality water.

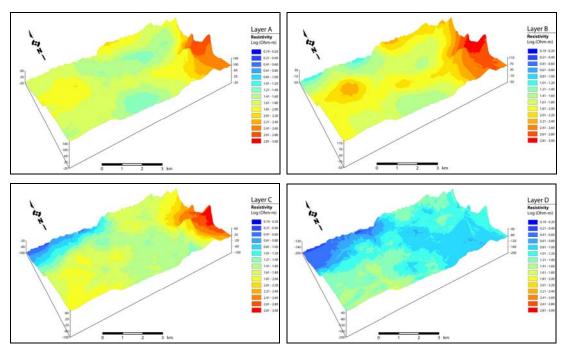
As it is already mentioned on **section 2.3** of *Chapter 2*, two aquifers are expected in the area (phreatic and deep), where from log information (Appendix A) the pumping level ranges mostly between 20-100m depth. For this reason, chemical maps (groundwater quality maps, SAR, Revelle, and EC) are correlated with Layers B and C. At both B and C layers plattenkalk nappe was recognised (high resistivity values) at the eastern part. At the most south-eastern part, the values are not representative because there is no TEM data coverage, but these values are given after interpolation of resistivity data (ordinary kriging). Actually, these values are expected higher. The same situation in the phyllite/quartzite nappe at the north-eastern part, the coverage is not adequate. So, probably some contamination from the sea through the fault (Fig. 5.5., Layer C) it is not depicted. On the contrary, in the north-western part (especially for Layer C) 50m below surface the most reasonable interpretation is that seawater intrudes inland. Except for contamination areas (where the resistivity measurements are not reliable), the same resistivity values exist for this nappe, as described earlier at 2D TEM interpretation (Table 5.1) which overlap with sediment resistivity values.

Layer D gives information about the size and geometry of contamination. Specifically, the south-western part of the 3D model seems unaffected from seawater. The north-eastern part of the area seems not contaminated as well, but (as mentioned above) no TEM measurements are available, and maybe seawater encroaches and contaminates plattenkalk nappe at the eastern part. Finally, a graben with NW-SE direction crosses the study area and it is envisaged here to be a major conduit for seawater.

Despite the fact that the sample locations are not well distributed, all chemical maps show similar results and they are in agreement with geophysical data interpretation i.e. they show contamination near seashore which extends inland. It is worth saying that Electrical Conductivity map from chemical analysis (Fig. 5.1) is in great spatial distribution agreement with the resistivity (inverse conductivity) layer C from TEM data interpretation.

#### Simple Hydrogeological Model

The four resistivity layers (Layer A: 0 - 20 m, Layer B: 20 - 50 m, Layer C: 50 - 100 m, Layer D: 100 - 200 m) that described in previous section (interpolated maps of TEM resistivity values in different depths) are represented with heights obtained by DEM showing the relief of the study area. These images mainly were constructed in order to make clear the physical mechanism of the seawater intrusion (section 2.4.1 of *Chapter 2*). From the physical point of view seawater intrusion cannot be occurred above the sea-level, so the NW part of the study area was contaminated firstly through fracture zones (low elevation), while the contamination of the SE part of the study area is shown only in Layer D approximately 80m below sea-level.



**Fig. 5.6**: The four resistivity layers (Layer A: 0 - 20 m, Layer B: 20 - 50 m, Layer C: 50 - 100 m, Layer D: 100 - 200 m) with heights obtained by DEM showing the relief of the study area.

Finally, it should be discussed how the results of this thesis relate to studies from other areas. Two places were selected to show general similarities and differences with Geropotamos study area, as they are considered as the most representative: the coastal strip of Israel and the coastal Rhodope area (north-eastern Greece). Of course, it is important to repeat that the northern part of Geropotamos was studied scientifically for the first time, while the Israeli coast and Rhodope aquifer system have been examined for many years. On the other hand, it is intended, like Goldman M., Kafri U. and Melloul did for their area (Israel), to continue TEM surveys, in order to cover more area of the Cretan coasts. In addition, the chemical analyses of groundwaters will be continued (like Petalas et al. did in north-eastern Greece), while more sampling points will be added. Therefore, the continuation of this project will be a good attempt for the seawater intrusion problem of Crete Island delineation.

In the Literature Review Chapter (section 2.5.1 of *Chapter 2*) a short reference at the seawater intrusion mapping the last 25 years by Goldman M., Kafri U. and Melloul A. in Israel was made (e.g. Goldman et al, 1988; Melloul and Bibas, 1991; Kafri et al., 1997; Goldman and Kafri, 2002; Kafri and Goldman, 2006; Kafri et al., 2007). They use mainly TEM technique making extensive surveys, covering the almost the whole Mediterranean coastal strip of Israel. At the same area Sivan et al. (2004) sampled saline and brackish groundwaters from the Israeli coastal aquifer in order to quantify the geochemical processes and the timescale of seawater intrusion into a coastal aquifer. At both places TEM technique and chemical analyses showed seawater intrusion to be the only contaminator of the groundwaters. In addition, for both places information from existed boreholes were used, which in conjunction with the results of the TEM surveys, the coastal aquifers were delineated successfully. Detailed chemical analyses by Sivan et al. (2004) that took place in Israel were independent from geophysical surveys, while for our case study in this thesis the two different approaches were done concordantly, and the results were directly compared.

Concerning Rhodope aquifer, repeated hydrogeological and hydrochemical investigations from Petalas et al. the last decade (Petalas et al, 1999; Petalas & Lambrakis, 2006; Petalas et al. 2009) have shown the origin and distribution of saline groundwaters in the coastal

area, illustrating the large extent of seawater intrusion in the Rhodope aquifer system. Using the same special interpretation of geochemical data, as it was used for Geropotamos area (dominant ions, Piper diagram, Durov diagram, ion exchange etc), they managed to characterise the groundwaters and determine the chemical processes. Even though Petalas et al. mainly combine the field observations with geochemistry, without using any other methodologies (e.g. geophysics), they were able to safely lead to better explanation of the origin of saline waters, proving one more time that geochemical data are a very effective tool for these kinds of salinity problems.

#### 5.5 Summary

In this section, the results from *Chapter 3* were discussed and the objective questions that were posed on *Chapter 1* were answered. Tectonic setting is the key point and supports the scenario of seawater intrusion, since the faults seem to act as conduits for seawater encroachment into aquifer. It showed that this state is in agreement with the results of the chemical analyses and their special interpretation. Then it was discussed the great relationship between the physical characteristics of geomorphology and geology with geophysical 2D and 3D geoelectrical models, as well as with the geochemical characters, decreasing the uncertainty of this assumption even lower. Therefore, there is a strong set of evidence which showed that all the quality problems are due to seawater intrusion and not evaporites.

# [CONCLUSIONS]

### **Chapter Contents**

- **▶** Introduction
- **▶** Conclusions
- ► Perspectives (Suggestion for future work)

#### 6.1 Introduction

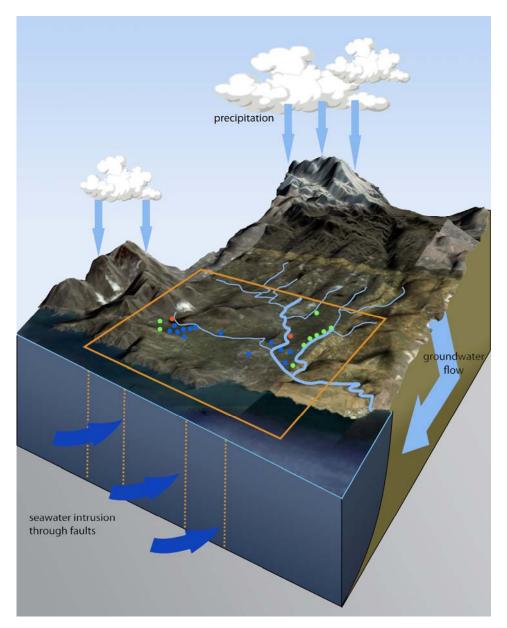
This chapter summarizes the major outcomes of the research and explains to what extend the aims have been achieved. In evaluating the relative strengths and weaknesses of the study, we need to consider one more time the key questions that have already been discussed at the previous chapter:

- What is the relationship between the geomorphology, rock types and structure?
- What is the relationship between the water quality and the physical characteristics of geomorphology and geology?
- What is the relationship between the physical & geochemical characters of the area and the geophysical surveys?

#### 6.2 Conclusions

The conclusions of this study are catalogued here:

1. The evidence presented in previous chapters is best interpreted that the saline water is due to seawater intrusion. This disproves previous work. Figure 6.1 shows a simple diagram of the Geropotamos drainage basin which combines together all the aspects of this thesis. Hence, during the winter period precipitation (mainly snow and rain), falling mostly in the mountains (Psiloritis Mountain and Talea Ori Mountain), either runs off surficially (creating Geropotamos River), or soaks into the ground as infiltration (replenishment of deep aquifer - plattenkalk nappe, or phreatic aquifer - Neogene sediments). During summer season, seawater intrudes inland through faults with NE-SW direction (dashed orange colour lines), contaminating the freshwater. Blue points indicate the boreholes with NaCl water type, red points the boreholes with CaCl<sub>2</sub> water type, while green points the boreholes with Ca(HCO<sub>3</sub>)<sub>2</sub> water type.



**Fig. 6.1**. Schematic three-dimensional reconstruction of the dynamics of the study area; see text for explanation.

2. Evidence that groundwater of Geropotamos aquifer has already been contaminated by seawater encroachment is presented in this thesis. Winter rainfall every year recharges the deep and phreatic aquifers, providing relatively fresh water to the local population. Nevertheless, climate change and/or increasing water demand (increasing pumping rates), could easily lead to shortage of

freshwater supplies, and increased salination of the aquifers of the area. For that reason, water management projects are essential.

- 3. Geochemical research, which is the direct characterization of the aquifer, and geophysical research, which is the indirect characterization of the aquifer, showed similar results. Nevertheless, TEM and VES techniques provide a crude model of the aquifer (qualitative characteristics) since geophysical measurements are on multiface materials (aquifer and hosted rocks). Geochemical analyses proved the most accurate for groundwater quality determination, but samplings can take place only where boreholes exist. In the contrary, with TEM and VES geophysical techniques dense grid can be created. In complex environments, like Geropotamos area, the interpretation of geophysical results does not always lead to single interpretations and needs experience, due to resistivity values overlapping (Table 5.1 of Chapter 5). Nevertheless the methods are robust in that brackish waters can be easily distinguished by TEM and VES, but the range of variation within brackish waters is not fully determinable.
- 4. The multi-proxy approach used in this thesis shows correlation between the outcomes of those methods. The physical characteristics (geomorphology, geological structure) are clearly related to the geochemical and geophysical properties. All information was correlated together decreasing the uncertainty, and seawater was concluded as the only contaminator of the northern part of Geropotamos basin.
- 5. This work emphasizes that the application of TEM technique is successful in groundwater resources assessment. The reliability of the data, the portable nature of the equipment, the fast data gathering and the minimal participants needed for its operation (3 people maximum) make this electromagnetic technique an excellent tool for hydrogeology. It can be used even alone, extracting trustworthy results. However, TEM in correlation with other methods, e.g. chemical analyses or other geophysical techniques as used within the frames of this thesis, makes the project more robust.

6. Remote sensing analysis, even though it was a preliminary work, showed wonderful results, confirming documented faults (IGME map) or giving entirely new lineaments, which seem to be in agreement with TEM geophysical investigation. However, fieldwork will confirm this work

- 7. Therefore, overall, this thesis offers three contributions to knowledge:
  - **1** A practical demonstration of the value of TEM and VES geophysical methodologies in groundwater studies
  - 2 A new set of geophysical and geochemical data
  - **3** Established that seawater and not evaporites (halites), as people up to now believed, is the most likely contaminator of the study area's groundwaters.

#### 6.3 Perspectives (Suggestions for future work)

From the scientific point of view, even though this study is a multi-proxy approach which reaches coherent conclusions, future work has the potential to decrease the uncertainty even further. Some suggestions concerning both additional geochemical and geophysical work are given next.

- A) For geophysics, joint inversion of TEM and VES data maybe could improve the 1D models. This requires deeper VES soundings and of course good quality VES and TEM raw data. In addition, 3D TEM inversion using very innovative algorithms can also show better results.
- B) For geochemistry, more comprehensive and longer records of water sampling would give more information about the seasonal variation of the groundwater quality, and it is in the future plans of the author. 1 or 2 years of continuous monitoring (water sampling every 2 months), with simultaneous graphs (Piper, Durov, Stiff, molar ratios, etc) and vulnerability maps (e.g. GQI) creation, could give a more consistent model. Isotopic study is a great tool for identifying the origin of saline waters too.

To sum up, geophysical and geochemical interpretation showed safely the source of contamination, as well as the qualitative and quantitative characteristics of the groundwaters. So, the results of this thesis can lend a hand to find solutions for water management in order to achieve and preserve a long-term protection of the available groundwater resources of the area.

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## **Appendices**

## **Contents**

- A Borehole Information
- ${\bf B}$  TEM Soundings Information from data acquisition and rms from 1D Inversion
- **C** Chemical Data of the three soundings
- **D** TEM 1D Inversion Results (CD attached)

[APPENDIX A]

| s/n | code number | District                   | x         | у          | completion date | formation (near the filters)                           | Borehole Depth<br>(m) | Pump Q<br>(m3/h) | Static water level (m) | Pumping level (m) |
|-----|-------------|----------------------------|-----------|------------|-----------------|--|-----------------------|------------------|------------------------|-------------------|
| 1   | G-01        | Achlades (Stavros 1)       | 566614,57 | 3916591,42 |                 | melidoni marbles                                       | 75                    | 25               | 57.3                   |                   |
| 2   | G-05        | Achlades (Zoules 1)        | 566895,96 | 3916884,04 | 1985            | dolomitic limestone                                    | 146                   | 110              | 66,5                   | 75,6              |
| 3   | G-06        | Achlades (Zoules 2)        | 566598,31 | 3917211,33 | 1998            | melidoni marbles                                       | 75                    | 36               | 52,9                   | 62,03             |
| 4   | G-09        | Achlades (Stavros 2)       | 566730,98 | 3916795,65 | 1989            | melidoni marbles                                       | 144                   | 100              | 63                     | 65.30             |
| 5   | G-10        | Achlades (Agathes)         | 563248,73 | 3915484,67 |                 |  |                       | 20               |                        |                   |
| 6   | G-12        | Aggeliana (Spilio Psaraki) | 560738,49 | 3915767,76 | 1987            | marly limestone  | 141                   | 30               | 27                     |                   |
| 7   | G-15        | Aggeliana (Hanothiana)     | 561360,01 | 3914985,42 | 1975            | marly limestone  | 150                   | 80               | 29,5                   | 51,96             |
| 8   | G-17        | Aggeliana (Vrisida)        | 560340,4  | 3916643,2  | 1995            | marly limestone / sandstone / conglomerate             | 150                   | 60               | 36                     | 85                |
| 9   | G-18        | Aggeliana (Aspros Poros)   | 559896,4  | 3916875,63 | 1991            | marly limestone / sandstone / conglomerate             | 146                   | 10               | 50                     | 112               |
| 10  | G-20        | Aggeliana (Podikou)        | 560898,68 | 3915326,59 |                 |  |                       | 35               |                        |                   |
| 11  | G-39        | Melidoni (Maniaki)         | 567893,47 | 3917020,11 | 1984            | dolomitic limestone                                    | 162                   | 35               | 118                    |                   |
| 12  | G-40        | Melidoni (Gonia-Exadis)    | 567531,24 | 3917411,7  | 1969            | dolomitic limestone                                    | 130                   | 25               | 75                     |                   |
| 13  | G-44        | Melidoni (Tzigromouri)     | 567219,8  | 3917299,51 |                 |  |                       | 130              |                        |                   |
| 14  | G-50        | Panormos (Chalikias)       | 561013,5  | 3917803,03 | 1969            | marly limestone  | 80                    | 50               | 14                     | 50                |
| 15  | G-52        | Panormos (Dalambelos)      | 561595,91 | 3917333,62 | 1995            | marly limestone  | 75                    | 20               | 24.2                   | 30                |
| 16  | G-53        | Panormos (Zigardeli)       | 562236,8  | 3917140,97 | 2000            | marly limestone  | 100                   | 25               | 50                     | 53                |
| 17  | G-55        | Perama (Melissokipos)      | 567620,62 | 3916590,69 | 1986            | dolomitic limestone                                    | 180                   | 30               | 120,36                 | 157,76            |
| 18  | G-56        | Perama (Exandi)            | 567296,25 | 3916819,25 | 1986            | dolomitic limestone                                    | 182                   | 60               | 83.80                  |                   |
| 19  | G-59        | Perama (Livadia)           | 562396,02 | 3914658,3  | 1976            | conglomerate / marly limestone / sandy marly limestone | 125                   | 20               | artesian               | 43                |
| 20  | G-63        | Roumeli (Vlicho Pigadi)    | 563106,82 | 3917992,1  | 1994            | marly limestone / sandstone                            | 57                    | 50               | 9,5                    | 30                |
| 21  | G-80        | Skepasti (Zoules)          | 566858,98 | 3917214,12 |                 |  |                       | 120              |                        |                   |
| 22  | G-81        | Skepasti (Tzanouros)       | 565241,62 | 3917787,88 | 1987            | marly limestone  | 66                    | 8                | 33.78                  |                   |

[APPENDIX B]

| Name   | Х      | Υ       | Z   | Place  | time | stack | ı   | TR | REC | Conf   | Bat     | Turns | Ampifier | Filter | deff | rms   |
|--------|--------|---------|-----|--------|------|-------|-----|----|-----|--------|---------|-------|----------|--------|------|-------|
| 0001-B | 563995 | 3914758 | 52  | Perama | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2,3   |
| 0002-A | 563901 | 3914333 | 48  | Perama | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2,49  |
| 0003-A | 563703 | 3914400 | 53  | Perama | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,55  |
| 4      | 563508 | 3914463 | 53  | Perama | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2     |
| 0005-B | 563275 | 3914511 | 60  | Perama | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,18  |
| 0006-A | 563011 | 3914586 | 64  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 0,87  |
| 0008-A | 562573 | 3914822 | 62  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,75  |
| 0009-A | 562364 | 3914873 | 62  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,46  |
| 0010-A | 562151 | 3914971 | 72  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,16  |
| 0011-A | 562475 | 3914647 | 73  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,4   |
| 0012-A | 562670 | 3914555 | 68  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 0,58  |
| 0013-A | 562007 | 3915011 | 84  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,33  |
| 0014-A | 562033 | 3914846 | 85  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,65  |
| 0015-B | 562081 | 3914625 | 86  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 0,62  |
| 0016-B | 562274 | 3914654 | 75  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,07  |
| 0017-A | 561303 | 3914787 | 81  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 10,82 |
| 0018-C | 561484 | 3914781 | 81  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2,21  |
| 0019-A | 561586 | 3914822 | 81  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,74  |
| 20     | 561932 | 3914926 | 89  | Aggel  | 5    | 5     | 2   | 50 | 50  | single | 12(int) | 1     | Off      | 50     | 6    | 0,9   |
| 0021-B | 561183 | 3914980 | 77  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2,61  |
| 0022-A | 561302 | 3914655 | 83  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 4,88  |
| 0023-A | 561479 | 3914697 | 82  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 6,19  |
| 0024-A | 561682 | 3914721 | 83  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 3,68  |
| 0025-B | 561940 | 3914779 | 88  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,23  |
| 0026-C | 560951 | 3915336 | 70  | Aggel  | 5    | 5     | 3,8 | 50 | 50  | single | 24      | 1     | Off      | 60     | 6    | 6,3   |
| 0027-B | 561153 | 3915383 | 100 | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 60     | 6    | 2,22  |
| 0029-A | 561660 | 3915540 | 96  | Aggel  | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2,42  |
| 0030-В | 561900 | 3915581 | 80  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,26  |
| 0031-C | 562094 | 3915462 | 66  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,83  |
| 0032-В | 562297 | 3915499 | 63  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 0,95  |
| 0033-C | 562493 | 3915454 | 64  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 0,82  |
| 0034-B | 562727 | 3915459 | 47  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,36  |
| 0035-В | 562884 | 3915467 | 38  | Aggel  | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,91  |
| 0036-В | 563327 | 3915530 | 43  | Achlad | 5    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 1,58  |
| 37     | 563506 | 3915492 | 41  | Achlad | 5    | 5     | 1,9 | 50 | 50  | single | 12(int) | 1     | Off      | 50     | 6    | 1,97  |
| 0052-B | 564277 | 3916165 | 56  | Achlad | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 2,31  |
| 0053-B | 564173 | 3916018 | 59  | Achlad | 6    | 5     | 3,7 | 50 | 50  | single | 24      | 1     | Off      | 50     | 6    | 4,96  |

| _      | ı      |         |    |         |   |   |     |    |    |        |         | T |     | T  |   |       |
|--------|--------|---------|----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|-------|
| 54     | 563898 | 3916245 | 51 | Achlad  | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,19  |
| 55     | 563772 | 3916127 | 63 | Achlad  | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,93  |
| 0056-В | 563573 | 3916164 | 64 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,89  |
| 0057-В | 563346 | 3916209 | 50 | Achlad  | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,62  |
| 0058-B | 563177 | 3916215 | 64 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,43  |
| 0059-В | 562980 | 3916156 | 55 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,25  |
| 0060-В | 562752 | 3916176 | 44 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,99  |
| 0061-B | 562493 | 3916069 | 31 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,97  |
| 0063-B | 562120 | 3916222 | 80 | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,1   |
| 0064-B | 561965 | 3916388 | 84 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,74  |
| 0065-В | 561770 | 3916504 | 78 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,97  |
| 0066-В | 561501 | 3916675 | 61 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,49  |
| 0067-C | 561458 | 3916500 | 68 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,26  |
| 0068-B | 561139 | 3916394 | 64 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,61  |
| 0069-В | 560965 | 3916317 | 78 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,71  |
| 0070-В | 560622 | 3916381 | 64 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,65  |
| 0071-A | 560323 | 3916769 | 83 | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 14,98 |
| 0072-В | 560625 | 3916834 | 66 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,41  |
| 0073-A | 560893 | 3916712 | 64 | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,45  |
| 0074-B | 561082 | 3916797 | 49 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,72  |
| 0075-C | 561203 | 3916866 | 50 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,93  |
| 0076-A | 561450 | 3917062 | 54 | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,51  |
| 0077-В | 561665 | 3916979 | 48 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,15  |
| 0078-A | 561881 | 3916972 | 43 | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,22  |
| 0079-В | 562099 | 3916959 | 49 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,89  |
| 0080-C | 562236 | 3917140 | 73 | Roumeli | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 11,43 |
| 0081-C | 562488 | 3917030 | 70 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,83  |
| 0082-B | 562651 | 3917075 | 66 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,42  |
| 0083-В | 562805 | 3917132 | 24 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,11  |
| 0085-B | 563018 | 3917072 | 25 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,17  |
| 0086-В | 563239 | 3917178 | 28 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,51  |
| 0087-В | 563448 | 3917197 | 52 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,51  |
| 0088-B | 563630 | 3917289 | 61 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,36  |
| 0089-B | 563834 | 3917271 | 74 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,28  |
| 0090-В | 563925 | 3917414 | 67 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,12  |
| 0091-B | 565719 | 3917370 | 48 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,13  |
| 0092-В | 565548 | 3917265 | 44 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,44  |
| 0093-C | 565309 | 3917304 | 51 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,82  |

| 0094-B | 565144 | 3917333 | 59 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,44 |
|--------|--------|---------|----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|------|
| 0095-B | 564921 | 3917260 | 52 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,66 |
| 0096-В | 564697 | 3917294 | 38 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,91 |
| 0097-В | 564419 | 3917317 | 35 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,31 |
| 0098-B | 564294 | 3917172 | 40 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,87 |
| 0099-В | 564081 | 3917146 | 58 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,46 |
| 0100-C | 565754 | 3918128 | 76 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,25 |
| 0101-C | 565475 | 3918184 | 63 | Skepa   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,27 |
| 0102-В | 565265 | 3918152 | 60 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,34 |
| 0103-C | 565081 | 3918206 | 58 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,16 |
| 0104-B | 564930 | 3918297 | 43 | Skepa   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,03 |
| 0105-В | 564704 | 3918282 | 52 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,57 |
| 106    | 564556 | 3918371 | 43 | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,05 |
| 0107-В | 564291 | 3918311 | 29 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,8  |
| 0108-B | 564070 | 3918336 | 27 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,41 |
| 0109-В | 563911 | 3918396 | 29 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,3  |
| 0110-В | 563717 | 3918357 | 24 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,92 |
| 0111-B | 563464 | 3918349 | 24 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,89 |
| 0112-B | 563346 | 3918411 | 24 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,18 |
| 0113-C | 563177 | 3918343 | 35 | Roumeli | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,1  |
| 0114-B | 562762 | 3918416 | 34 | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,27 |
| 0115-B | 562939 | 3918324 | 39 | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,25 |
| 0116-D | 562523 | 3918515 | 31 | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,97 |
| 0117-D | 562060 | 3918469 | 23 | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,08 |
| 0118-D | 562328 | 3918486 | 25 | Panorm  | 6 | 5 | 1   | 50 | 50 | single | 24      | 1 | Off | 50 | 5 | 1,47 |
| 0119-В | 561697 | 3918376 | 18 | Panorm  | 6 | 5 | 1   | 50 | 50 | single | 24      | 1 | Off | 50 | 5 | 2,45 |
| 0120-C | 561834 | 3918378 | 33 | Panorm  | 5 | 5 | 1   | 50 | 50 | single | 24      | 1 | Off | 50 | 5 | 2,15 |
| 121    | 561502 | 3918532 | 14 | Panorm  | 5 | 5 | 1   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 5 | 0,95 |
| 0122-A | 561411 | 3918613 | 13 | Panorm  | 5 | 5 | 1   | 50 | 50 | single | 24      | 1 | Off | 50 | 5 | 0,46 |
| 0123-B | 561140 | 3918506 | 7  | Panorm  | 5 | 5 | 1   | 50 | 50 | single | 24      | 1 | Off | 50 | 5 | 1,39 |
| 0124-B | 561019 | 3918234 | 30 | Panorm  | 5 | 5 | 1   | 50 | 50 | single | 24      | 1 | Off | 50 | 5 | 2,48 |
| 0125-D | 561137 | 3918351 | 28 | Panorm  | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,5  |
| 126    | 560780 | 3918513 | 14 | Panorm  | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,63 |
| 0127-B | 561448 | 3917729 | 40 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,27 |
| 0128-B | 561620 | 3917868 | 21 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,68 |
| 0129-В | 561780 | 3917814 | 19 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,49 |
| 0130-В | 562017 | 3917796 | 21 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,29 |
| 0131-B | 562212 | 3917821 | 18 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,15 |

|        | ı      |         |    |         |   | ı | ı   | 1  | ı  | 1      |         | 1 | 1   | 1  | ı |       |
|--------|--------|---------|----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|-------|
| 0132-A | 562520 | 3917914 | 20 | Roumeli | 5 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,58  |
| 0133-A | 562733 | 3917961 | 23 | Roumeli | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,54  |
| 0134-C | 562291 | 3917906 | 26 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,08  |
| 0135-C | 562940 | 3917999 | 23 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,51  |
| 0136-В | 563133 | 3918035 | 21 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,5   |
| 0137-В | 563556 | 3918127 | 28 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,43  |
| 0138-В | 563725 | 3917991 | 45 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,81  |
| 0139-C | 564084 | 3918031 | 34 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,11  |
| 0140-C | 564560 | 3917920 | 62 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 16,53 |
| 0141-B | 564339 | 3917893 | 57 | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,63  |
| 0142-B | 564801 | 3917916 | 49 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,48  |
| 0143-C | 565013 | 3917822 | 53 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,19  |
| 0144-B | 565291 | 3917871 | 50 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,65  |
| 0145-B | 565519 | 3917766 | 54 | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,95  |
| 0146-B | 565669 | 3917813 | 67 | Achlad  | 6 | 5 | 3,6 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,87  |
| 0147-B | 563677 | 3914933 | 41 | Perama  | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,96  |
| 0148-B | 563297 | 3915034 | 52 | Perama  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,41  |
| 0149-B | 563094 | 3915118 | 53 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,8   |
| 0150-В | 562873 | 3915175 | 50 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,2   |
| 0151-D | 561951 | 3915410 | 71 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,2   |
| 0152-B | 562147 | 3915278 | 68 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,1   |
| 0153-C | 562334 | 3915224 | 61 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,76  |
| 0154-B | 562662 | 3915230 | 58 | Aggel   | 6 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 3,72  |
| 0155-В | 562775 | 3915068 | 57 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,31  |
| 0156-C | 563019 | 3915327 | 41 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,26  |
| 0157-B | 562946 | 3914898 | 70 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,92  |
| 0158-B | 563205 | 3914846 | 57 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,05  |
| 0159-C | 563371 | 3914879 | 53 | Perama  | 6 | 5 | 2,8 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,4   |
| 0160-A | 563562 | 3914735 | 46 | Perama  | 5 | 5 | 3,1 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,58  |
| 0161-C | 563458 | 3916768 | 30 | Achlad  | 6 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,73  |
| 0162-B | 563675 | 3916722 | 29 | Achlad  | 6 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,76  |
| 0163-C | 563891 | 3916743 | 31 | Achlad  | 6 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,51  |
| 0164-C | 564102 | 3916749 | 31 | Achlad  | 6 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,42  |
| 0165-A | 564315 | 3916758 | 33 | Achlad  | 6 | 5 | 3,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,84  |
| 0166-C | 564523 | 3916834 | 35 | Achlad  | 6 | 5 | 3,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,66  |
| 0167-A | 564775 | 3916886 | 35 | Achlad  | 6 | 5 | 3,3 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,5   |
| 0168-B | 564988 | 3916967 | 38 | Achlad  | 6 | 5 | 3,1 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,35  |
| 0169-В | 565171 | 3917046 | 40 | Achlad  | 6 | 5 | 2,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,65  |

| 0170-В | 563251 | 3916812 | 29  | Achlad | 6 | 5 | 2,2 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,86 |
|--------|--------|---------|-----|--------|---|---|-----|----|----|--------|---------|---|-----|----|---|------|
| 0171-A | 561260 | 3914381 | 91  | Aggel  | 5 | 5 | 2,6 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,16 |
| 0172-A | 561519 | 3914280 | 94  | Aggel  | 5 | 5 | 2,2 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,63 |
| 0173-B | 561729 | 3914500 | 86  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,36 |
| 0174-B | 562007 | 3914478 | 91  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,53 |
| 0175-B | 562207 | 3914480 | 85  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,69 |
| 0176-B | 562474 | 3914521 | 81  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,76 |
| 0177-C | 562888 | 3914506 | 64  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,11 |
| 0178-B | 563284 | 3914741 | 65  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,3  |
| 0179-C | 563669 | 3914610 | 48  | Perama | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,83 |
| 0180-A | 563970 | 3914510 | 50  | Perama | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,88 |
| 181    | 563855 | 3915893 | 69  | Achlad | 5 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,23 |
| 0182-A | 563702 | 3915971 | 68  | Achlad | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,52 |
| 0183-A | 563517 | 3915845 | 79  | Achlad | 5 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,92 |
| 0184-A | 563303 | 3915903 | 72  | Achlad | 5 | 5 | 3,2 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,54 |
| 0185-C | 563096 | 3915864 | 47  | Achlad | 6 | 5 | 2,8 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,17 |
| 0186-В | 562931 | 3915895 | 39  | Achlad | 6 | 5 | 2,6 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,24 |
| 0187-В | 562672 | 3915904 | 41  | Aggel  | 6 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,87 |
| 0188-B | 562534 | 3915853 | 66  | Aggel  | 6 | 5 | 2,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,98 |
| 0189-B | 562278 | 3915801 | 71  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,67 |
| 0190-В | 562217 | 3915987 | 71  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,26 |
| 0191-B | 562022 | 3916054 | 65  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,96 |
| 0192-В | 562082 | 3915860 | 70  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,59 |
| 193    | 561758 | 3915772 | 115 | Aggel  | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,88 |
| 0194-B | 561679 | 3915991 | 107 | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,3  |
| 0195-В | 561670 | 3916274 | 65  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,89 |
| 0196-В | 561456 | 3916302 | 61  | Aggel  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,01 |
| 0197-В | 561478 | 3915963 | 102 | Aggel  | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,14 |
| 0198-C | 561558 | 3915873 | 119 | Aggel  | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,01 |
| 199    | 561166 | 3915884 | 95  | Aggel  | 5 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,58 |
| 0200-A | 561364 | 3915805 | 106 | Aggel  | 5 | 5 | 3,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,93 |
| 0201-D | 560979 | 3915906 | 97  | Aggel  | 6 | 5 | 3,2 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,44 |
| 0202-B | 561033 | 3916183 | 98  | Aggel  | 6 | 5 | 3,2 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,6  |
| 0203-C | 560782 | 3916084 | 97  | Aggel  | 6 | 5 | 2,9 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,32 |
| 0204-C | 561068 | 3916073 | 86  | Aggel  | 6 | 5 | 2,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,12 |
| 205    | 560701 | 3919367 | 16  | Panorm | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 7,03 |
| 0207-B | 561108 | 3919373 | 14  | Panorm | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,17 |
| 0208-C | 561407 | 3919381 | 6   | Panorm | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,45 |

| 0209-B | 561615 | 3919326 | 7   | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,77  |
|--------|--------|---------|-----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|-------|
| 0210-C | 561885 | 3919523 | 4   | Panorm  | 7 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,26  |
| 0211-C | 562050 | 3919482 | 10  | Panorm  | 7 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,27  |
| 0212-B | 562245 | 3919353 | 12  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,28  |
| 0213-B | 562468 | 3919393 | 8   | Panorm  | 6 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,27  |
| 214    | 562621 | 3919365 | 12  | Panorm  | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 9,02  |
| 0215-A | 562902 | 3919428 | 33  | Panorm  | 5 | 5 | 3,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,83  |
| 0216-B | 563085 | 3919517 | 57  | Panorm  | 6 | 5 | 3,1 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,07  |
| 0217-C | 563236 | 3919392 | 67  | Panorm  | 6 | 5 | 2,9 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,61  |
| 0218-B | 563551 | 3919455 | 78  | Roumeli | 6 | 5 | 2,8 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,63  |
| 0219-A | 563791 | 3919413 | 93  | Roumeli | 5 | 5 | 2,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,21  |
| 0220-C | 563992 | 3919444 | 76  | Roumeli | 7 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,28  |
| 0221-B | 564214 | 3919455 | 75  | Skepa   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,49  |
| 0222-C | 564371 | 3919535 | 67  | Skepa   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,41  |
| 0223-C | 564606 | 3919664 | 93  | Skepa   | 5 | 5 | 3,3 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,47  |
| 0224-B | 564795 | 3919601 | 88  | Skepa   | 6 | 5 | 3,1 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,31  |
| 0225-B | 565023 | 3919572 | 82  | Skepa   | 6 | 5 | 3   | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,54  |
| 0226-B | 565229 | 3919588 | 69  | Skepa   | 6 | 5 | 2,9 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,31  |
| 0227-B | 565429 | 3919631 | 80  | Skepa   | 6 | 5 | 2,6 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,71  |
| 0228-B | 565614 | 3919551 | 74  | Skepa   | 6 | 5 | 2,6 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,39  |
| 0229-B | 565911 | 3919527 | 106 | Skepa   | 6 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,38  |
| 0230-C | 565966 | 3918980 | 97  | Skepa   | 6 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,48  |
| 231    | 565039 | 3918947 | 60  | Skepa   | 5 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 3,54  |
| 232    | 564853 | 3919004 | 59  | Skepa   | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,22  |
| 233    | 565614 | 3919097 | 77  | Skepa   | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,75  |
| 234    | 564567 | 3918978 | 50  | Skepa   | 5 | 5 | 3,7 | 49 | 49 | single | 12(int) | 1 | Off | 50 | 6 | 2,93  |
| 235    | 564172 | 3919071 | 72  | Roumeli | 5 | 5 | 2   | 49 | 49 | single | 12(int) | 1 | Off | 50 | 6 | 3,35  |
| 0236-A | 563709 | 3919056 | 59  | Roumeli | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,41  |
| 0237-A | 563201 | 3919146 | 49  | Panorm  | 5 | 5 | 3,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,01  |
| 84     | 562877 | 3917044 | 30  | Roumeli | 5 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 0,67  |
| 0238-B | 562921 | 3919122 | 35  | Panorm  | 6 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,64  |
| 0239-A | 562717 | 3918871 | 47  | Panorm  | 5 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,81  |
| 0240-A | 562334 | 3918875 | 50  | Panorm  | 5 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,83  |
| 0241-A | 561725 | 3918946 | 48  | Panorm  | 5 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,97  |
| 0242-A | 561948 | 3918970 | 46  | Panorm  | 5 | 5 | 2,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,52  |
| 243    | 567736 | 3917789 | 88  | Melid   | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 7,34  |
| 0244-C | 567678 | 3917554 | 99  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 8,22  |
| 0245-B | 566897 | 3916920 | 78  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 10,83 |

| 0246-B | 566799 | 3917110 | 68  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,67  |
|--------|--------|---------|-----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|-------|
| 0247-C | 566886 | 3917313 | 67  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,06  |
| 0248-B | 566949 | 3917435 | 68  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,95  |
| 0249-A | 567137 | 3917552 | 71  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,94  |
| 0250-A | 567121 | 3917807 | 84  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,6   |
| 0251-B | 567384 | 3917818 | 94  | Melid   | 6 | 5 | 3,6 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,5   |
| 0252-B | 567648 | 3917801 | 87  | Melid   | 6 | 5 | 3,5 | 49 | 49 | single | 24      | 1 | Off | 50 | 6 | 7,71  |
| 0253-B | 567498 | 3917386 | 84  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 7,2   |
| 0254-B | 567274 | 3917331 | 78  | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,39  |
| 0255-B | 567457 | 3917212 | 100 | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,51  |
| 256    | 567306 | 3917026 | 104 | Melid   | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 10,71 |
| 257    | 567157 | 3916729 | 90  | Melid   | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 14,81 |
| 0258-B | 566916 | 3916818 | 78  | Achlad  | 6 | 5 | 3,4 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,31  |
| 0259-B | 566713 | 3916850 | 67  | Achlad  | 6 | 5 | 3,3 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,15  |
| 0260-B | 566520 | 3916846 | 62  | Achlad  | 6 | 5 | 3,2 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 8,36  |
| 0261-B | 566286 | 3916923 | 53  | Achlad  | 6 | 5 | 3   | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,66  |
| 0262-B | 566072 | 3916885 | 53  | Achlad  | 6 | 5 | 2,9 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,29  |
| 0263-C | 565900 | 3916966 | 54  | Achlad  | 5 | 5 | 2,5 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,6   |
| 0264-A | 565931 | 3917316 | 68  | Achlad  | 6 | 5 | 2,9 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 5,45  |
| 0265-D | 566171 | 3917360 | 80  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,98  |
| 0266-C | 566622 | 3917443 | 84  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 7,47  |
| 0267-A | 566477 | 3917495 | 73  | Achlad  | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 7,36  |
| 0268-B | 566233 | 3917168 | 82  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 7,61  |
| 0269-B | 566382 | 3917117 | 88  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 7,37  |
| 0270-B | 565764 | 3917145 | 44  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,92  |
| 0271-C | 565663 | 3917035 | 47  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,04  |
| 0272-C | 565390 | 3917065 | 41  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,57  |
| 0273-A | 566902 | 3917692 | 82  | Achlad  | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 20,75 |
| 0274-B | 566469 | 3917695 | 77  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,32  |
| 0275-B | 566098 | 3917718 | 57  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,26  |
| 276    | 562413 | 3917590 | 23  | Roumeli | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,76  |
| 277    | 562294 | 3917437 | 28  | Roumeli | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 0,92  |
| 278    | 562170 | 3917615 | 23  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 0,98  |
| 279    | 562019 | 3917469 | 43  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,75  |
| 0280-A | 562003 | 3917252 | 42  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,28  |
| 281    | 561778 | 3917258 | 41  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 0,97  |
| 282    | 561538 | 3917285 | 41  | Aggel   | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,87  |
| 0283-A | 561765 | 3917668 | 24  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,24  |
|        |        |         |     |         |   |   |     |    |    |        |         |   |     |    |   |       |

| 0284-B | 561285 | 3918218 | 22  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,83  |
|--------|--------|---------|-----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|-------|
| 0285-B | 561478 | 3918104 | 21  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,11  |
| 0286-A | 561649 | 3918105 | 20  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,89  |
| 0287-B | 562346 | 3918269 | 38  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,01  |
| 0288-A | 561915 | 3918150 | 17  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,03  |
| 0289-A | 562052 | 3918309 | 22  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,49  |
| 0290-A | 561535 | 3915121 | 89  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,55  |
| 0291-B | 561668 | 3915426 | 90  | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,83  |
| 0292-B | 561519 | 3915680 | 107 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,05  |
| 0293-A | 561094 | 3915749 | 85  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,97  |
| 0294-B | 560757 | 3915883 | 65  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,92  |
| 0295-B | 561182 | 3915571 | 98  | Aggel   | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,88  |
| 0296-В | 560978 | 3915555 | 93  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,35  |
| 0297-A | 560304 | 3917574 | 76  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,48  |
| 0298-A | 560574 | 3917639 | 80  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,19  |
| 0299-A | 560715 | 3917843 | 68  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,91  |
| 0300-A | 560849 | 3918027 | 46  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,04  |
| 0301-A | 561174 | 3918116 | 16  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,56  |
| 0302-A | 561234 | 3917965 | 19  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,49  |
| 0303-В | 561176 | 3917718 | 25  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,83  |
| 0304-A | 560851 | 3917696 | 53  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,53  |
| 0305-A | 560303 | 3917103 | 86  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,86  |
| 0306-A | 560518 | 3917272 | 86  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,86  |
| 0307-A | 560553 | 3916602 | 70  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,34  |
| 308    | 560931 | 3916889 | 75  | Aggel   | 5 | 5 | 2,1 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 4,72  |
| 0309-A | 561066 | 3916973 | 49  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,84  |
| 0310-A | 562179 | 3918779 | 39  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,81  |
| 0311-B | 561565 | 3919088 | 35  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,32  |
| 0312-A | 561007 | 3919229 | 39  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,4   |
| 0313-В | 563183 | 3918618 | 37  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,56  |
| 0314-A | 563442 | 3918718 | 30  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,07  |
| 0315-B | 563688 | 3918750 | 33  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,47  |
| 0316-A | 563889 | 3918795 | 44  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,18  |
| 0317-A | 564065 | 3917742 | 61  | Roumeli | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 13,22 |
| 0318-A | 564412 | 3917700 | 47  | Roumeli | 6 | 5 | 1,9 | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,16  |
| 0319-A | 564859 | 3917633 | 46  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,93  |
| 0320-В | 563382 | 3916638 | 0   | Achlad  | 6 | 6 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,62  |
| 0321-B | 563217 | 3916479 | 37  | Achlad  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,58  |

|         |        |         | 1   |         | 1 |   |     |    |    | •      |         | • |     | •  | , |       |
|---------|--------|---------|-----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|-------|
| 0322-A  | 563021 | 3916564 | 68  | Achlad  | 6 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 5,97  |
| 0323-A  | 562863 | 3916526 | 69  | Achlad  | 6 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 3,21  |
| 0324-B  | 562801 | 3917433 | 23  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 3,2   |
| 0325-A  | 562913 | 3917726 | 82  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 5,77  |
| 0326-A  | 563412 | 3917599 | 84  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 11,21 |
| 0327-В  | 563247 | 3917493 | 82  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,22  |
| 0328-A  | 562919 | 3916940 | 26  | Roumeli | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,79  |
| 0329-A  | 565210 | 3918636 | 53  | Skepa   | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,87  |
| 0330-В  | 564905 | 3918653 | 39  | Skepa   | 5 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 2,16  |
| 0331-A  | 565350 | 3914318 | 131 | Melid   | 4 | 5 | 1   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 4,99  |
| 332     | 558599 | 3918271 | 41  | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,21  |
| 333     | 559158 | 3919367 | 14  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,36  |
| 334     | 559349 | 3919354 | 13  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,41  |
| 0335-A  | 559450 | 3919384 | 14  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,39  |
| 0336-A  | 559917 | 3919419 | 14  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,85  |
| 337     | 560099 | 3919448 | 15  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 0,97  |
| 0338-A  | 560320 | 3919434 | 12  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,65  |
| 0339-A  | 560510 | 3919427 | 17  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,68  |
| 340     | 560700 | 3918704 | 55  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,78  |
| 0341-A  | 561089 | 3918832 | 50  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,2   |
| 342     | 561459 | 3918999 | 67  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,04  |
| 0343-A  | 560724 | 3919235 | 40  | Panorm  | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,08  |
| 0344-A  | 560534 | 3919257 | 40  | Panorm  | 6 | 5 | 2   | 50 | 50 | single | 12(int) | 1 | Off | 50 | 6 | 1,01  |
| G39-01B | 567939 | 3917034 | 119 | Melid   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 8,14  |
| PAN-01  | 561994 | 3917778 | 24  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,36  |
| PAN-02  | 562017 | 3917790 | 22  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,46  |
| PAN-03  | 562034 | 3917803 | 21  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 1,7   |
| PAN-04A | 562051 | 3917849 | 16  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,28  |
| PAN-05  | 562081 | 3917866 | 17  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 1,19  |
| PAN-06A | 562103 | 3917880 | 15  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 1,95  |
| PAN-07A | 562122 | 3917920 | 14  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 60 | 3 | 2,83  |
| PAN-08A | 562135 | 3917934 | 12  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,53  |
| PAN-09  | 562157 | 3917985 | 14  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,69  |
| PAN-10A | 562181 | 3918017 | 14  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 60 | 3 | 2,53  |
| PAN-11  | 562210 | 3918021 | 15  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 60 | 3 | 1,67  |
| PAN-12  | 561967 | 3917733 | 28  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 60 | 3 | 1,66  |
| PAN-13  | 561955 | 3917706 | 13  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 60 | 3 | 0,99  |
| PAN-14A | 561929 | 3917694 | 33  | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 1,88  |

| PAN-15A | 561912 | 3917672 | 37 | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,22 |
|---------|--------|---------|----|---------|---|---|-----|----|----|--------|---------|---|-----|----|---|------|
| PAN-16  | 561902 | 3917648 | 38 | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 2,82 |
| PAN-17  | 561911 | 3917604 | 39 | Roumeli | 5 | 5 | 1   | 25 | 25 | single | 12(int) | 1 | Off | 50 | 3 | 1,95 |
| G63-01A | 563261 | 3917991 | 33 | Roumeli | 5 | 5 | 3,8 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 4,3  |
| G63-02A | 563256 | 3918071 | 26 | Roumeli | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 6,6  |
| G63-03A | 563241 | 3918110 | 25 | Roumeli | 5 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 2,34 |
| G10-01B | 563084 | 3915426 | 36 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,7  |
| G59-01B | 562482 | 3914645 | 74 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 1,14 |
| G59-02B | 562453 | 3914711 | 71 | Aggel   | 6 | 5 | 3,7 | 50 | 50 | single | 24      | 1 | Off | 50 | 6 | 3,54 |

[APPENDIX C]

| ALKALIN       | NITY & BICARBONA | TI | E CONCENTRA | TIONS       |
|---------------|------------------|----|-------------|-------------|
| Samping Date: |                  | C  | 1 10 2008   |             |
|               |                  |    |             |             |
| Borehole      | as CaCO3 (mg/L)  |    | HCO3 (mg/L) | HCO3 (me/L) |
| G-01          | 335,1            |    | 408,8       | 6,7         |
| G-05          | 281,3            |    | 343,2       | 5,6         |
| G-06          | 240,1            |    | 292,9       | 4,8         |
| G-09          | 310,0            |    | 378,2       | 6,2         |
| G-10          | 385,2            |    | 470,0       | 7,7         |
| G-12          | 331,5            |    | 404,4       | 6,6         |
| G-15          | 320,7            |    | 391,3       | 6,4         |
| G-17          | 293,9            |    | 358,5       | 5,9         |
| G-18          | 277,7            |    | 338,8       | 5,6         |
| G-20          | 304,6            |    | 371,6       | 6,1         |
| G-39          | 394,2            |    | 480,9       | 7,9         |
| G-40          | 385,2            |    | 470,0       | 7,7         |
| G-44          | 320,7            |    | 391,3       | 6,4         |
| G-50          | 250,9            |    | 306,0       | 5,0         |
| G-52          | 277,7            |    | 338,8       | 5,6         |
| G-53          | 274,1            |    | 334,5       | 5,5         |
| G-55          | 322,5            |    | 393,5       | 6,4         |
| G-56          | 317,2            |    | 386,9       | 6,3         |
| G-59          | 322,5            |    | 393,5       | 6,4         |
| G-63          | 227,6            |    | 277,6       | 4,6         |
| G-80          | 261,6            |    | 319,2       | 5,2         |
| G-81          | 256,2            |    | 312,6       | 5,1         |
| SWEET-SPR     | 297,4            |    | 362,9       | 5,9         |
| SALTY-SPR     | 202,5            |    | 247,0       | 4,0         |

|               | TOTAL HARDNESS  |                 |                 |  |  |  |  |
|---------------|-----------------|-----------------|-----------------|--|--|--|--|
| Samping Date: | 04 06 2008      | 28 07 2008      | 01 10 2008      |  |  |  |  |
|               |                 |                 |                 |  |  |  |  |
| Borehole      | as CaCO3 (mg/L) | as CaCO3 (mg/L) | as CaCO3 (mg/L) |  |  |  |  |
| G-01          | 537,1           | 598,6           | 606,8           |  |  |  |  |
| G-05          | 565,8           | 584,3           | 467,4           |  |  |  |  |
| G-06          | 155,8           | 332,1           | 332,1           |  |  |  |  |
| G-09          | 709,3           | 656,0           | 660,1           |  |  |  |  |
| G-10          |                 | 278,8           | 373,1           |  |  |  |  |
| G-12          |                 | 381,3           | 414,1           |  |  |  |  |
| G-15          |                 | 205,0           | 155,8           |  |  |  |  |
| G-17          |                 | 246,0           | 381,3           |  |  |  |  |
| G-18          |                 | 270,6           | 303,4           |  |  |  |  |
| G-20          |                 | 311,6           | 323,9           |  |  |  |  |
| G-39          |                 | 381,3           | 410,0           |  |  |  |  |
| G-40          |                 | 442,8           | 442,8           |  |  |  |  |
| G-44          |                 | 438,7           | 426,4           |  |  |  |  |
| G-50          | 574,0           | 442,8           | 672,4           |  |  |  |  |
| G-52          |                 | 487,9           | 705,2           |  |  |  |  |
| G-53          | 455,1           | 373,1           | 393,6           |  |  |  |  |
| G-55          |                 | 340,3           | 463,3           |  |  |  |  |
| G-56          |                 | 516,6           | 451,0           |  |  |  |  |
| G-59          |                 | 401,8           | 451,0           |  |  |  |  |
| G-63          |                 | 360,8           | 795,4           |  |  |  |  |
| G-80          | 496,1           | 492,0           | 512,5           |  |  |  |  |
| G-81          | 492,0           | 446,9           | 504,3           |  |  |  |  |
| SWEET-SPR     | 332,1           | 114,8           | 278,8           |  |  |  |  |
| SALTY-SPR     | 885,6           | 574,0           | 1090,6          |  |  |  |  |

|               | Е          | lectrical Conductivi | ty         | -          | Total Disolved Solid | ls         |
|---------------|------------|----------------------|------------|------------|----------------------|------------|
| Samping Date: | 04 06 2008 | 28 07 2008           | 01 10 2008 | 04 06 2008 | 28 07 2008           | 01 10 2008 |
| Borehole      | uS/cm      | uS/cm                | uS/cm      | mg/L       | mg/L                 | mg/L       |
| G-01          | 2170       | 2220                 | 2140       | 1411       | 1443                 | 1391       |
| G-05          | 2430       | 2580                 | 2670       | 1580       | 1677                 | 1736       |
| G-06          | 990        | 1010                 | 940        | 644        | 657                  | 611        |
| G-09          | 3500       | 3100                 | 3010       | 2275       | 2015                 | 1957       |
| G-10          |            | 1470                 | 1750       |            | 956                  | 1138       |
| G-12          |            | 930                  | 950        |            | 605                  | 618        |
| G-15          |            | 842                  | 852        |            | 547                  | 554        |
| G-17          |            | 877                  | 900        |            | 570                  | 585        |
| G-18          |            | 726                  | 721        |            | 472                  | 469        |
| G-20          |            | 729                  | 728        |            | 474                  | 473        |
| G-39          |            | 808                  | 1190       |            | 525                  | 774        |
| G-40          |            | 1070                 | 910        |            | 696                  | 592        |
| G-44          |            | 1830                 | 2030       |            | 1190                 | 1320       |
| G-50          | 2500       | 3340                 | 3900       | 1625       | 2171                 | 2535       |
| G-52          |            | 2900                 | 2920       |            | 1885                 | 1898       |
| G-53          | 1250       | 1510                 | 1560       | 813        | 982                  | 1014       |
| G-55          |            | 1230                 | 1210       |            | 800                  | 787        |
| G-56          |            | 2050                 | 2060       |            | 1333                 | 1339       |
| G-59          |            | 1040                 | 990        |            | 676                  | 644        |
| G-63          |            | 5810                 | 4630       |            | 3777                 | 3010       |
| G-80          | 1950       | 2150                 | 2240       | 1268       | 1398                 | 1456       |
| G-81          | 1990       | 1960                 | 1960       | 1294       | 1274                 | 1274       |
| SWEET-SPR     | 776        | 767                  | 757        | 504        | 499                  | 492        |
| SALTY-SPR     | 5250       | 6470                 | 6860       | 3413       | 4206                 | 4459       |

| SALINITY      |            |            |            |  |  |  |
|---------------|------------|------------|------------|--|--|--|
| Samping Date: | 04 06 2008 | 28 07 2008 | 01 10 2008 |  |  |  |
|               |            |            |            |  |  |  |
| Borehole      | mg/L       | mg/L       | mg/L       |  |  |  |
| G-01          | 0,982      | 1,006      | 0,968      |  |  |  |
| G-05          | 1,107      | 1,180      | 1,223      |  |  |  |
| G-06          | 0,426      | 0,435      | 0,403      |  |  |  |
| G-09          | 1,630      | 1,433      | 1,389      |  |  |  |
| G-10          |            | 0,650      | 0,782      |  |  |  |
| G-12          |            | 0,398      | 0,407      |  |  |  |
| G-15          |            | 0,357      | 0,362      |  |  |  |
| G-17          | -          | 0,374      | 0,384      |  |  |  |
| G-18          |            | 0,304      | 0,302      |  |  |  |
| G-20          |            | 0,305      | 0,305      |  |  |  |
| G-39          |            | 0,342      | 0,519      |  |  |  |
| G-40          |            | 0,463      | 0,389      |  |  |  |
| G-44          |            | 0,820      | 0,915      |  |  |  |
| G-50          | 1,141      | 1,551      | 1,828      |  |  |  |
| G-52          |            | 1,335      | 1,345      |  |  |  |
| G-53          | 0,547      | 0,669      | 0,692      |  |  |  |
| G-55          |            | 0,537      | 0,528      |  |  |  |
| G-56          |            | 0,925      | 0,929      |  |  |  |
| G-59          |            | 0,449      | 0,426      |  |  |  |
| G-63          |            | 2,793      | 2,194      |  |  |  |
| G-80          | 0,877      | 0,973      | 1,016      |  |  |  |
| G-81          | 0,896      | 0,882      | 0,882      |  |  |  |
| SWEET-SPR     | 0,327      | 0,323      | 0,318      |  |  |  |
| SALTY-SPR     | 2,508      | 3,133      | 3,335      |  |  |  |

| TEMPERATURE   |            |            |      |  |  |  |
|---------------|------------|------------|------|--|--|--|
| Samping Date: | 04 06 2008 | 01 10 2008 |      |  |  |  |
|               |            |            |      |  |  |  |
| Borehole      | °C         | Ç          | °C   |  |  |  |
| G-01          | 21,1       | 20,6       | 20,5 |  |  |  |
| G-05          | 20,0       | 20,6       | 20,7 |  |  |  |
| G-06          | 21,2       | 21,2       | 21,1 |  |  |  |
| G-09          | 19,6       | 20,8       | 20,6 |  |  |  |
| G-10          |            | 22,9       | 23,0 |  |  |  |
| G-12          |            | 20,0       | 19,2 |  |  |  |
| G-15          |            | 19,7       | 19,8 |  |  |  |
| G-17          |            | 19,9       | 19,6 |  |  |  |
| G-18          |            | 20,7       | 20,8 |  |  |  |
| G-20          |            | 19,5       | 19,8 |  |  |  |
| G-39          |            | 20,8       | 20,5 |  |  |  |
| G-40          |            | 20,9       | 20,7 |  |  |  |
| G-44          |            | 20,9       | 21,0 |  |  |  |
| G-50          | 19,0       | 19,3       | 18,7 |  |  |  |
| G-52          |            | 19,9       | 20,1 |  |  |  |
| G-53          | 19,1       | 19,6       | 19,0 |  |  |  |
| G-55          |            | 21,5       | 20,2 |  |  |  |
| G-56          |            | 20,6       | 20,5 |  |  |  |
| G-59          |            | 20,6       | 19,6 |  |  |  |
| G-63          |            | 18,1       | 18,8 |  |  |  |
| G-80          | 21,1       | 20,8       | 20,8 |  |  |  |
| G-81          | 21,2       | 21,2       | 21,1 |  |  |  |
| SWEET-SPR     | 19,6       | 19,3       | 19,0 |  |  |  |
| SALTY-SPR     | 18,0       | 19,0       | 18,2 |  |  |  |

|               | CALCIUM |      |        |      |        |      |  |
|---------------|---------|------|--------|------|--------|------|--|
| Samping Date: | 04 06   | 2008 | 28 07  | 2008 | 01 10  | 2008 |  |
|               |         |      |        |      |        |      |  |
| Borehole      | mg/L    | me/L | mg/L   | me/L | mg/L   | me/L |  |
| G-01          | 82,50   | 4,12 | 108,00 | 5,39 | 104,80 | 5,23 |  |
| G-05          | 87,50   | 4,37 | 104,00 | 5,19 | 111,93 | 5,59 |  |
| G-06          | 49,50   | 2,47 | 63,25  | 3,16 | 59,40  | 2,96 |  |
| G-09          | 109,75  | 5,48 | 117,75 | 5,88 | 117,73 | 5,87 |  |
| G-10          |         |      | 133,00 | 6,64 | 150,30 | 7,50 |  |
| G-12          |         |      | 102,50 | 5,11 | 108,40 | 5,41 |  |
| G-15          |         |      | 113,50 | 5,66 | 110,08 | 5,49 |  |
| G-17          |         |      | 104,00 | 5,19 | 101,40 | 5,06 |  |
| G-18          |         |      | 80,00  | 3,99 | 76,60  | 3,82 |  |
| G-20          |         |      | 98,75  | 4,93 | 97,18  | 4,85 |  |
| G-39          |         |      | 70,25  | 3,51 | 92,85  | 4,63 |  |
| G-40          |         |      | 84,00  | 4,19 | 75,43  | 3,76 |  |
| G-44          |         |      | 92,75  | 4,63 | 77,28  | 3,86 |  |
| G-50          | 111,50  | 5,56 | 160,50 | 8,01 | 185,63 | 9,26 |  |
| G-52          |         |      | 178,00 | 8,88 | 186,83 | 9,32 |  |
| G-53          | 81,00   | 4,04 | 117,75 | 5,88 | 122,28 | 6,10 |  |
| G-55          |         |      | 77,75  | 3,88 | 76,75  | 3,83 |  |
| G-56          |         |      | 96,50  | 4,82 | 100,88 | 5,03 |  |
| G-59          |         |      | 132,50 | 6,61 | 127,33 | 6,35 |  |
| G-63          |         |      | 148,75 | 7,42 | 148,15 | 7,39 |  |
| G-80          | 71,00   | 3,54 | 97,50  | 4,87 | 97,23  | 4,85 |  |
| G-81          | 109,00  | 5,44 | 118,25 | 5,90 | 114,23 | 5,70 |  |
| SWEET-SPR     | 81,00   | 4,04 | 93,00  | 4,64 | 92,75  | 4,63 |  |
| SALTY-SPR     | 132,00  | 6,59 | 157,75 | 7,87 | 148,60 | 7,42 |  |

|               |        | MAG  | NESIUM |            |        |      |
|---------------|--------|------|--------|------------|--------|------|
| Samping Date: | 04 06  | 2008 | 28 07  | 28 07 2008 |        | 2008 |
|               |        |      |        |            |        |      |
| Borehole      | mg/L   | me/L | mg/L   | me/L       | mg/L   | me/L |
| G-01          | 64,50  | 5,31 | 61,00  | 5,02       | 68,80  | 5,66 |
| G-05          | 65,00  | 5,35 | 68,00  | 5,60       | 70,60  | 5,81 |
| G-06          | 32,00  | 2,63 | 31,00  | 2,55       | 28,50  | 2,35 |
| G-09          | 86,50  | 7,12 | 79,00  | 6,50       | 77,90  | 6,41 |
| G-10          |        |      | 25,50  | 2,10       | 23,33  | 1,92 |
| G-12          |        |      | 21,75  | 1,79       | 16,65  | 1,37 |
| G-15          |        |      | 13,50  | 1,11       | 11,35  | 0,93 |
| G-17          |        |      | 14,75  | 1,21       | 11,93  | 0,98 |
| G-18          |        |      | 13,00  | 1,07       | 15,33  | 1,26 |
| G-20          |        |      | 11,25  | 0,93       | 10,38  | 0,85 |
| G-39          |        |      | 33,00  | 2,72       | 54,00  | 4,44 |
| G-40          |        |      | 45,00  | 3,70       | 41,10  | 3,38 |
| G-44          |        |      | 50,00  | 4,11       | 60,40  | 4,97 |
| G-50          | 34,50  | 2,84 | 54,00  | 4,44       | 68,40  | 5,63 |
| G-52          |        |      | 41,00  | 3,37       | 41,30  | 3,40 |
| G-53          | 21,25  | 1,75 | 24,00  | 1,97       | 23,60  | 1,94 |
| G-55          |        |      | 41,00  | 3,37       | 44,50  | 3,66 |
| G-56          |        |      | 57,00  | 4,69       | 61,90  | 5,09 |
| G-59          |        |      | 18,25  | 1,50       | 14,88  | 1,22 |
| G-63          |        |      | 109,00 | 8,97       | 88,20  | 7,26 |
| G-80          | 53,25  | 4,38 | 55,00  | 4,53       | 55,10  | 4,53 |
| G-81          | 32,00  | 2,63 | 30,75  | 2,53       | 28,25  | 2,32 |
| SWEET-SPR     | 12,75  | 1,05 | 12,50  | 1,03       | 11,70  | 0,96 |
| SALTY-SPR     | 112,00 | 9,22 | 110,00 | 9,05       | 114,00 | 9,38 |

|               | POTASSIUM |      |            |      |       |      |
|---------------|-----------|------|------------|------|-------|------|
| Samping Date: | 04 06     | 2008 | 28 07 2008 |      | 01 10 | 2008 |
|               |           |      |            |      |       |      |
| Borehole      | mg/L      | me/L | mg/L       | me/L | mg/L  | me/L |
| G-01          | 5,90      | 0,15 | 3,98       | 0,10 | 4,79  | 0,12 |
| G-05          | 7,30      | 0,19 | 7,48       | 0,19 | 6,25  | 0,16 |
| G-06          | 2,30      | 0,06 | 2,23       | 0,06 | 1,94  | 0,05 |
| G-09          | 12,00     | 0,31 | 9,20       | 0,24 | 7,70  | 0,20 |
| G-10          |           |      | 9,95       | 0,25 | 6,83  | 0,17 |
| G-12          |           |      | 3,01       | 0,08 | 2,63  | 0,07 |
| G-15          |           |      | 1,89       | 0,05 | 1,96  | 0,05 |
| G-17          |           |      | 2,12       | 0,05 | 1,47  | 0,04 |
| G-18          |           |      | 1,42       | 0,04 | 1,36  | 0,03 |
| G-20          |           |      | 1,20       | 0,03 | 1,00  | 0,03 |
| G-39          |           |      | 1,11       | 0,03 | 5,40  | 0,14 |
| G-40          |           |      | 0,72       | 0,02 | 0,56  | 0,01 |
| G-44          |           |      | 5,20       | 0,13 | 5,22  | 0,13 |
| G-50          | 10,00     | 0,26 | 10,83      | 0,28 | 10,65 | 0,27 |
| G-52          |           |      | 5,75       | 0,15 | 4,65  | 0,12 |
| G-53          | 3,70      | 0,09 | 4,51       | 0,12 | 4,26  | 0,11 |
| G-55          |           |      | 2,66       | 0,07 | 2,25  | 0,06 |
| G-56          |           |      | 5,11       | 0,13 | 4,63  | 0,12 |
| G-59          |           |      | 3,33       | 0,09 | 3,20  | 0,08 |
| G-63          |           |      | 30,50      | 0,78 | 18,40 | 0,47 |
| G-80          | 5,90      | 0,15 | 6,03       | 0,15 | 6,35  | 0,16 |
| G-81          | 4,70      | 0,12 | 4,10       | 0,10 | 3,63  | 0,09 |
| SWEET-SPR     | 1,50      | 0,04 | 1,26       | 0,03 | 1,15  | 0,03 |
| SALTY-SPR     | 31,00     | 0,79 | 31,75      | 0,81 | 29,75 | 0,76 |

|               | SODIUM |       |        |       |         |       |  |
|---------------|--------|-------|--------|-------|---------|-------|--|
| Samping Date: | 04 06  | 2008  | 28 07  | 2008  | 01 10   | 2008  |  |
|               |        |       |        |       |         |       |  |
| Borehole      | mg/L   | me/L  | mg/L   | me/L  | mg/L    | me/L  |  |
| G-01          | 187,50 | 8,16  | 145,00 | 6,31  | 290,00  | 12,62 |  |
| G-05          | 207,50 | 9,03  | 205,00 | 8,92  | 410,00  | 17,84 |  |
| G-06          | 67,50  | 2,94  | 45,00  | 1,96  | 127,00  | 5,52  |  |
| G-09          | 260,00 | 11,31 | 240,00 | 10,44 | 442,50  | 19,25 |  |
| G-10          |        |       | 85,00  | 3,70  | 170,75  | 7,43  |  |
| G-12          |        |       | 34,00  | 1,48  | 25,75   | 1,12  |  |
| G-15          |        |       | 30,50  | 1,33  | 44,00   | 1,91  |  |
| G-17          |        |       | 35,50  | 1,54  | 56,25   | 2,45  |  |
| G-18          |        |       | 31,25  | 1,36  | 51,25   | 2,23  |  |
| G-20          |        |       | 25,50  | 1,11  | 40,50   | 1,76  |  |
| G-39          |        |       | 23,75  | 1,03  | 55,00   | 2,39  |  |
| G-40          |        |       | 40,75  | 1,77  | 54,25   | 2,36  |  |
| G-44          |        |       | 126,00 | 5,48  | 252,00  | 10,96 |  |
| G-50          | 162,50 | 7,07  | 277,50 | 12,07 | 607,50  | 26,43 |  |
| G-52          |        |       | 217,50 | 9,46  | 395,00  | 17,18 |  |
| G-53          | 71,00  | 3,09  | 84,00  | 3,65  | 156,00  | 6,79  |  |
| G-55          |        |       | 58,50  | 2,54  | 85,00   | 3,70  |  |
| G-56          |        |       | 139,50 | 6,07  | 266,00  | 11,57 |  |
| G-59          |        |       | 38,00  | 1,65  | 53,50   | 2,33  |  |
| G-63          |        |       | 535,00 | 23,27 | 761,50  | 33,13 |  |
| G-80          | 150,00 | 6,53  | 159,00 | 6,92  | 307,50  | 13,38 |  |
| G-81          | 157,50 | 6,85  | 125,00 | 5,44  | 211,00  | 9,18  |  |
| SWEET-SPR     | 23,00  | 1,00  | 30,50  | 1,33  | 47,50   | 2,07  |  |
| SALTY-SPR     | 486,50 | 21,16 | 568,75 | 24,74 | 1230,00 | 53,51 |  |

|               | IRON  |      |       |      |       |      |  |
|---------------|-------|------|-------|------|-------|------|--|
| Samping Date: | 04 06 | 2008 | 28 07 | 2008 | 01 10 | 2008 |  |
|               |       |      |       |      |       |      |  |
| Borehole      | mg/L  | me/L | mg/L  | me/L | mg/L  | me/L |  |
| G-01          | 0,00  | 0,01 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-05          | 0,00  | 0,01 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-06          | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-09          | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-10          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-12          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-15          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-17          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-18          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-20          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-39          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-40          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-44          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-50          | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-52          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-53          | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-55          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-56          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-59          |       | 0,02 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-63          |       | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-80          | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| G-81          | 0,00  | 0,18 | 0,09  | 0,00 | 0,00  | 0,00 |  |
| SWEET-SPR     | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |
| SALTY-SPR     | 0,00  | 0,00 | 0,00  | 0,00 | 0,00  | 0,00 |  |

| BORON         |       |      |  |  |  |
|---------------|-------|------|--|--|--|
| Samping Date: | 01 10 | 2008 |  |  |  |
|               |       |      |  |  |  |
| Borehole      | mg/L  | me/L |  |  |  |
| G-01          | 0,06  | 0,02 |  |  |  |
| G-05          | 0,08  | 0,02 |  |  |  |
| G-06          | 0,02  | 0,01 |  |  |  |
| G-09          | 0,10  | 0,03 |  |  |  |
| G-10          | 0,10  | 0,03 |  |  |  |
| G-12          | 0,03  | 0,01 |  |  |  |
| G-15          | 0,04  | 0,01 |  |  |  |
| G-18          | 0,05  | 0,01 |  |  |  |
| G-20          | 0,03  | 0,01 |  |  |  |
| G-39          | 0,03  | 0,01 |  |  |  |
| G-40          | 0,03  | 0,01 |  |  |  |
| G-44          | 0,06  | 0,02 |  |  |  |
| G-50          | 0,10  | 0,03 |  |  |  |
| G-52          | 0,09  | 0,02 |  |  |  |
| G-53          | 0,06  | 0,02 |  |  |  |
| G-55          | 0,03  | 0,01 |  |  |  |
| G-56          | 0,06  | 0,02 |  |  |  |
| G-59          | 0,05  | 0,01 |  |  |  |
| G-63          | 0,18  | 0,05 |  |  |  |
| G-80          | 0,08  | 0,02 |  |  |  |
| G-81          | 0,02  | 0,01 |  |  |  |
| SWEET-SPR     | 0,04  | 0,01 |  |  |  |
| SALTY-SPR     | 0,27  | 0,08 |  |  |  |

|               | CHLORIDE |      |        |      |        |      |  |
|---------------|----------|------|--------|------|--------|------|--|
| Samping Date: | 04 06    | 2008 | 28 07  | 2008 | 01 10  | 2008 |  |
|               |          |      |        |      |        |      |  |
| Borehole      | mg/L     | me/L | mg/L   | me/L | mg/L   | me/L |  |
| G-01          | 506,8    | 14,3 | 526,3  | 14,8 | 515,8  | 14,6 |  |
| G-05          | 626,8    | 17,7 | 636,3  | 18,0 | 725,8  | 20,5 |  |
| G-06          | 162,0    | 4,6  | 186,4  | 5,3  | 185,9  | 5,2  |  |
| G-09          | 916,7    | 25,9 | 816,3  | 23,0 | 825,7  | 23,3 |  |
| G-10          |          |      | 256,4  | 7,2  | 355,9  | 10,0 |  |
| G-12          |          |      | 106,5  | 3,0  | 126,0  | 3,6  |  |
| G-15          |          |      | 96,5   | 2,7  | 106,0  | 3,0  |  |
| G-17          |          |      | 101,5  | 2,9  | 126,0  | 3,6  |  |
| G-18          |          |      | 96,5   | 2,7  | 116,0  | 3,3  |  |
| G-20          |          |      | 54,5   | 1,5  | 86,0   | 2,4  |  |
| G-39          |          |      | 91,5   | 2,6  | 166,0  | 4,7  |  |
| G-40          |          |      | 107,5  | 3,0  | 116,0  | 3,3  |  |
| G-44          |          |      | 396,4  | 11,2 | 395,9  | 11,2 |  |
| G-50          | 596,8    | 16,8 | 951,2  | 26,8 | 1121,7 | 31,6 |  |
| G-52          |          |      | 746,3  | 21,1 | 765,8  | 21,6 |  |
| G-53          | 201,9    | 5,7  | 311,4  | 8,8  | 325,9  | 9,2  |  |
| G-55          |          |      | 231,4  | 6,5  | 235,9  | 6,7  |  |
| G-56          |          |      | 466,4  | 13,2 | 425,9  | 12,0 |  |
| G-59          |          |      | 126,5  | 3,6  | 116,0  | 3,3  |  |
| G-63          |          |      | 1825,9 | 51,5 | 1315,6 | 37,1 |  |
| G-80          | 476,9    | 13,5 | 526,3  | 14,8 | 595,8  | 16,8 |  |
| G-81          | 506,8    | 14,3 | 471,4  | 13,3 | 451,9  | 12,7 |  |
| SWEET-SPR     | 87,0     | 2,5  | 91,5   | 2,6  | 96,0   | 2,7  |  |
| SALTY-SPR     | 1536,5   | 43,3 | 2055,9 | 58,0 | 2125,3 | 60,0 |  |

|               | pH valu    | ıe         |            |
|---------------|------------|------------|------------|
| Samping Date: | 04 06 2008 | 28 07 2008 | 01 10 2008 |
|               |            |            |            |
| Borehole      |            |            |            |
| G-01          | 7,2        | 6,9        | 7,1        |
| G-05          | 7,1        | 6,8        | 6,9        |
| G-06          | 7,3        | 7,4        | 7,6        |
| G-09          | 7,0        | 6,9        | 6,8        |
| G-10          |            | 7,1        | 7,1        |
| G-12          |            | 7,3        | 7,4        |
| G-15          |            | 7,2        | 7,2        |
| G-17          |            | 7,7        | 7,5        |
| G-18          |            | 6,9        | 7,1        |
| G-20          |            | 7,0        | 7,2        |
| G-39          |            | 7,2        | 7,1        |
| G-40          |            | 7,2        | 6,8        |
| G-44          |            | 7,7        | 7,5        |
| G-50          | 6,9        | 7,3        | 7,3        |
| G-52          |            | 6,8        | 7,0        |
| G-53          | 6,8        | 7,2        | 7,2        |
| G-55          |            | 7,3        | 7,0        |
| G-56          |            | 7,0        | 6,9        |
| G-59          |            | 6,8        | 7,0        |
| G-63          |            | 7,5        | 7,4        |
| G-80          | 7,5        | 7,4        | 7,0        |
| G-81          | 7,2        | 6,8        | 7,1        |
| SWEET-SPR     | 7,0        | 7,0        | 7,0        |
| SALTY-SPR     | 7,3        | 7,3        | 7,5        |

| NITRATE       |            |      |
|---------------|------------|------|
| Samping Date: | 01 10 2008 |      |
|               |            |      |
| Borehole      | mg/L       | me/L |
| G-01          | 9,33       | 0,15 |
| G-05          | 6,43       | 0,10 |
| G-06          | 10,79      | 0,17 |
| G-09          | 5,20       | 0,08 |
| G-10          | 9,52       | 0,15 |
| G-12          | 5,33       | 0,09 |
| G-15          | 5,77       | 0,09 |
| G-18          | 20,57      | 0,33 |
| G-20          | 6,30       | 0,10 |
| G-39          | 6,49       | 0,10 |
| G-40          | 7,36       | 0,12 |
| G-44          | 11,56      | 0,19 |
| G-50          | 7,00       | 0,11 |
| G-52          | 6,16       | 0,10 |
| G-53          | 7,20       | 0,12 |
| G-55          | 4,48       | 0,07 |
| G-56          | 14,03      | 0,23 |
| G-59          | 5,85       | 0,09 |
| G-63          | 6,10       | 0,10 |
| G-80          | 6,14       | 0,10 |
| G-81          | 5,75       | 0,09 |
| SWEET-SPR     | 0,04       | 0,01 |
| SALTY-SPR     | 0,27       | 0,08 |

| SULPHATE      |            |      |            |      |            |      |  |
|---------------|------------|------|------------|------|------------|------|--|
| Samping Date: | 04 06 2008 |      | 28 07 2008 |      | 01 10 2008 |      |  |
|               |            |      |            |      |            |      |  |
| Borehole      | mg/L       | me/L | mg/L       | me/L | mg/L       | me/L |  |
| G-01          | 80         | 2    | 80         | 2    | 140        | 3    |  |
| G-05          | 80         | 2    | 140        | 3    | 140        | 3    |  |
| G-06          | 50         | 1    | 50         | 1    | 50         | 1    |  |
| G-09          | 140        | 3    | 200        | 4    | 200        | 4    |  |
| G-10          |            |      | 50         | 1    | 110        | 2    |  |
| G-12          |            |      | 80         | 2    | 80         | 2    |  |
| G-15          |            |      | 50         | 1    | 140        | 3    |  |
| G-17          |            |      | 50         | 1    | 50         | 1    |  |
| G-18          |            |      | 25         | 1    | 110        | 2    |  |
| G-20          |            |      | 50         | 1    | 200        | 4    |  |
| G-39          |            |      | 50         | 1    | 50         | 1    |  |
| G-40          |            |      | 80         | 2    | 50         | 1    |  |
| G-44          |            |      | 80         | 2    | 110        | 2    |  |
| G-50          | 110        | 2    | 50         | 1    | 200        | 4    |  |
| G-52          |            |      | 200        | 4    | 80         | 2    |  |
| G-53          | 80         | 2    | 110        | 2    | 110        | 2    |  |
| G-55          |            |      | 50         | 1    | 200        | 4    |  |
| G-56          |            |      | 80         | 2    | 80         | 2    |  |
| G-59          |            |      | 110        | 2    | 140        | 3    |  |
| G-63          |            |      | 400        | 8    | 400        | 8    |  |
| G-80          | 80         | 2    | 80         | 2    | 110        | 2    |  |
| G-81          | 80         | 2    | 110        | 2    | 80         | 2    |  |
| SWEET-SPR     | 25         | 1    | 50         | 1    | 50         | 1    |  |
| SALTY-SPR     | 400        | 8    | 400        | 8    | 400        | 8    |  |

| PHOSPHATE     |            |      |  |  |  |
|---------------|------------|------|--|--|--|
| Samping Date: | 28 07 2008 |      |  |  |  |
|               |            |      |  |  |  |
| Borehole      | mg/L       | me/L |  |  |  |
| G-01          | 0,00       | 0,00 |  |  |  |
| G-05          | 0,00       | 0,00 |  |  |  |
| G-06          | 0,00       | 0,00 |  |  |  |
| G-09          | 0,00       | 0,00 |  |  |  |
| G-10          | 0,00       | 0,00 |  |  |  |
| G-12          | 0,00       | 0,00 |  |  |  |
| G-15          | 0,00       | 0,00 |  |  |  |
| G-17          | 0,00       | 0,00 |  |  |  |
| G-18          | 0,00       | 0,00 |  |  |  |
| G-20          | 0,00       | 0,00 |  |  |  |
| G-39          | 0,00       | 0,00 |  |  |  |
| G-40          | 0,00       | 0,00 |  |  |  |
| G-44          | 0,00       | 0,00 |  |  |  |
| G-50          | 0,00       | 0,00 |  |  |  |
| G-52          | 0,00       | 0,00 |  |  |  |
| G-53          | 0,00       | 0,00 |  |  |  |
| G-55          | 0,00       | 0,00 |  |  |  |
| G-56          | 0,00       | 0,00 |  |  |  |
| G-59          | 0,00       | 0,00 |  |  |  |
| G-63          | 0,00       | 0,00 |  |  |  |
| G-80          | 0,00       | 0,00 |  |  |  |
| G-81          | 0,00       | 0,00 |  |  |  |
| SWEET-SPR     | 0,00       | 0,00 |  |  |  |
| SALTY-SPR     | 0,00       | 0,00 |  |  |  |

[APPENDIX D]

```
1D_Inversion_Results_TEM.txt
#GEOSEC: 0001-B / 50.0/ 50.0/ 1.0/ 563995.000/ 3914758.000/ 52.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                                           0.000/rms=230.00
S [V/A]: +3.113e+001 +2.321e+001 +2.074e+001 +2.016e+001 +2.035e+001 +2.098e+001 +2.148e+001 +2.173e+001 +2.189e+001 +2.189e+001 +2.189e+001
+2.188e+001 +2.199e+001 +2.223e+001 +2.246e+001 +2.259e+001 +2.261e+001 +2.236e+001 +2.198e+001 +2.158e+001 +2.109e+001 +2.059e+001 +2.023e+001 +1.994e+001 +1.956e+001 +1.899e+001 +1.837e+001 +1.773e+001 +1.683e+001
+1.567e+001 +1.462e+001 +1.364e+001
Err[V/A]: +5.000e-001 +4.780e-001 +2.980e-001 +6.600e-002 +8.700e-002 +1.270e-001 +9.700e-002 +5.800e-002 +2.000e-002 -5.000e-003 +1.000e-015 +1.600e-002 +3.800e-002 +5.600e-002 +4.800e-002 +2.300e-002 -2.300e-002 -7.800e-002 -1.120e-001 -1.250e-001 -1.220e-001 -1.090e-001 -1.010e-001 -1.030e-001 -1.230e-001 -1.670e-001 -2.120e-001 -2.500e-001 -2.910e-001
-3.330e-001 -3.710e-001 -4.040e-001
   21.3908
                         3.07
   21.7660
                        36.53
   11.5947
                       20.00
     9.5358
                        30.28
     3.0000 10000000000.00
<Date: Sat May 31 08:21:38 2008
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                6 Ampl=OFF
<Remark: NORTH PERAMA, NEAR INDUSTRY</pre>
*****
#GEOSEC: 0002-A
                                        50.0/ 50.0/
                                                                1.0/ 563901.000/ 3914333.000/
48.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                              0.000 DH =
                                                                                                           0.000/rms=249.00
S [V/A]: +0.000e+000 +1.485e+001 +3.007e+001 +3.990e+001 +4.865e+001 +5.536e+001 +5.863e+001 +6.012e+001 +6.081e+001 +6.064e+001 +6.004e+001
+5.935e+001 +5.834e+001 +5.697e+001 +5.570e+001 +5.456e+001 +5.319e+001
+5.176e+001 +5.081e+001 +5.022e+001 +4.979e+001 +4.965e+001 +4.975e+001 +4.993e+001 +5.021e+001 +5.044e+001 +5.038e+001 +4.995e+001 +4.865e+001
+4.576e+001 +4.222e+001 +3.861e+001 +3.391e+001 +2.870e+001 +2.489e+001
+2.207e+001
                  -9.000e-001 -9.000e-001 -9.000e-001 -8.460e-001 +6.500e-001
Err[V/A]:
+3.980e-001 +2.220e-001 +1.140e-001 +2.600e-002 -3.700e-002 -6.700e-002
-8.400e-002 -1.020e-001 -1.200e-001 -1.330e-001 -1.380e-001 -1.350e-001 -1.170e-001 -9.200e-002 -6.600e-002 -3.200e-002 +1.000e-015 +1.900e-002 +2.800e-002 +2.700e-002 +6.000e-003 -3.500e-002 -9.900e-002 -2.090e-001
 -3.420e-001 -4.200e-001 -4.570e-001 -4.770e-001 -4.840e-001 -4.850e-001
-4.840e-001
   30.7217
71.7535
                       27.70
   36.4232
                       47.37
   35.0927
                       63.98
     3.0000 10000000000.00
<Date: Sat May 31 09:07:30 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                               6 Ampl=OFF
<Remark: WE CROSSED THE RIVER TO WEST</pre>
*****
#GEOSEC: 0003-A / 50.0/ 50.0/ 1. 53.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                   1.0/ 563703.000/ 3914400.000/
                                                                               0.000 DH =
                                                                                                           0.000/rms=155.00
S [V/A]: +0.000e+000 +0.000e+000 +5.477e+000 +1.381e+001 +1.862e+001 +2.080e+001 +2.185e+001 +2.270e+001 +2.383e+001 +2.530e+001 +2.666e+001 +2.789e+001 +2.941e+001 +3.110e+001 +3.240e+001 +3.335e+001 +3.430e+001
+3.508e+001 +3.552e+001 +3.579e+001 +3.608e+001 +3.640e+001 +3.671e+001 +3.703e+001 +3.749e+001 +3.804e+001 +3.837e+001 +3.842e+001 +3.794e+001 +3.647e+001 +3.453e+001 +3.258e+001 +3.014e+001 +2.767e+001 +2.612e+001
+2.522e+001
Err[V/A]:
                  +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.550e-001
+3.450e-001 +2.460e-001 +2.450e-001 +2.600e-001 +2.790e-001 +2.890e-001 +2.870e-001 +2.730e-001 +2.450e-001 +2.120e-001 +1.770e-001 +1.330e-001 +8.900e-002 +6.200e-002 +4.900e-002 +4.400e-002 +4.700e-002 +5.600e-002 +6.400e-002 +6.900e-002 +6.000e-002 +2.800e-002 -2.700e-002 -1.260e-001 -2.470e-001 -3.220e-001 -3.560e-001 -3.620e-001 -3.290e-001 -2.670e-001
-1.910e-001
```

```
1D_Inversion_Results_TEM.txt
  12.9215
34.1574
                  2.08
                 20.00
  52.8399
                 30.88
  29.8572
                 87.69
    6.4847 10000000000.00
<Date: Sat May 31 09:44:31 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                     6 Ampl=OFF
<Remark: WE CONTINUED WEST, PIG</pre>
<Place: PERAMA
#GEOSEC: 0004 / 50.0/ 50.0/ 1
53.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 563508.000/ 3914463.000/
                                                          0.000 DH =
                                                                              0.000/rms=200.00
            +0.000e+000 +0.000e+000 +0.000e+000 +9.395e+000 +1.758e+001
S [V/A]:
+2.125e+001 +2.248e+001 +2.309e+001 +2.358e+001 +2.404e+001 +2.442e+001 +2.482e+001 +2.540e+001 +2.625e+001 +2.707e+001 +2.782e+001 +2.876e+001
+2.978e+001 +3.055e+001 +3.113e+001 +3.183e+001 +3.273e+001 +3.369e+001
+3.471e+001 +3.621e+001 +3.807e+001 +3.931e+001 +3.988e+001 +3.961e+001
+3.792e+001 +3.560e+001 +3.321e+001 +3.002e+001 +2.626e+001 +2.322e+001
+2.074e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.970e-001 +4.890e-001 +2.250e-001 +1.430e-001 +1.010e-001 +8.900e-002 +9.800e-002
+1.160e-001 +1.400e-001 +1.660e-001 +1.800e-001 +1.840e-001 +1.760e-001
+1.560e-001 +1.370e-001 +1.270e-001 +1.290e-001 +1.530e-001 +1.870e-001 +2.180e-001 +2.360e-001 +2.120e-001 +1.410e-001 +3.700e-002 -1.180e-001
-2.760e-001 -3.620e-001 -4.080e-001 -4.400e-001 -4.630e-001 -4.740e-001
-4.810e-001
  14.4748
29.3353
                 2.00
25.27
                 53.90
  44.1546
  30.2612
                 58.57
    3.0000 10000000000.00
<Date: Sat May 31 10:08:32 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                     6 Ampl=OFF
<Remark: WE CONTINUED WEST, IN THE OLIV</pre>
<Place: PERAMA
<****************************
#GEOSEC: 0005-B
                           / 50.0/ 50.0/
                                               1.0/ 563275.000/ 3914511.000/
60.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          0.000 DH =
             +3.480e+000 +2.654e+000 +3.994e+000 +5.923e+000 +8.664e+000
+1.172e+001 +1.382e+001 +1.523e+001 +1.651e+001 +1.749e+001 +1.800e+001 +1.828e+001 +1.851e+001 +1.869e+001 +1.883e+001 +1.898e+001 +1.920e+001
+1.956e+001 +1.995e+001 +2.034e+001 +2.088e+001 +2.158e+001 +2.217e+001
+2.265e+001 +2.315e+001 +2.356e+001 +2.373e+001 +2.377e+001 +2.371e+001 +2.360e+001 +2.352e+001 +2.350e+001 +2.350e+001 +2.360e+001
+2.236e+001
Err[V/A]:
             +5.000e-001 -5.720e-001 -8.980e-001 -8.980e-001 +8.800e-001
+7.830e-001 +6.280e-001 +4.870e-001 +3.390e-001 +2.070e-001 +1.280e-001
+8.600e-002 +5.900e-002 +4.400e-002 +4.800e-002 +5.900e-002 +7.700e-002 +1.030e-001 +1.240e-001 +1.390e-001 +1.530e-001 +1.580e-001 +1.510e-001 +1.360e-001 +1.060e-001 +6.200e-002 +2.600e-002 +1.000e-015 -1.800e-002 -2.100e-002 -1.300e-002 -4.000e-003 -8.000e-003 -5.700e-002 -1.530e-001
-2.520e-001
  10.0360
22.0253
                 41.97
  36,6612
                 20.00
  36.6612
                 20.00
  18.8949 10000000000.00
<Date: Sat May 31 10:42:56 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                     6 Ampl=OFF
<Remark: FENSES IN LOOP</pre>
******
#GEOSEC: 0006-A
                             50.0/ 50.0/ 1.0/ 563011.000/ 3914586.000/
64.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          0.000 DH =
                                                                              0.000/\text{rms} = 87.00
S [V/A]: +7.987e+000 +5.528e+000 +5.859e+000 +6.917e+000 +8.545e+000
                                            Σελίδα 2
```

```
1D_Inversion_Results_TEM.txt
+1.035e+001 +1.151e+001 +1.225e+001 +1.292e+001 +1.351e+001 +1.394e+001 +1.433e+001 +1.488e+001 +1.559e+001 +1.625e+001 +1.686e+001 +1.763e+001 +1.857e+001 +1.940e+001 +2.014e+001 +2.111e+001 +2.229e+001 +2.328e+001
+2.410e+001 +2.504e+001 +2.600e+001 +2.667e+001 +2.718e+001 +2.775e+001
+2.834e+001 +2.877e+001 +2.910e+001 +2.939e+001 +2.947e+001 +2.922e+001
+2.873e+001
Err[V/A]: +5.000e-001 +3.710e-001 -5.710e-001 -7.530e-001 +7.300e-001
+5.960e-001 +4.440e-001 +3.320e-001 +2.400e-001 +1.880e-001 +1.800e-001
+1.910e-001 +2.100e-001 +2.290e-001 +2.400e-001 +2.440e-001 +2.450e-001
+2.480e-001 +2.520e-001 +2.560e-001 +2.590e-001 +2.540e-001 +2.420e-001 +2.250e-001 +1.980e-001 +1.650e-001 +1.410e-001 +1.240e-001 +1.100e-001 +9.600e-002 +8.400e-002 +6.800e-002 +3.600e-002 -2.100e-002 -8.600e-002
-1.470e-001
   9.7566
18.9965
                     2.62
                   23.32
   58.8326
                   22.14
   34.0865
                  114.17
   20.0000 10000000000.00
<Date: Sat May 31 11:19:22 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                               6 Ampl=OFF
<Remark: NEAR A STREET</pre>
<Place: PERAMA
<******************************
*****
                                 50.0/ 50.0/
#GEOSEC: 0008-A
                                                      1.0/ 562573.000/ 3914822.000/
                                                                 0.000 DH=
62.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                         0.000/rms=175.00
S [V/A]: +1.100e+001 +7.936e+000 +7.929e+000 +8.721e+000 +9.995e+000
+1.132e+001 +1.208e+001 +1.247e+001 +1.272e+001 +1.287e+001 +1.301e+001 +1.316e+001 +1.344e+001 +1.390e+001 +1.439e+001 +1.490e+001 +1.562e+001
+1.662e+001 +1.759e+001 +1.852e+001 +1.980e+001 +2.144e+001 +2.288e+001
+2.413e+001 +2.561e+001 +2.719e+001 +2.833e+001 +2.920e+001 +3.014e+001
+3.106e+001 +3.169e+001 +3.213e+001 +3.253e+001 +3.281e+001 +3.294e+001
+3.303e+001
Err[V/A]: +5.000e-001 +4.130e-001 -2.890e-001 -5.390e-001 +5.420e-001 +4.090e-001 +2.610e-001 +1.550e-001 +8.200e-002 +5.700e-002 +6.800e-002
+9.400e-002 +1.360e-001 +1.810e-001 +2.160e-001 +2.430e-001 +2.740e-001
+3.070e-001 +3.320e-001 +3.500e-001 +3.650e-001 +3.680e-001 +3.590e-001 +3.400e-001 +3.060e-001 +2.600e-001 +2.220e-001 +1.930e-001 +1.630e-001 +1.310e-001 +1.060e-001 +8.400e-002 +5.700e-002 +3.200e-002 +2.100e-002
+1.800e-002
   9.8758
16.1986
                     2.00
                   23.94
                   25.90
 102.4118
   46.4548
                  103.64
   20.0000 10000000000.00
<Date: Sat May 31 12:14:22 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                               6 Ampl=OFF
<Remark: NEAR A POWER LINE</pre>
<Place: PERAMA
<****
*****
                                                     1.0/ 562364.000/ 3914873.000/
#GEOSEC: 0009-A / 50.0/ 50.0/ 1.0 62.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                 0.000 DH =
                                                                                         0.000/rms=146.00
S [V/A]: +9.959e+000 +6.684e+000 +6.539e+000 +7.258e+000 +8.517e+000 +9.933e+000 +1.084e+001 +1.136e+001 +1.177e+001 +1.204e+001 +1.220e+001 +1.235e+001 +1.255e+001 +1.285e+001 +1.316e+001 +1.348e+001 +1.393e+001
+1.457e+001 +1.521e+001 +1.584e+001 +1.674e+001 +1.794e+001 +1.904e+001
+2.003e+001 +2.126e+001 +2.268e+001 +2.378e+001 +2.468e+001 +2.573e+001 +2.686e+001 +2.772e+001 +2.838e+001 +2.909e+001 +2.974e+001 +3.016e+001
+3.048e+001
              +5.000e-001 +4.660e-001 -2.740e-001 -5.940e-001 +6.220e-001
Err[V/A]:
+5.060e-001 +3.600e-001 +2.440e-001 +1.470e-001 +8.700e-002 +7.800e-002
+8.400e-002 +9.900e-002 +1.260e-001 +1.500e-001 +1.710e-001 +1.970e-001 +2.310e-001 +2.610e-001 +2.860e-001 +3.120e-001 +3.320e-001 +3.370e-001 +3.320e-001 +3.160e-001 +2.880e-001 +2.630e-001 +2.430e-001 +2.200e-001
+1.950e-001 +1.730e-001 +1.530e-001 +1.250e-001 +9.400e-002 +7.700e-002
+6.800e-002
    8.8803
                     2.12
```

```
1D_Inversion_Results_TEM.txt
  15.4761
64.2305
                   26.88
                   21.01
   48.8436
                 101.13
   20.0000 10000000000.00
<Date: Sat May 31 12:37:57 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: NEXT TO LITTLE RIVER</pre>
                                                                             6 Ampl=OFF
<Place: PERAMA
*****
                                50.0/ 50.0/
#GEOSEC: 0010-A
                                                      1.0/ 562151.000/ 3914971.000/
72.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      0.000/rms=116.00
                                                                0.000 DH=
              +0.000e+000 +0.000e+000 +7.572e+000 +1.386e+001 +1.700e+001
S \left[ V/A \right]:
+1.791e+001 +1.788e+001 +1.769e+001 +1.735e+001 +1.695e+001 +1.665e+001
+1.645e+001 +1.629e+001 +1.620e+001 +1.620e+001 +1.625e+001 +1.639e+001
+1.665e+001 +1.698e+001 +1.734e+001 +1.791e+001 +1.872e+001 +1.952e+001
+2.028e+001 +2.129e+001 +2.254e+001 +2.361e+001 +2.456e+001 +2.575e+001 +2.713e+001 +2.828e+001 +2.927e+001 +3.048e+001 +3.192e+001 +3.321e+001
+3.445e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +5.610e-001 +9.600e-002 -4.100e-002 -8.300e-002 -1.030e-001 -1.030e-001 -9.000e-002 -6.700e-002 -4.100e-002 -1.300e-002 +1.200e-002 +3.300e-002 +6.100e-002
+9.700e-002 +1.300e-001 +1.600e-001 +1.950e-001 +2.290e-001 +2.500e-001
+2.620e-001 +2.690e-001 +2.710e-001 +2.680e-001 +2.640e-001 +2.560e-001 +2.460e-001 +2.370e-001 +2.300e-001 +2.250e-001 +2.270e-001 +2.400e-001
+2.570e-001
   18.9002
                    2.40
   16.5309
                 32.48
149.45
   50.8849
   41.2500
                  150.00
   20.0000 10000000000.00
<Date: Sat May 31 13:00:59 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: NEAR G-59 WELL</pre>
                                                                             6 Ampl=OFF
<Place: PERAMA
*****
#GEOSEC: 0011-A / 50.0/ 50.0/ 1 73.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 562475.000/ 3914647.000/
                                                                                      0.000/rms=140.00
                                                                0.000 DH=
              +0.000e+000 +0.000e+000 +0.000e+000 +1.031e+001 +1.633e+001
+1.736e+001 +1.710e+001 +1.683e+001 +1.663e+001 +1.642e+001 +1.622e+001 +1.600e+001 +1.575e+001 +1.557e+001 +1.560e+001 +1.578e+001 +1.625e+001 +1.716e+001 +1.824e+001 +1.939e+001 +2.107e+001 +2.331e+001 +2.525e+001 +2.686e+001 +2.854e+001 +2.989e+001 +3.036e+001 +3.026e+001 +2.945e+001
+2.765e+001 +2.565e+001 +2.380e+001 +2.163e+001 +1.948e+001 +1.808e+001
+1.716e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.430e-001 +7.400e-002 -8.900e-002 -8.200e-002 -6.200e-002 -6.500e-002 -8.000e-002
-8.700e-002 -7.100e-002 -1.900e-002 +4.700e-002 +1.160e-001 +2.080e-001
+3.050e-001 +3.730e-001 +4.160e-001 +4.460e-001 +4.490e-001 +4.200e-001 +3.710e-001 +2.810e-001 +1.510e-001 +3.100e-002 -8.100e-002 -2.150e-001 -3.330e-001 -3.900e-001 -4.100e-001 -4.100e-001 -3.860e-001 -3.430e-001
-2.920e-001
 18.3219
16.1083
200.0000
                   3.10
27.12
48.90
                   20.00
 200,0000
    4.8873 10000000000.00
<Date: Sat May 31 14:46:09 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NEXT TO G-59 WELL
                                                                             6 Ampl=OFF
<Place: PERAMA
<****
*****
#GEOSEC: 0012-A / 50.0/ 50.0/ 1.68.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 562670.000/ 3914555.000/
                                                                0.000 DH =
                                                                                      0.000/rms = 58.00
S [V/A]: +0.000e+000 +0.000e+000 +5.883e+000 +1.341e+001 +1.782e+001
+1.974e+001 +2.039e+001 +2.067e+001 +2.079e+001 +2.075e+001 +2.065e+001
                                                Σελίδα 4
```

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1D_Inversion_Results_TEM.txt
+2.056e+001 +2.050e+001 +2.051e+001 +2.063e+001 +2.081e+001 +2.115e+001 +2.171e+001 +2.232e+001 +2.294e+001 +2.383e+001 +2.501e+001 +2.608e+001 +2.705e+001 +2.826e+001 +2.964e+001 +3.067e+001 +3.144e+001 +3.218e+001
+3.265e+001 +3.272e+001 +3.255e+001 +3.213e+001 +3.134e+001 +3.039e+001
+2.925e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.330e-001 +2.870e-001 +1.250e-001 +6.000e-002 +1.100e-002 -1.800e-002 -2.700e-002
-2.300e-002 -7.000e-003 +1.900e-002 +4.700e-002 +7.400e-002 +1.070e-001
+1.450e-001 +1.750e-001 +1.970e-001 +2.200e-001 +2.380e-001 +2.450e-001
+2.450e-001 +2.350e-001 +2.130e-001 +1.850e-001 +1.520e-001 +1.030e-001 +3.900e-002 -1.300e-002 -5.200e-002 -9.500e-002 -1.510e-001 -2.160e-001
-2.790e-001
   17.0808
                     2.00
   22.0969
                   36.99
   69.0838
                   48.50
   33.5301
                   65.49
   15.1508 10000000000.00
<Date: Sat May 31 15:11:26 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: SOME FENSES
                                                                               6 Ampl=OFF
<Place: PERAMA
*****
#GEOSEC: 0013-A / 50.0/ 50.0/ 1.
84.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                       1.0/ 562007.000/ 3915011.000/
                                                                  0.000 DH=
                                                                                        0.000/\text{rms}=133.00
              +0.000e+000 +0.000e+000 +1.110e+001 +2.021e+001 +2.414e+001
S [V/A]:
+2.427e+001 +2.333e+001 +2.240e+001 +2.133e+001 +2.023e+001 +1.950e+001
+1.900e+001 +1.853e+001 +1.814e+001 +1.792e+001 +1.780e+001 +1.771e+001 +1.770e+001 +1.779e+001 +1.793e+001 +1.820e+001 +1.867e+001 +1.920e+001
+1.975e+001 +2.058e+001 +2.176e+001 +2.289e+001 +2.398e+001 +2.541e+001
+2.705e+001 +2.826e+001 +2.905e+001 +2.964e+001 +2.976e+001 +2.953e+001
+2.924e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +4.380e-001 -1.040e-001 -2.240e-001 -2.420e-001 -2.370e-001 -2.130e-001 -1.820e-001 -1.530e-001 -1.190e-001 -8.300e-002 -5.800e-002 -3.900e-002 -1.500e-002
+1.400e-002 +4.100e-002 +6.800e-002 +1.030e-001 +1.450e-001 +1.800e-001
+2.100e-001 +2.450e-001 +2.810e-001 +3.030e-001 +3.140e-001 +3.080e-001
+2.740e-001 +2.190e-001 +1.550e-001 +6.900e-002 -1.600e-002 -5.700e-002
-7.800e-002
   34.9445
                     3.29
   16.6326
                   38.07
                  138.24
   52.5923
   10.0773 10000000000.00
<Date: Sun Jun 01 08:09:32 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                               6 Ampl=OFF
<Remark: BEFORE AGGELIANA VILLAGE</pre>
<Place: PERAMA
*****
#GEOSEC: 0014-A / 50.0 / 50.0 / 1.85.0 / 36/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 562033.000/ 3914846.000/
                                                                 0.000 DH =
                                                                                        0.000/rms=165.00
    [V/A]: +0.000e+000 +0.000e+000 +4.134e+000 +1.175e+001 +1.563e+001
+1.663e+001 +1.658e+001 +1.637e+001 +1.606e+001 +1.573e+001 +1.550e+001
+1.536e+001 +1.524e+001 +1.519e+001 +1.520e+001 +1.524e+001 +1.533e+001 +1.548e+001 +1.565e+001 +1.582e+001 +1.610e+001 +1.650e+001 +1.692e+001 +1.736e+001 +1.799e+001 +1.887e+001 +1.967e+001 +2.040e+001 +2.128e+001 +2.222e+001 +2.292e+001 +2.351e+001 +2.435e+001 +2.578e+001 +2.765e+001
+3.001e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.960e-001 +1.110e-001 -5.000e-002 -8.900e-002 -9.800e-002 -8.700e-002 -7.000e-002
-5.300e-002 -3.100e-002 -5.000e-003 +1.300e-002 +2.500e-002 +3.800e-002
+5.600e-002 +7.100e-002 +8.500e-002 +1.070e-001 +1.350e-001 +1.610e-001 +1.850e-001 +2.120e-001 +2.360e-001 +2.450e-001 +2.420e-001 +2.230e-001 +1.940e-001 +1.770e-001 +1.840e-001 +2.320e-001 +3.410e-001 +4.620e-001
+5.650e-001
   16.0961
   15.1924
                   26.52
   33.8890
                  149.92
```

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1D_Inversion_Results_TEM.txt
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```
28.2164
                  115.53
    1.0000 100000000000.00
<Date: Sun Jun 01 08:30:55 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: SOUTH OF AGGELIANA VILLAGE</pre>
<Place: PERAMA
*****
0.000/\text{rms} = 62.00
+7.631e+000 +8.524e+000 +9.079e+000 +9.549e+000 +9.903e+000 +1.014e+001
+1.032e+001 +1.056e+001 +1.086e+001 +1.114e+001 +1.138e+001 +1.170e+001
+1.209e+001 +1.244e+001 +1.276e+001 +1.319e+001 +1.375e+001 +1.431e+001 +1.485e+001 +1.559e+001 +1.653e+001 +1.730e+001 +1.793e+001 +1.863e+001 +1.933e+001 +1.983e+001 +2.022e+001 +2.058e+001 +2.071e+001 +2.035e+001
+1.953e+001
Err[V/A]: +5.000e-001 +4.950e-001 -2.560e-001 -6.730e-001 +7.120e-001 +6.020e-001 +4.530e-001 +3.280e-001 +2.170e-001 +1.490e-001 +1.230e-001 +1.200e-001 +1.290e-001 +1.390e-001 +1.450e-001 +1.490e-001 +1.560e-001
+1.620e-001 +1.680e-001 +1.760e-001 +1.920e-001 +2.170e-001 +2.410e-001 +2.590e-001 +2.720e-001 +2.700e-001 +2.540e-001 +2.300e-001 +1.970e-001
+1.640e-001 +1.410e-001 +1.180e-001 +6.900e-002 -4.300e-002 -1.930e-001
-3.220e-001
    7.7847
                     2.15
   12.8370
                   23.28
                  103.87
   27.3803
    8.2788
                    54.37
    3.0000 10000000000.00
<Date: Sun Jun 01 08:55:05 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: MORE SOUTH OF AGGELIANA VILL</pre>
******
#GEOSEC: 0016-B / 50.0/ 50.0/ 1.0/ 562274.000/ 3914654.000/ 75.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +1.305e+001 +9.343e+000 +9.052e+000 +9.758e+000 +1.108e+001 +1.263e+001 +1.367e+001 +1.432e+001 +1.485e+001 +1.524e+001 +1.544e+001
                                                                                          0.000/rms=107.00
+1.562e+001 +1.581e+001 +1.608e+001 +1.634e+001 +1.659e+001 +1.694e+001 +1.743e+001 +1.793e+001 +1.842e+001 +1.912e+001 +2.006e+001 +2.090e+001 +2.164e+001 +2.253e+001 +2.352e+001 +2.427e+001 +2.487e+001 +2.555e+001 +2.625e+001 +2.678e+001 +2.720e+001 +2.769e+001 +2.823e+001 +2.871e+001
+2.917e+001
Err[V/A]: +5.000e-001 +4.460e-001 -1.660e-001 -4.760e-001 +5.350e-001 +4.530e-001 +3.380e-001 +2.440e-001 +1.570e-001 +9.500e-002 +7.400e-002 +7.100e-002 +7.400e-002 +8.600e-002 +9.800e-002 +1.090e-001 +1.260e-001 +1.500e-001 +1.740e-001 +1.950e-001 +2.370e-001 +2.370e-001
+2.310e-001 +2.170e-001 +1.940e-001 +1.750e-001 +1.590e-001 +1.420e-001
+1.250e-001 +1.130e-001 +1.040e-001 +9.700e-002 +9.700e-002 +1.060e-001
+1.170e-001
   12.0657
                     2.22
   17.6026
                    24.38
                  117.84
138.99
   35.5831
   18.6533
    3.0000 10000000000.00
<Date: Sun Jun 01 09:19:29 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                6 Ampl=OFF
<Remark: MORE EAST, NEAR G-59</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0017-B / 50.0/ 50.0/ 1.0/ 561303.000/ 3914787.000/ 81.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=1134.00
              +0.000e+000 +0.000e+000 +1.496e+001 +2.904e+001 +3.662e+001
   [V/A]:
+3.834e+001 +3.781e+001 +3.692e+001 +3.562e+001 +3.388e+001 +3.227e+001 +3.088e+001 +2.931e+001 +2.789e+001 +2.713e+001 +2.680e+001 +2.672e+001
```

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1D_Inversion_Results_TEM.txt
+2.693e+001 +2.719e+001 +2.738e+001 +2.758e+001 +2.793e+001 +2.855e+001 +2.951e+001 +3.146e+001 +3.519e+001 +3.981e+001 +4.526e+001 +5.422e+001 +6.777e+001 +8.001e+001 +8.816e+001 +9.107e+001 +8.487e+001 +7.654e+001
+6.971e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.000e-001 +4.900e-002 -1.140e-001 -1.640e-001 -2.000e-001 -2.390e-001 -2.630e-001 -2.670e-001 -2.460e-001 -1.870e-001 -1.160e-001 -5.300e-002 +9.000e-003
+4.800e-002 +5.200e-002 +4.500e-002 +5.000e-002 +9.800e-002 +1.810e-001 +2.810e-001 +4.200e-001 +5.730e-001 +6.740e-001 +7.370e-001 +7.780e-001 +7.700e-001 +6.730e-001 +6.730e-001 -4.460e-001
-4.550e-001
   28.8769
                      50.00
                    102.65
  160.9499
  200.0000
                    107.01
     1.0000 10000000000.00
<Date: Sun Jun 01 10:51:34 2008</p>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NEXT TO THE RIVER, NOT SQUARE
                                                                                         6 Ampl=OFF
*****
#GEOSEC: 0018-C / 50.0 / 50.0 / 1.81.0 / 32 / 4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                              1.0/ 561484.000/ 3914781.000/
                                                                           0.000 DH=
                                                                                                    0.000/rms=221.00
S [V/A]: +0.000e+000 +6.913e+000 +2.049e+001 +2.610e+001 +2.845e+001 +2.876e+001 +2.860e+001 +2.856e+001 +2.860e+001 +2.880e+001 +2.901e+001
+2.919e+001 +2.941e+001 +2.962e+001 +2.975e+001 +2.985e+001 +2.996e+001
+3.015e+001 +3.038e+001 +3.067e+001 +3.119e+001 +3.205e+001 +3.301e+001
+3.403e+001 +3.551e+001 +3.750e+001 +3.928e+001 +4.087e+001 +4.281e+001 +4.502e+001 +4.690e+001 +4.865e+001
Err[V/A]:
                -9.000e-001 -9.000e-001 -9.000e-001 -7.350e-001 +2.390e-001
+5.000e-003 -1.900e-002 -2.000e-003 +1.800e-002 +3.700e-002 +4.100e-002 +3.800e-002 +2.900e-002 +2.400e-002 +2.300e-002 +2.500e-002 +3.800e-002 +5.600e-002 +7.800e-002 +1.110e-001 +1.540e-001 +1.910e-001 +2.190e-001 +2.470e-001 +2.650e-001 +2.690e-001 +2.630e-001 +2.500e-001
+2.400e-001 +2.440e-001 +2.550e-001
                      49.43
   29.8968
   69.9100
                    147.49
36.42
   69.9100
   14.6626 10000000000.00
<Date: Sun Jun 01 11:56:47 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                         6 Ampl=OFF
<Remark: NEXT TO THE RIVER, NOT SQUARE</pre>
*****
#GEOSEC: 0019-A / 50.0 / 50.0 / 1.81.0 / 32 / 4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                              1.0/ 561586.000/ 3914822.000/
                                                                                                    0.000/rms=174.00
                                                                           0.000 DH =
                +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +1.380e+001
    [V/A]:
+2.112e+001 +2.231e+001 +2.233e+001 +2.213e+001 +2.200e+001 +2.201e+001 +2.211e+001 +2.233e+001 +2.274e+001 +2.320e+001 +2.368e+001 +2.438e+001 +2.535e+001 +2.629e+001 +2.720e+001 +2.844e+001 +3.000e+001 +3.134e+001 +3.246e+001 +3.374e+001 +3.590e+001 +3.661e+001 +3.743e+001
+3.823e+001 +3.844e+001 +3.791e+001
Err[V/A]: -1.000e-015 -1.000e-015 -1.000e-015 -9.000e-001 +9.000e-001 +7.530e-001 +1.350e-001 -1.900e-002 -3.800e-002 -1.100e-002 +1.800e-002 +4.100e-002 +6.800e-002 +1.010e-001 +1.280e-001 +1.490e-001 +1.730e-001 +2.000e-001 +2.210e-001 +2.370e-001 +2.540e-001 +2.540e-001 +2.450e-001
+2.270e-001 +1.970e-001 +1.620e-001 +1.410e-001 +1.300e-001 +1.150e-001 +6.500e-002 -3.700e-002 -1.530e-001
                      27.11
   22.9318
   53.4854
                    126.18
   22.3917
                    150.00
 156.0627 10000000000.00
<Date: Sun Jun 01 12:22:07 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: MORE TO THE EAST, FENSES
                                                                                         6 Ampl=OFF
<Place: AGGELIANA

<a hree</a>
```

## 1D\_Inversion\_Results\_TEM.txt

```
******
                                                          50.0/ 50.0/
#GEOSEC: 0020
                                                                                             1.0/ 561932.000/ 3914926.000/
89.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                0.000 \text{ DH} =
                                                                                                                                                      0.000/rms = 90.00
                        +0.000e+000 +0.000e+000 +4.179e+000 +7.901e+000 +1.063e+001
+1.180e+001 +1.187e+001 +1.166e+001 +1.133e+001 +1.103e+001 +1.086e+001
+1.077e+001 +1.071e+001 +1.069e+001 +1.070e+001 +1.074e+001 +1.079e+001 +1.090e+001 +1.101e+001 +1.112e+001 +1.130e+001 +1.158e+001 +1.189e+001
+1.223e+001 +1.275e+001 +1.350e+001 +1.419e+001 +1.480e+001 +1.548e+001
+1.613e+001 +1.658e+001 +1.695e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +7.480e-001 +2.180e-001 -4.800e-002 -1.280e-001 -1.350e-001 -1.030e-001 -6.900e-002 -4.400e-002 -2.200e-002 -1.000e-003 +1.500e-002 +2.600e-002 +3.700e-002 +5.400e-002 +6.600e-002 +7.900e-002 +1.030e-001 +1.370e-001 +1.740e-001
+2.100e-001 +2.500e-001 +2.810e-001 +2.860e-001 +2.690e-001 +2.270e-001
+1.770e-001 +1.570e-001 +1.530e-001
                                   2.00
     11.6857
                                 32.61
     11.0850
                                 79.10
     33.0780
     14.1491 10000000000.00
 <Date: Sun Jun 01 12:49:19 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                                                                     6 Ampl=OFF
<Remark: MORE TO EAST, WE CROSSED RIVER</pre>
<Place: AGGELIANA
 <
*****
#GEOSEC: 0021-B
                                                        50.0/ 50.0/ 1.0/ 561183.000/ 3914980.000/
77.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                            0.000 DH=
                                                                                                                                                     0.000/rms=261.00
S [V/A]: +0.000e+000 +9.155e+000 +4.573e+001 +7.159e+001 +9.556e+001 +1.121e+002 +1.194e+002 +1.235e+002 +1.273e+002 +1.308e+002 +1.332e+002 +1.349e+002 +1.369e+002 +1.392e+002 +1.427e+002 +1.427e+0
+1.454e+002 +1.453e+002 +1.445e+002 +1.426e+002 +1.395e+002 +1.362e+002 +1.328e+002 +1.274e+002 +1.192e+002 +1.111e+002 +1.035e+002 +9.417e+001 +8.395e+001 +7.611e+001 +6.977e+001 +6.229e+001 +5.388e+001 +4.716e+001
+4.174e+001
                         -9.000e-001 -9.000e-001 -9.000e-001 -8.970e-001 +7.820e-001
Err[V/A]:
+4.610e-001 +2.630e-001 +1.860e-001 +1.440e-001 +1.120e-001 +9.300e-002
+8.300e-002 +7.900e-002 +7.900e-002 +7.700e-002 +7.000e-002 +5.000e-002 +1.400e-002 -2.300e-002 -5.400e-002 -8.800e-002 -1.230e-001 -1.560e-001 -1.940e-001 -2.550e-001 -3.290e-001 -3.760e-001 -4.020e-001 -4.180e-001
 -4.270e-001 -4.340e-001 -4.430e-001 -4.580e-001 -4.740e-001 -4.830e-001
-4.880e-001
                                5.39
97.34
     66.4502
  160.0417
     49.0323
                                 80.83
       8.0545 10000000000.00
<Date: Sun Jun 01 14:09:58 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: WEST OF G-15, SOME FENSES
                                                                                                                                     6 Ampl=OFF
<Place: AGGELIANA
<****************
*****
                                                                                          1.0/ 561302.000/ 3914655.000/
#GEOSEC: 0022-B / 50.0 / 50.0 / 1.0 83.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                             0.000 DH =
                                                                                                                                                     0.000/\text{rms}=488.00
S [V/A]: +0.000e+000 +0.000e+000 +4.721e+000 +9.395e+000 +1.319e+001 +1.608e+001 +1.776e+001 +1.884e+001 +1.980e+001 +2.053e+001 +2.092e+001 +2.117e+001 +2.142e+001 +2.167e+001 +2.185e+001 +2.196e+001 +2.204e+001 +2.210e+001 +2.219e+001 +2.237e+001 +2.280e+001 +2.375e+001 +2.501e+001
+2.651e+001 +2.897e+001 +3.282e+001 +3.677e+001 +4.064e+001 +4.562e+001 +5.092e+001 +5.451e+001 +5.716e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.380e-001 +5.910e-001 +4.200e-001 +3.140e-001 +2.130e-001 +1.330e-001 +9.100e-002
+7.200e-002 +6.000e-002 +5.100e-002 +4.000e-002 +2.800e-002 +1.700e-002 +1.900e-002 +4.000e-002 +7.800e-002 +1.490e-001 +2.510e-001 +3.440e-001 +4.200e-001 +5.020e-001 +5.700e-001 +5.970e-001 +5.900e-001 +5.390e-001
+4.350e-001 +3.490e-001 +2.860e-001
     21.6387
                                43.01
   200.0000
                                 87.54
   200,0000
                              103.18
```

```
1D_Inversion_Results_TEM.txt
```

```
3.0000 10000000000.00
<Date: Sun Jun 01 14:56:40 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: EAST OF G-15
<Place: AGGELIANA
*****
                              50.0/ 50.0/
                                                1.0/ 561479.000/ 3914697.000/
#GEOSEC: 0023-A
82.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                         0.000 DH =
                                                                               0.000/\text{rms}=619.00
S [V/A]: +4.118e+001 +2.817e+001 +2.275e+001 +2.025e+001 +1.870e+001 +1.803e+001 +1.788e+001 +1.794e+001 +1.810e+001 +1.845e+001 +1.888e+001
+1.936e+001 +2.006e+001 +2.099e+001 +2.174e+001 +2.226e+001 +2.267e+001
+2.276e+001 +2.267e+001 +2.260e+001 +2.274e+001 +2.341e+001 +2.453e+001
+2.598e+001 +2.847e+001 +3.249e+001 +3.674e+001 +4.100e+001 +4.653e+001 +5.186e+001 +5.376e+001 +5.283e+001
Err[V/A]: +5.000e-001 +4.990e-001 +4.830e-001 +4.150e-001 -2.590e-001 -9.400e-002 -9.000e-003 +3.200e-002 +6.700e-002 +1.100e-001 +1.480e-001
+1.780e-001 +2.020e-001 +2.060e-001 +1.780e-001 +1.330e-001 +6.300e-002
-4.000e-003 -2.200e-002 +5.000e-003 +8.300e-002 +2.110e-001 +3.280e-001 +4.230e-001 +5.210e-001 +6.010e-001 +6.350e-001 +6.310e-001 +5.600e-001 +3.440e-001 +3.300e-002 -2.550e-001
  20.9860
                 36.67
  86.9618
                 40.42
 200.0000
                136.25
    3.0000 10000000000.00
<Date: Mon Jun 02 07:45:30 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: EAST OF 0022, CROSSED RIVER</pre>
<Place: ALEX HANI
<***************************
*****
#GEOSEC: 0024-A / 50.0/ 50.0/ 1.0/ 561682.000/ 3914721.000/ 83.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +1.077e+002 +7.125e+001 +5.330e+001 +4.311e+001 +3.506e+001
                                                                               0.000/\text{rms}=368.00
+2.955e+001 +2.694e+001 +2.563e+001 +2.477e+001 +2.446e+001 +2.450e+001
+2.467e+001 +2.493e+001 +2.531e+001 +2.569e+001 +2.607e+001 +2.664e+001
+2.734e+001 +2.784e+001 +2.809e+001 +2.809e+001 +2.775e+001 +2.742e+001
+2.729e+001 +2.752e+001 +2.851e+001 +2.985e+001 +3.122e+001 +3.269e+001
+3.317e+001 +3.208e+001 +3.018e+001
Err[V/A]: +5.000e-001 +5.000e-001 +5.000e-001 +4.980e-001 -4.890e-001 -4.380e-001 -3.420e-001 -2.400e-001 -1.210e-001 -2.100e-002 +2.900e-002 +5.100e-002 +6.400e-002 +7.900e-002 +9.400e-002 +1.090e-001 +1.220e-001 +1.150e-001 +8.100e-002 +3.400e-002 -2.700e-002 -6.600e-002 -5.100e-002
+4.000e-003 +1.050e-001 +2.240e-001 +2.860e-001 +2.800e-001 +1.710e-001
-7.600e-002 -2.890e-001 -4.090e-001
  26.0801
                 40.02
  40.4419
                120.40
  40.4419
                 20.00
 198.5836 10000000000.00
<Date: Mon Jun 02 08:04:58 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: EAST OF 0023
                                                                       6 Ampl=OFF
<Place: ALEX HANI
<
*****
#GEOSEC: 0025-B / 50.0/ 50.0/ 1
88.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 561940.000/ 3914779.000/
                                                           0.000 \text{ DH} =
                                                                               0.000/rms=123.00
             +1.132e+001 +7.144e+000 +6.488e+000 +6.862e+000 +7.796e+000
+8.957e+000 +9.721e+000 +1.018e+001 +1.052e+001 +1.071e+001 +1.078e+001 +1.084e+001 +1.090e+001 +1.102e+001 +1.114e+001 +1.126e+001 +1.142e+001
+1.163e+001 +1.180e+001 +1.197e+001 +1.219e+001 +1.252e+001 +1.285e+001
+1.318e+001 +1.361e+001 +1.410e+001 +1.442e+001 +1.463e+001 +1.482e+001
+1.506e+001 +1.538e+001 +1.580e+001 +1.650e+001 +1.743e+001 +1.800e+001
+1.795e+001
Err[V/A]:
             +5.000e-001 +4.960e-001 +3.200e-002 -4.300e-001 +5.470e-001
+4.720e-001 +3.440e-001 +2.330e-001 +1.290e-001 +5.800e-002 +3.700e-002 +3.500e-002 +4.000e-002 +5.800e-002 +6.700e-002 +7.400e-002 +8.300e-002
+8.600e-002 +9.200e-002 +9.900e-002 +1.150e-001 +1.410e-001 +1.640e-001
```

```
1D_Inversion_Results_TEM.txt
+1.770e-001 +1.760e-001 +1.500e-001 +1.150e-001 +8.700e-002 +7.600e-002 +1.030e-001 +1.560e-001 +2.090e-001 +2.520e-001 +2.220e-001 +7.800e-002
-1.080e-001
    8.7930
                    2.00
  12.2143
19.6899
                  26.57
                  56.91
                  98.59
  13.5289
    1.0000 10000000000.00
<Date: Mon Jun 02 08:32:32 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: BEWEEN 0024-0015</pre>
*****
#GEOSEC: 0026-C / 50.0 / 50.0 / 1.70.0 / 32/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 560951.000/ 3915336.000/
                                                              0.000 DH=
                                                                                    0.000/rms=630.00
S [V/A]: +0.000e+000 +3.491e+000 +1.479e+001 +2.352e+001 +3.221e+001
+3.991e+001 +4.472e+001 +4.778e+001 +5.036e+001 +5.216e+001 +5.314e+001
+5.394e+001 +5.517e+001 +5.722e+001 +5.946e+001 +6.160e+001 +6.424e+001 +6.690e+001 +6.867e+001 +6.997e+001 +7.160e+001 +7.386e+001 +7.605e+001
+7.797e+001 +8.001e+001 +8.162e+001 +8.244e+001 +8.312e+001 +8.440e+001
+8.692e+001 +8.969e+001 +9.200e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 +8.310e-001 +6.370e-001 +4.680e-001 +3.420e-001 +2.200e-001 +1.300e-001 +1.020e-001 +1.100e-001 +1.460e-001 +1.970e-001 +2.280e-001 +2.340e-001 +2.130e-001
+1.710e-001 +1.390e-001 +1.290e-001 +1.390e-001 +1.610e-001 +1.710e-001 +1.590e-001 +1.230e-001 +7.600e-002 +5.800e-002 +7.000e-002 +1.130e-001
+1.650e-001 +1.790e-001 +1.700e-001
   47.4530
                    2.00
                  20.00
  48.4401
  97.8289
                 128.21
                 114.76
   37.6240
    2.0354 10000000000.00
<Date: Mon Jun 02 09:17:46 2008</pre>
<Time Range=5 Currrent= 3.80 Stack= 5 Filter=60 Deff=
                                                                           6 Ampl=OFF
<Remark: NEAR G-20, IN USE
<Place: AGGELIANA
*****
#GEOSEC: 0027-B / 50.0/ 50.0/ 1.0/ 561153.000/ 3915383.000/ 100.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=222.00
    [V/A]: +0.000e+000 +2.379e+000 +2.276e+001 +3.455e+001 +4.297e+001
+4.789e+001 +4.991e+001 +5.084e+001 +5.137e+001 +5.156e+001 +5.159e+001
+5.161e+001 +5.171e+001 +5.183e+001 +5.182e+001 +5.163e+001 +5.110e+001 +5.006e+001 +4.890e+001 +4.776e+001 +4.616e+001 +4.398e+001 +4.180e+001 +3.960e+001 +3.648e+001 +3.244e+001 +2.906e+001 +2.626e+001 +2.315e+001
+2.009e+001 +1.799e+001 +1.648e+001 +1.492e+001 +1.337e+001 +1.217e+001
+1.113e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.910e-001 +6.550e-001 +3.210e-001 +1.630e-001 +8.900e-002 +3.700e-002 +1.000e-002 +3.000e-003 +6.000e-003 +1.100e-002 +4.000e-003 -1.400e-002 -3.900e-002 -7.700e-002
-1.180e-001 -1.470e-001 -1.700e-001 -2.030e-001 -2.520e-001 -3.040e-001 -3.520e-001 -4.030e-001 -4.420e-001 -4.590e-001 -4.650e-001 -4.650e-001 -4.570e-001 -4.450e-001 -4.330e-001 -4.200e-001 -4.180e-001 -4.340e-001
-4.520e-001
   32.2906
                    2.00
  53.0166
19.5663
                  40.93
                  37.34
                  39.16
    3.1405
    3.5220 10000000000.00
<Date: Mon Jun 02 09:46:30 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=60 Deff=</pre>
                                                                           6 Ampl=OFF
<Remark: AGGELIANA CEMETERY, FENCES</pre>
*****
#GEOSEC: 0029-A
                             / 50.0/ 50.0/ 1.0/ 561660.000/ 3915540.000/
```

Σελίδα 10

```
1D_Inversion_Results_TEM.txt
96.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +0.000e+000 +0.000e+000 +9.459e+000 +1.709e+001 +2.297e+001
+2.604e+001 +2.674e+001 +2.667e+001 +2.637e+001 +2.611e+001 +2.615e+001
                                                                                      0.000/rms=242.00
+2.638e+001 +2.689e+001 +2.768e+001 +2.843e+001 +2.901e+001 +2.960e+001
+3.002e+001 +3.017e+001 +3.023e+001 +3.025e+001 +3.026e+001 +3.018e+001
+2.995e+001 +2.935e+001 +2.815e+001 +2.683e+001 +2.555e+001 +2.389e+001
+2.195e+001 +2.031e+001 +1.884e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.640e-001 +3.120e-001 +5.600e-002 -3.600e-002 -5.300e-002 -1.500e-002 +3.600e-002
+7.800e-002 +1.200e-001 +1.450e-001 +1.440e-001 +1.260e-001 +9.100e-002 +4.700e-002 +2.100e-002 +9.000e-003 +3.000e-003 -8.000e-003 -3.600e-002 -8.000e-002 -1.510e-001 -2.340e-001 -2.860e-001 -3.160e-001 -3.410e-001 -3.670e-001 -3.940e-001 -4.180e-001
   24.6017
                    2.00
                   20.00
   27.5373
   31.5457
                   54.74
    7.7250 10000000000.00
<Date: Mon Jun 02 10:58:11 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NE OF AGGELIANA, IN VILLAGE
                                                                            6 Ampl=OFF
<Place: AGGELIANA
*****
#GEOSEC: 0030-B / 50.0/50.0/1. 80.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 561900.000/ 3915581.000/
                                                               0.000 DH=
                                                                                      0.000/\text{rms}=126.00
S [V/A]: +0.000e+000 +0.000e+000 +7.279e+000 +1.555e+001 +2.099e+001
+2.409e+001 +2.558e+001 +2.648e+001 +2.724e+001 +2.780e+001 +2.811e+001
+2.832e+001 +2.859e+001 +2.899e+001 +2.944e+001 +2.993e+001 +3.069e+001 +3.181e+001 +3.297e+001 +3.415e+001 +3.580e+001 +3.797e+001 +3.994e+001
+4.171e+001 +4.396e+001 +4.672e+001 +4.909e+001 +5.113e+001 +5.335e+001
+5.473e+001 +5.415e+001 +5.213e+001 +4.804e+001 +4.211e+001 +3.708e+001
+3.307e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.770e-001 +4.180e-001 +2.590e-001 +1.850e-001 +1.230e-001 +7.600e-002 +5.500e-002
+5.100e-002 +5.900e-002 +7.800e-002 +1.010e-001 +1.240e-001 +1.540e-001
+1.920e-001 +2.230e-001 +2.460e-001 +2.690e-001 +2.850e-001 +2.900e-001
+2.900e-001 +2.890e-001 +2.870e-001 +2.800e-001 +2.580e-001 +1.850e-001 +2.200e-002 -1.660e-001 -3.130e-001 -4.180e-001 -4.640e-001 -4.770e-001
-4.820e-001
   19.6130
                    3.34
   33.3432
                   34.90
                 139.48
   68.8701
    3.0954 10000000000.00
<Date: Mon Jun 02 11:36:40 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                            6 Ampl=OFF
<Remark: EAST OF 0029
<Place: AGGELIANA
*****
#GEOSEC: 0031-C / 50.0 / 50.0 / 1.66.0 / 36 /4/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 562094.000/ 3915462.000/
                                                               0.000 DH =
                                                                                      0.000/rms=183.00
S [V/A]: +0.000e+000 +0.000e+000 +8.673e+000 +1.676e+001 +2.060e+001
+2.122e+001 +2.077e+001 +2.020e+001 +1.947e+001 +1.871e+001 +1.822e+001
+1.790e+001 +1.765e+001 +1.753e+001 +1.755e+001 +1.761e+001 +1.775e+001
+1.796e+001 +1.818e+001 +1.840e+001 +1.872e+001 +1.919e+001 +1.968e+001 +2.020e+001 +2.100e+001 +2.217e+001 +2.334e+001 +2.448e+001 +2.598e+001
+2.771e+001 +2.898e+001 +2.992e+001 +3.094e+001 +3.223e+001 +3.373e+001
+3.559e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +5.330e-001 -6.000e-003 -1.450e-001 -1.780e-001 -1.830e-001 -1.600e-001 -1.300e-001
-9.800e-002 -5.500e-002 -1.100e-002 +1.600e-002 +3.300e-002 +5.000e-002
+6.500e-002 +7.700e-002 +8.900e-002 +1.070e-001 +1.350e-001 +1.640e-001 +1.940e-001 +2.350e-001 +2.800e-001 +3.090e-001 +3.220e-001 +3.160e-001 +2.810e-001 +2.370e-001 +2.040e-001 +1.930e-001 +2.340e-001 +3.140e-001
+3.970e-001
   28.6824
                   37.02
   17.3921
   48.8361
                   48.82
```

```
1D_Inversion_Results_TEM.txt
    60.2127 10000000000.00
 <Date: Mon Jun 02 12:08:32 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                       6 Ampl=OFF
<Remark: EAST OF 0030
<Place: AGGELIANA
*****
#GEOSEC: 0032-B / 50.0 / 50.0 / 1.0 63.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                   1.0/ 562297.000/ 3915499.000/
                                                                                                 0.000 DH =
                                                                                                                                      0.000/\text{rms} = 95.00
S [V/A]: +0.000e+000 +0.000e+000 +4.410e+000 +1.171e+001 +1.649e+001 +1.878e+001 +1.953e+001 +1.978e+001 +1.986e+001 +1.984e+001 +1.983e+001
+1.986e+001 +1.997e+001 +2.018e+001 +2.041e+001 +2.063e+001 +2.090e+001
+2.120e+001 +2.143e+001 +2.162e+001 +2.184e+001 +2.210e+001 +2.234e+001
+2.257e+001 +2.288e+001 +2.329e+001 +2.366e+001 +2.403e+001 +2.454e+001
+2.525e+001 +2.589e+001 +2.642e+001 +2.684e+001 +2.659e+001 +2.541e+001
+2.358e+001
Err[V/A]:
                      +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.060e-001
+3.520e-001 +1.370e-001 +5.400e-002 +9.000e-003 -4.000e-003 +5.000e-003
+1.900e-002 +3.900e-002 +5.900e-002 +6.900e-002 +7.200e-002 +7.100e-002 +6.600e-002 +6.100e-002 +5.800e-002 +5.800e-002 +6.200e-002 +6.700e-002 +7.300e-002 +8.000e-002 +9.100e-002 +1.010e-001 +1.120e-001 +1.280e-001 +1.430e-001 +1.430e-001 +1.160e-001 +2.700e-002 -1.630e-001 -3.450e-001
-4.460e-001
    16.7020
    21.4182
                             25.09
    25.4077
                           147.79
       3.0000 10000000000.00
<Date: Mon Jun 02 12:35:17_2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: EAST OF 0031
                                                                                                                       6 Ampl=OFF
<Place: AGGELIANA
<****************
*****
                                                  50.0/ 50.0/
                                                                                 1.0/ 562493.000/ 3915454.000/
#GEOSEC: 0033-C
64.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                  0.000 DH=
                                                                                                                                      0.000/\text{rms} = 82.00
S [V/A]: +6.216e+000 +4.974e+000 +6.126e+000 +7.856e+000 +1.024e+001
+1.275e+001 +1.435e+001 +1.535e+001 +1.616e+001 +1.672e+001 +1.700e+001 +1.718e+001 +1.738e+001 +1.761e+001 +1.783e+001 +1.802e+001 +1.828e+001
+1.860e+001 +1.891e+001 +1.921e+001 +1.961e+001 +2.012e+001 +2.054e+001
+2.090e+001 +2.132e+001 +2.180e+001 +2.220e+001 +2.258e+001 +2.308e+001
+2.367e+001 +2.408e+001 +2.428e+001 +2.420e+001 +2.355e+001 +2.263e+001
+2.172e+001
Err[V/A]:
                      +5.000e-001 -1.890e-001 -8.270e-001 -8.540e-001 +8.010e-001
+6.490e-001 +4.780e-001 +3.430e-001 +2.160e-001 +1.210e-001 +8.100e-002 +6.800e-002 +6.300e-002 +6.800e-002 +7.100e-002 +7.500e-002 +8.200e-002 +9.100e-002 +1.020e-001 +1.110e-001 +1.190e-001 +1.230e-001 +1.200e-001 +1.160e-001 +1.100e-001 +1.080e-001 +1.120e-001 +1.190e-001 +1.230e-001 +1.230
 -2.810e-001
    11.7547
                               2.51
                             31.83
     20.1932
                           125.39
    27.3492
      7.7868 10000000000.00
<Date: Mon Jun 02 13:01:29 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: EAST OF 0032
                                                                                                                       6 Ampl=OFF
<Place: AGGELIANA
<********************************
*****
#GEOSEC: 0034-B / 50.0/ 50.0/ 1. 47.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                   1.0/ 562727.000/ 3915459.000/
                                                                                                   0.000 DH=
                                                                                                                                      0.000/rms=136.00
                      +0.000e+000 +0.000e+000 +2.894e+000 +9.439e+000 +1.386e+001
+1.613e+001 +1.684e+001 +1.699e+001 +1.692e+001 +1.669e+001 +1.658e+001 +1.661e+001 +1.684e+001 +1.734e+001 +1.794e+001 +1.854e+001 +1.934e+001 +2.029e+001 +2.103e+001 +2.161e+001 +2.224e+001 +2.292e+001 +2.351e+001 +2.410e+001 +2.497e+001 +2.622e+001 +2.737e+001 +2.839e+001 +2.952e+001 +3.036e+001 +3.041e+001 +2.985e+001 +2.844e+001 +2.610e+001 +2.397e+001
+2.226e+001
```

```
1D_Inversion_Results_TEM.txt
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.420e-001 +4.000e-001 +1.350e-001 +2.000e-002 -4.200e-002 -4.900e-002 -1.000e-002
+4.000e-002 +1.050e-001 +1.690e-001 +2.070e-001 +2.250e-001 +2.300e-001
+2.170e-001 +1.950e-001 +1.730e-001 +1.530e-001 +1.470e-001 +1.600e-001
+1.830e-001 +2.140e-001 +2.430e-001 +2.490e-001 +2.340e-001 +1.800e-001 +6.800e-002 -6.400e-002 -1.870e-001 -3.060e-001 -3.810e-001 -4.010e-001
-4.060e-001
  14.1925
                  20.12
   18.6818
   33.7357
                 123.22
    4.0403
                  20.00
    3.1443 10000000000.00
<Date: Mon Jun 02 13:25:38 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: EAST OF 0033</pre>
<Place: AGGELIANA
******
#GEOSEC: 0035-B / 50.0/ 50.0/ 1.
38.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 562884.000/ 3915467.000/
                                                             0.000 DH =
                                                                                 0.000/\text{rms}=191.00
             +0.000e+000 +0.000e+000 +2.290e+000 +1.132e+001 +1.743e+001
    [V/A]:
+2.046e+001 +2.144e+001 +2.171e+001 +2.167e+001 +2.129e+001 +2.086e+001
+2.052e+001 +2.021e+001 +2.004e+001 +2.010e+001 +2.028e+001 +2.067e+001
+2.128e+001 +2.186e+001 +2.232e+001 +2.281e+001 +2.319e+001 +2.333e+001 +2.335e+001 +2.329e+001 +2.316e+001 +2.301e+001 +2.285e+001 +2.258e+001
+2.213e+001 +2.163e+001 +2.111e+001 +2.042e+001 +1.967e+001 +1.915e+001
+1.882e+001
-9.700e-002 -6.400e-002 -9.000e-003 +4.100e-002 +8.200e-002 +1.220e-001
+1.480e-001 +1.490e-001 +1.330e-001 +1.010e-001 +5.600e-002 +2.100e-002 -2.000e-003 -2.100e-002 -3.400e-002 -4.400e-002 -5.600e-002 -8.000e-002 -1.180e-001 -1.510e-001 -1.710e-001 -1.800e-001 -1.660e-001 -1.350e-001
-1.000e-001
   21.1412
                  21.53
   20.6050
                  74.04
   25.8297
    7.8263
                  20.00
   15.8826 10000000000.00
<Date: Mon Jun 02 13:54:50 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                        6 Ampl=OFF
<Remark: BETWEEN 0034 AND G-10</pre>
*****
#GEOSEC: 0036-B / 50.0/ 50.0/ 1.0/ 563327.000/ 3915530.000/ 43.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +6.469e+000+4.693e+000+5.544e+000+7.103e+000+9.353e+000
                                                                                 0.000/rms=158.00
+1.179e+001 +1.337e+001 +1.432e+001 +1.506e+001 +1.551e+001 +1.575e+001
+1.595e+001 +1.626e+001 +1.672e+001 +1.719e+001 +1.761e+001 +1.813e+001 +1.868e+001 +1.909e+001 +1.944e+001 +1.994e+001 +2.071e+001 +2.157e+001 +2.250e+001 +2.393e+001 +2.588e+001 +2.753e+001 +2.877e+001 +2.975e+001
+2.990e+001 +2.939e+001 +2.877e+001
Err[V/A]: +5.000e-001 +8.000e-002 -8.040e-001 -8.570e-001 +8.150e-001 +6.750e-001 +4.950e-001 +3.430e-001 +2.030e-001 +1.090e-001 +8.400e-002 +9.300e-002 +1.180e-001 +1.460e-001 +1.610e-001 +1.630e-001 +1.520e-001
+1.340e-001 +1.260e-001 +1.330e-001 +1.600e-001 +2.110e-001 +2.630e-001
+3.080e-001 +3.480e-001 +3.590e-001 +3.230e-001 +2.470e-001 +1.120e-001
-4.400e-002 -1.250e-001 -1.660e-001
  12.2857
                   3.12
   19.3885
                  26.27
   37.9545
                  99.91
                  20.00
    8.3179
    3.0000 10000000000.00
<Date: Mon Jun 02 14:28:10 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                        6 Ampl=OFF
<Remark: NE OF G-10
<Place: ACHLADES
```

```
*****
#GEOSEC: 0037 / 50.0/ 50.0/ 1 41.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 563506.000/ 3915492.000/
                                                                           0.000 DH=
                                                                                                     0.000/rms=197.00
S [V/A]: +0.000e+000 +0.000e+000 +1.082e+000 +1.444e+001 +2.329e+001
+2.665e+001 +2.724e+001 +2.719e+001 +2.695e+001 +2.652e+001 +2.615e+001 +2.585e+001 +2.556e+001 +2.534e+001 +2.528e+001 +2.531e+001 +2.544e+001
+2.566e+001 +2.587e+001 +2.603e+001 +2.619e+001 +2.632e+001 +2.643e+001 +2.657e+001 +2.684e+001 +2.731e+001 +2.777e+001 +2.816e+001 +2.852e+001
+2.864e+001 +2.844e+001 +2.808e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.720e-001 +3.150e-001 +4.700e-002 -2.700e-002 -5.900e-002 -7.600e-002 -7.700e-002 -6.900e-002 -5.200e-002 -2.600e-002 -2.000e-003 +1.700e-002 +3.500e-002
+4.500e-002 +4.400e-002 +3.900e-002 +3.000e-002 +2.500e-002 +3.100e-002 +4.600e-002 +6.900e-002 +9.300e-002 +9.800e-002 +8.500e-002 +4.800e-002 -1.300e-002 -6.600e-002 -1.080e-001
   26.3734
                      15.55
                      25.11
   24.6119
                     106.72
   31.6565
   10.8489
                      20.00
   20.0000 10000000000.00
<Date: Mon Jun 02 14:45:19 2008</pre>
<Time Range=5 Currrent= 1.90 Stack= 5 Filter=50 Deff=
                                                                                          6 Ampl=OFF
<Remark: EAST OF 0036</pre>
<Place: ACHLADES
#GEOSEC: 0038 / 50.0/ 50.0/ 1. 33.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               1.0/ 563261.000/ 3917991.000/
                                                                           0.000 \, DH =
                                                                                                     0.000/\text{rms}=349.00
                +0.000e+000 +0.000e+000 +0.000e+000 +7.396e+000 +1.493e+001
     [V/A]:
+1.898e+001 +1.973e+001 +1.941e+001 +1.867e+001 +1.792e+001 +1.763e+001
+1.763e+001 +1.773e+001 +1.941e+001 +1.807e+001 +1.752e+001 +1.763e+001 +1.763e+001 +1.844e+001 +1.901e+001 +1.951e+001 +2.003e+001 +2.048e+001 +2.073e+001 +2.091e+001 +2.116e+001 +2.161e+001 +2.217e+001 +2.279e+001 +2.363e+001 +2.446e+001 +2.478e+001 +2.471e+001 +2.423e+001
+2.340e+001 +2.266e+001 +2.201e+001 +2.108e+001 +1.958e+001 +1.782e+001
+1.599e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.990e-001 +5.250e-001 +3.800e-002 -1.460e-001 -1.900e-001 -1.330e-001 -4.200e-002
+3.500e-002 +1.100e-001 +1.610e-001 +1.730e-001 +1.610e-001 +1.290e-001
+8.700e-002 +6.500e-002 +6.300e-002 +8.300e-002 +1.280e-001 +1.700e-001 +1.930e-001 +1.850e-001 +1.180e-001 +2.500e-002 -6.100e-002 -1.360e-001 -1.760e-001 -1.890e-001 -2.100e-001 -2.740e-001 -3.830e-001 -4.540e-001
-4.850e-001
   19.0092
   18.6626
27.3853
                      20.00
                      87.53
     6.8326
                     108.87
   20.0000 10000000000.00
<Date: Tue May 20 11:52:27 2008</pre>
<Time Range=6 Currrent= 3.80 Stack= 5 Filter=50 Deff=
                                                                                          6 Ampl=OFF
               NEXT TO VILLAGE<Place: ROUMEL
<Remark:
#GEOSEC: 0049 / 50.0/ 50.0/ 1.0/ 561299.000/ 3915007.000/ 80.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +3.135e+001 +2.722e+001 +2.705e+001 +2.794e+001 +2.949e+001
                                                                                                     0.000/\text{rms}=435.00
+3.119e+001 +3.225e+001 +3.284e+001 +3.322e+001 +3.356e+001 +3.411e+001 +3.499e+001 +3.672e+001 +3.971e+001 +4.297e+001 +4.602e+001 +4.964e+001 +5.276e+001 +5.403e+001 +5.422e+001 +5.373e+001 +5.285e+001 +5.226e+001
+5.193e+001 +5.162e+001 +5.093e+001 +4.966e+001 +4.788e+001 +4.489e+001
+4.075e+001 +3.717e+001 +3.418e+001 +3.067e+001 +2.676e+001 +2.357e+001
+2.084e+001
Err[V/A]: +4.810e-001 +2.340e-001 -8.800e-002 -2.180e-001 +2.480e-001 +2.040e-001 +1.420e-001 +9.000e-002 +5.400e-002 +7.100e-002 +1.330e-001
+2.090e-001 +3.060e-001 +3.960e-001 +4.320e-001 +4.200e-001 +3.480e-001 +2.070e-001 +7.700e-002 -1.000e-002 -6.400e-002 -7.200e-002 -5.400e-002 -3.900e-002 -4.900e-002 -1.110e-001 -1.970e-001 -2.770e-001 -3.530e-001
```

```
1D_Inversion_Results_TEM.txt
-4.030e-001 -4.240e-001 -4.360e-001 -4.490e-001 -4.660e-001 -4.810e-001
-4.900e-001
    34.2385
                             25.23
  200.0000
                             44.71
                             69.97
    17.3512
       2.2102 10000000000.00
 <Date: Mon May 16 19:28:39 2005</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NEXT TO RIVER<Place: HANOTHIAN
                                                                                                                      6 Ampl=OFF
*****
0.000/\text{rms}=231.00
+9.185e+001 +8.503e+001 +7.925e+001 +7.214e+001 +6.406e+001 +5.775e+001
+5.284e+001 +4.752e+001 +4.228e+001 +3.858e+001 +3.565e+001 +3.220e+001 +2.828e+001 +2.509e+001 +2.252e+001 +1.967e+001 +1.692e+001 +1.512e+001
+1.391e+001
                      -9.000e-001 -9.000e-001 -9.000e-001 -8.950e-001 -8.380e-001
+6.590e-001 +4.480e-001 +2.570e-001 +3.000e-002 -1.980e-001 -3.220e-001 -3.780e-001 -4.060e-001 -4.110e-001 -4.000e-001 -3.870e-001 -3.730e-001 -3.710e-001 -3.820e-001 -3.990e-001 -4.200e-001 -4.360e-001 -4.410e-001
-4.390e-001 -4.310e-001 -4.210e-001 -4.170e-001 -4.220e-001 -4.380e-001
-4.580e-001 -4.690e-001 -4.740e-001 -4.730e-001 -4.630e-001 -4.430e-001
-4.130e-001
38.7771
                               2.00
  200.0000
                             49.30
    17.3704
5.5834
                             35.98
                             26.86
       3.0000 10000000000.00
<Date: Tue Jun 17 06:52:45 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                      6 Ampl=OFF
<Remark: POWER LINES</pre>
<Place: SOLOCHIANA
 *****
#GEOSEC: 0053-B / 50.0/ 50.0/ 1.0/ 564173.000/ 3916018.000/ 59.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/r S [V/A]: +0.000e+000 +4.152e+001 +8.437e+001 +1.223e+002 +1.679e+002 +2.104e+002 +2.331e+002 +2.421e+002 +2.421e+00
                                                                                                                                     0.000/rms=496.00
+2.319e+002 +2.167e+002 +1.976e+002 +1.817e+002 +1.687e+002 +1.532e+002
+1.361e+002 +1.228e+002 +1.123e+002 +1.008e+002 +8.964e+001 +8.210e+001 +7.669e+001 +7.106e+001 +6.546e+001 +6.133e+001 +5.797e+001 +5.406e+001 +4.980e+001 +4.647e+001 +4.372e+001 +4.037e+001 +3.624e+001 +3.245e+001
+2.892e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.940e-001 +8.370e-001 +6.300e-001 +3.950e-001 +2.260e-001 +6.100e-002 -1.070e-001 -2.210e-001 -2.920e-001 -3.460e-001 -3.790e-001 -3.960e-001 -4.070e-001 -4.200e-001
-4.330e-001 -4.400e-001 -4.400e-001 -4.330e-001 -4.160e-001 -3.940e-001
 -3.740e-001 -3.530e-001 -3.390e-001 -3.370e-001 -3.390e-001 -3.430e-001
 -3.470e-001 -3.540e-001 -3.650e-001 -3.920e-001 -4.360e-001 -4.700e-001
 -4.870e-001
  200.0000
                               3.74
                             67.35
  200,0000
    22.1778
18.9391
                             25.90
                             75.50
       4.7471 10000000000.00
<Date: Tue Jun 17 07:20:45 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: NEAR WELL AND CONTAMINATION</pre>
<Place: SOLOCHIANA
 ******
                                              / 50.0/ 50.0/ 1.0/ 563898.000/ 3916245.000/
#GEOSEC: 0054
51.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                   0.000 DH =
                                                                                                                                    0.000/\text{rms}=219.00
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +2.397e+001 +4.214e+001 +5.507e+001 +6.868e+001 +8.195e+001 +9.075e+001 +9.669e+001 +1.023e+002 +1.073e+002 +1.104e+002 +1.121e+002 +1.127e+002 +1.107e+002 +1.074e+002 +1.039e+002 +9.970e+001 +9.546e+001 +9.253e+001 +9.025e+001 +8.733e+001 +8.325e+001 +7.907e+001
+7.504e+001 +6.989e+001 +6.424e+001 +6.025e+001 +5.731e+001 +5.415e+001
+5.043e+001 +4.655e+001 +4.232e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.980e-001 -8.470e-001 +7.280e-001 +5.680e-001 +4.370e-001 +3.420e-001 +2.560e-001 +1.850e-001 +1.290e-001 +6.800e-002 -2.600e-002 -1.320e-001 -1.930e-001 -2.150e-001 -2.110e-001 -1.880e-001 -1.710e-001 -1.720e-001 -1.990e-001 -2.530e-001 -3.000e-001 -3.300e-001 -3.470e-001 -3.200e-001 -3.000e-001 -3.000e-001
-3.540e-001 -4.280e-001 -4.720e-001
   34.4216
                        4.66
  200.0000
                       43.50
   44.8666
                       72.35
                       20.00
   15.0303
   17.7737 10000000000.00
<Date: Tue Jun 17 07:50:05 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=</pre>
                                                                                             6 Ampl=OFF
<Remark: IN THE OLIVE TREES
<Place: WEST OF SOLOCHIANA</pre>
*****
#GEOSEC: 0055 / 50.0/ 50.0/ 1.
63.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                 1.0/ 563772.000/ 3916127.000/
                                                                              0.000 DH=
                                                                                                         0.000/\text{rms}=293.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.076e+001 +2.516e+001
+3.563e+001 +4.241e+001 +4.790e+001 +5.478e+001 +6.269e+001 +6.864e+001 +7.279e+001 +7.640e+001 +7.869e+001 +7.952e+001 +7.980e+001 +8.000e+001 +8.039e+001 +8.100e+001 +8.169e+001 +8.249e+001 +8.263e+001 +8.138e+001
+7.895e+001 +7.432e+001 +6.751e+001 +6.173e+001 +5.706e+001 +5.194e+001
+4.680e+001 +4.287e+001 +3.951e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.170e-001 +6.880e-001 +6.320e-001 +5.860e-001 +5.110e-001 +4.190e-001 +3.220e-001 +2.040e-001 +9.700e-002 +4.000e-002 +1.900e-002 +1.800e-002 +3.500e-002 +5.200e-002 +5.600e-002 +3.300e-002 -4.500e-002 -1.510e-001 -2.500e-001 -3.430e-001 -3.990e-001 -4.150e-001 -4.140e-001 -4.070e-001
-4.050e-001 -4.170e-001 -4.330e-001
   26.1995
                        6.81
                       38.81
  200.0000
                       55.99
22.26
   52.0127
   52.0127
     8.4202 10000000000.00
<Date: Tue Jun 17 08:14:09 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=
                                                                                             6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
<Place: BETWEEN SOLOCHIANA AND PINALI</pre>
******
#GEOSEC: 0056-B / 50.0/ 50.0/ 1.0/ 563573.000/ 3916164.000/ 64.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri S [V/A]: +0.000e+000 +1.444e+000 +4.652e+000 +7.565e+000 +1.093e+001 +1.439e+001 +1.691e+001 +1.889e+001 +2.414e+001 +2.414e+001 +2.672e+001
                                                                                                         0.000/rms=489.00
+2.916e+001 +3.247e+001 +3.664e+001 +4.028e+001 +4.321e+001 +4.624e+001
+4.839e+001 +4.888e+001 +4.843e+001 +4.708e+001 +4.485e+001 +4.277e+001 +4.099e+001 +3.893e+001 +3.674e+001 +3.502e+001 +3.345e+001 +3.123e+001 +2.809e+001 +2.511e+001 +2.247e+001 +1.937e+001 +1.618e+001 +1.393e+001
+1.227e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +8.720e-001 +7.610e-001 +6.510e-001 +5.860e-001 +5.440e-001 +5.220e-001 +5.210e-001
+5.270e-001 +5.270e-001 +5.090e-001 +4.710e-001 +4.090e-001 +2.950e-001
+1.310e-001 -7.000e-003 -1.050e-001 -1.880e-001 -2.430e-001 -2.650e-001
 -2.690e-001 -2.650e-001 -2.620e-001 -2.770e-001 -3.100e-001 -3.720e-001
-4.360e-001 -4.680e-001 -4.810e-001 -4.870e-001 -4.890e-001 -4.890e-001
-4.880e-001
   21.2187
                       12.49
  160.4547
                       38.75
   20.8280
                       24.21
     8.5950
                       33.07
```

```
1D_Inversion_Results_TEM.txt
    3.0000 10000000000.00
<Date: Tue Jun 17 08:49:32 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
<Place: EAST OF PINALI</pre>
#GEOSEC: 0057-B / 50.0/ 50.0/ 1.0 50.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                       1.0/ 563346.000/ 3916209.000/
                                                                  0.000 \, DH =
                                                                                           0.000/\text{rms}=262.00
S [V/A]: +0.000e+000 +6.650e-001 +2.821e+001 +4.487e+001 +5.622e+001 +6.146e+001 +6.299e+001 +6.369e+001 +6.409e+001 +6.367e+001 +6.214e+001
+5.986e+001 +5.608e+001 +5.113e+001 +4.709e+001 +4.407e+001 +4.094e+001
+3.811e+001 +3.622e+001 +3.482e+001 +3.322e+001 +3.143e+001 +2.995e+001
+2.874e+001 +2.735e+001 +2.597e+001 +2.500e+001 +2.425e+001 +2.327e+001
+2.174e+001 +1.990e+001 +1.787e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.960e-001 +6.430e-001 +2.410e-001 +9.700e-002 +5.300e-002 +4.000e-003 -8.800e-002 -1.900e-001
-2.730e-001 -3.420e-001 -3.770e-001 -3.780e-001 -3.630e-001 -3.310e-001
-2.890e-001 -2.610e-001 -2.500e-001 -2.490e-001 -2.570e-001 -2.630e-001 -2.610e-001 -2.480e-001 -2.250e-001 -2.080e-001 -2.110e-001 -2.590e-001 -3.660e-001 -4.500e-001 -4.850e-001
   55.0978
                     5.46
   58.1643
                    26.83
   14.1742
7.3988
                    51.61
                    24.95
    3.0000 10000000000.00
<Date: Tue Jun 17 09:19:17 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: IN OLIVE TREES, POWER LINES</pre>
<Place: EAST OF PINALI</pre>
*****
#GEOSEC: 0058-B / 50.0/ 50.0/ 1.0/ 563177.000/ 3916215.000/ 64.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +8.299e+000 +1.692e+001
                                                                                           0.000/\text{rms}=143.00
+2.155e+001 +2.390e+001 +2.564e+001 +2.780e+001 +3.056e+001 +3.307e+001
+3.540e+001 +3.840e+001 +4.191e+001 +4.469e+001 +4.676e+001 +4.882e+001 +5.045e+001 +5.126e+001 +5.169e+001 +5.201e+001 +5.220e+001 +5.225e+001 +5.220e+001 +5.200e+001 +5.157e+001 +5.103e+001 +5.042e+001 +4.946e+001
+4.801e+001 +4.655e+001 +4.518e+001 +4.345e+001 +4.155e+001 +4.020e+001
+3.928e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.990e-001 +6.500e-001 +4.590e-001 +4.120e-001 +4.080e-001 +4.160e-001 +4.220e-001
+4.220e-001 +4.080e-001 +3.730e-001 +3.240e-001 +2.710e-001 +1.990e-001
+1.230e-001 +7.400e-002 +4.700e-002 +2.700e-002 +1.100e-002 -1.000e-003 -1.300e-002 -3.000e-002 -5.300e-002 -7.300e-002 -9.400e-002 -1.240e-001 -1.610e-001 -1.880e-001 -2.040e-001 -2.100e-001 -1.980e-001 -1.710e-001
-1.410e-001
   16.1525
                     4.94
   73.1381
66.5764
                    48.17
                    20.00
   36.4820
                  104.77
   20.0000 10000000000.00
<Date: Tue Jun 17 09:45:56 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: IN OLIVE TREES
                                                                                 6 Ampl=OFF
<place: EAST OF PINALI</pre>
*****
#GEOSEC: 0059-B / 50.0/ 50.0/ 1.
55.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 562980.000/ 3916156.000/
                                                                   0.000 DH=
                                                                                           0.000/rms=125.00
               +0.000e+000 +0.000e+000 +0.000e+000 +8.031e+000 +2.010e+001
+2.890e+001 +3.450e+001 +3.891e+001 +4.426e+001 +5.048e+001 +5.570e+001 +6.017e+001 +6.570e+001 +7.208e+001 +7.734e+001 +8.155e+001 +8.615e+001 +9.021e+001 +9.223e+001 +9.285e+001 +9.222e+001 +8.982e+001 +8.682e+001 +8.383e+001 +7.999e+001 +7.571e+001 +7.254e+001 +7.004e+001 +6.715e+001 +6.374e+001 +6.050e+001 +5.722e+001 +5.246e+001 +4.601e+001 +4.021e+001
```

+3.522e+001

```
1D_Inversion_Results_TEM.txt
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.260e-001 +6.890e-001 +6.220e-001 +5.700e-001 +5.230e-001 +4.880e-001 +4.630e-001 +4.340e-001 +4.000e-001 +3.640e-001 +3.250e-001 +2.610e-001
+1.700e-001 +8.400e-002 +8.000e-003 -8.000e-002 -1.630e-001 -2.120e-001 -2.370e-001 -2.480e-001 -2.440e-001 -2.340e-001 -2.270e-001 -2.320e-001 -2.630e-001 -3.110e-001 -3.640e-001 -4.240e-001 -4.690e-001 -4.870e-001
-4.940e-001
   14.3202
                        3.75
  197.2729
                      23.54
 122.3601
                      72.09
   21.4310
                      94.99
     3.0000 10000000000.00
<Date: Tue Jun 17 10:10:48 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                         6 Ampl=OFF
<Remark: IN OLIVE TREES
<Place: PINALI</pre>
<*************************
******
#GEOSEC: 0060-B / 50.0 / 50.0 / 1.44.0 / 36 / 4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                              1.0/ 562752.000/ 3916176.000/
                                                                           0.000 DH =
                                                                                                    0.000/\text{rms}=299.00
                +0.000e+000 +0.000e+000 +2.061e+001 +3.923e+001 +5.411e+001
     [V/A]:
+6.\overline{507}e^{+001} +7.218e+001 +7.822e+001 +8.620e+001 +9.631e+001 +1.052e+002
+1.128e+002 +1.217e+002 +1.309e+002 +1.370e+002 +1.406e+002 +1.426e+002 +1.414e+002 +1.380e+002 +1.338e+002 +1.279e+002 +1.211e+002 +1.160e+002 +1.119e+002 +1.072e+002 +1.015e+002 +9.668e+001 +9.243e+001 +8.742e+001
+8.220e+001 +7.833e+001 +7.515e+001 +7.113e+001 +6.605e+001 +6.164e+001
+5.803e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.210e-001 +5.820e-001 +4.870e-001 +4.720e-001 +4.730e-001 +4.660e-001 +4.460e-001
+4.180e-001 +3.680e-001 +2.920e-001 +2.120e-001 +1.310e-001 +2.300e-002
-9.700e-002 -1.750e-001 -2.180e-001 -2.410e-001 -2.430e-001 -2.350e-001 -2.310e-001 -2.380e-001 -2.580e-001 -2.760e-001 -2.840e-001 -2.820e-001 -2.700e-001 +2.650e-001 +2.740e-001 -3.010e-001 -3.360e-001 -3.520e-001
-3.570e-001
   20.1825
  200.0000
                      20.13
  200.0000
                      78.75
   40.5518 10000000000.00
<Date: Tue Jun 17 10:44:08 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                         6 Ampl=OFF
<Remark: IN OLIVE TREES</pre>
<Place: PINALI
*****
#GEOSEC: 0061-B / 50.0/ 50.0/ 1.0/ 562493.000/ 3916069.000/ 31.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                                    0.000/rms=397.00
     [V/A]: +0.000e+000 +0.000e+000 +4.577e+000 +1.188e+001 +1.670e+001
+1.969e+001 +2.156e+001 +2.306e+001 +2.489e+001 +2.716e+001 +2.917e+001
+3.104e+001 +3.349e+001 +3.658e+001 +3.939e+001 +4.190e+001 +4.509e+001 +4.884e+001 +5.191e+001 +5.443e+001 +5.730e+001 +6.016e+001 +6.206e+001 +6.324e+001 +6.407e+001 +6.413e+001 +6.353e+001 +6.263e+001 +6.117e+001 +5.907e+001 +5.690e+001 +5.454e+001 +5.077e+001 +4.502e+001 +3.937e+001
+3.429e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.230e-001 +5.290e-001 +4.250e-001 +3.940e-001 +3.840e-001 +3.830e-001 +3.870e-001 +3.920e-001 +3.970e-001 +4.010e-001 +4.000e-001 +3.940e-001 +3.800e-001
+3.550e-001 +3.280e-001 +3.000e-001 +2.590e-001 +2.050e-001 +1.530e-001
+1.040e-001 +4.200e-002 -2.900e-002 -7.800e-002 -1.130e-001 -1.470e-001 -1.910e-001 -2.440e-001 -3.070e-001 -3.930e-001 -4.640e-001 -4.890e-001
-4.960e-001
   15.8240
                       4.47
   52.4335
                      20.00
   93.4409
                    122.60
   13.9666 10000000000.00
<Date: Tue Jun 17 11:12:27 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                         6 Ampl=OFF
<Remark: WEST OF RIVER, NOT EAST!!</pre>
<Place: NEAR GEROP.RIVER</pre>
```

```
1D_Inversion_Results_TEM.txt
```

```
_************
                                                                                  .
**********
*****
#GEOSEC: 0063-B / 50.0 / 50.0 / 180.0 /32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                     1.0/ 562120.000/ 3916222.000/
                                                                                   0.000 DH=
                                                                                                               0.000/rms=110.00
     [V/A]: +6.364e+000 +1.681e+001 +2.472e+001 +3.034e+001 +3.569e+001
+4.014e+001 +4.272e+001 +4.428e+001 +4.567e+001 +4.680e+001 +4.747e+001 +4.792e+001 +4.835e+001 +4.874e+001 +4.908e+001 +4.944e+001 +5.009e+001
+5.128e+001 +5.274e+001 +5.439e+001 +5.695e+001 +6.064e+001 +6.420e+001 +6.747e+001 +7.157e+001 +7.617e+001 +7.972e+001 +8.260e+001 +8.574e+001
+8.780e+001 +8.652e+001 +8.207e+001

Err[V/A]: -9.000e-001 -9.000e-001 -8.690e-001 -7.570e-001 +5.790e-001

+3.900e-001 +2.690e-001 +1.960e-001 +1.380e-001 +9.500e-002 +7.100e-002
+5.600e-002 +4.400e-002 +3.900e-002 +4.500e-002 +6.000e-002 +9.200e-002
+1.400e-001 +1.870e-001 +2.290e-001 +2.740e-001 +3.120e-001 +3.280e-001 +3.270e-001 +3.090e-001 +2.780e-001 +2.520e-001 +2.260e-001 +1.660e-001 +5.000e-003 -2.250e-001 -3.950e-001
    21.1366
                          2.02
    56.2943
                        62.87
  200.0000
                       150.00
    20.3267 10000000000.00
<Date: Tue Jun 17 12:10:01 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                   6 Ampl=OFF
<Remark: WEST OF RIVER</pre>
*****
#GEOSEC: 0064-B / 50.0/ 50.0/ 1.0/ 561965.000/ 3916388.000/ 84.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +1.190e+000 +1.215e+001 +1.975e+001 +2.638e+001
                                                                                                               0.000/rms=174.00
+3.159e+001 +3.456e+001 +3.636e+001 +3.778e+001 +3.858e+001 +3.878e+001
+3.877e+001 +3.864e+001 +3.854e+001 +3.856e+001 +3.869e+001 +3.902e+001
+3.877e+001 +3.804e+001 +3.834e+001 +3.836e+001 +3.803e+001 +3.902e+001 +4.972e+001 +4.058e+001 +4.155e+001 +4.301e+001 +4.499e+001 +4.675e+001 +4.817e+001 +4.961e+001 +5.057e+001 +5.068e+001 +5.032e+001 +4.949e+001 +4.828e+001 +4.725e+001 +4.640e+001 +4.527e+001 +4.352e+001 +4.133e+001
+3.873e+001
                   -9.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +7.960e-001
Err[V/A]:
+5.490e-001 +3.760e-001 +2.620e-001 +1.510e-001 +5.900e-002 +1.200e-002 -9.000e-003 -1.500e-002 -5.000e-003 +1.400e-002 +3.400e-002 +6.500e-002 +1.070e-001 +1.440e-001 +1.740e-001 +2.040e-001 +2.200e-001 +2.120e-001
+1.870e-001 +1.320e-001 +4.900e-002 -2.100e-002 -6.900e-002 -1.060e-001 -1.220e-001 -1.250e-001 -1.300e-001 -1.600e-001 -2.390e-001 -3.340e-001
-4.060e-001
   19.5705
                          2.00
    43.4457
                         66.20
   96.8397
                        64.42
                        88.82
    10.1122
      1.0000 10000000000.00
<Date: Tue Jun 17 12:44:35 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                   6 Ampl=OFF
<Remark: WEST OF GEROP. RIVER</pre>
*****
#GEOSEC: 0065-B / 50.0/ 50.0/ 1.0/ 561770.000/ 3916504.000/ 78.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +0.000e+000 +7.918e+000 +2.011e+001 +2.845e+001 +3.336e+001 +3.582e+001 +3.738e+001 +3.881e+001 +3.995e+001 +4.062e+001
                                                                                                               0.000/rms = 97.00
+4.108e+001 +4.164e+001 +4.235e+001 +4.300e+001 +4.359e+001 +4.431e+001 +4.515e+001 +4.584e+001 +4.642e+001 +4.775e+001 +4.758e+001 +4.733e+001 +4.643e+001 +4.472e+001 +4.293e+001 +4.120e+001 +3.895e+001
+3.622e+001 +3.384e+001 +3.169e+001 +2.895e+001 +2.572e+001 +2.314e+001
+2.111e+001
+2.11e+001

Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.250e-001

+4.780e-001 +3.100e-001 +2.330e-001 +1.660e-001 +1.120e-001 +8.300e-002

+7.400e-002 +7.700e-002 +8.400e-002 +9.000e-002 +9.200e-002 +9.100e-002

+8.900e-002 +8.700e-002 +8.200e-002 +6.600e-002 +2.800e-002 -2.100e-002

-7.300e-002 -1.400e-001 -2.060e-001 -2.480e-001 -2.740e-001 -3.010e-001

-3.320e-001 -3.620e-001 -3.880e-001 -4.170e-001 -4.380e-001 -4.470e-001
```

```
1D_Inversion_Results_TEM.txt
-4.500e-001
  17.6510
                   2.00
   48.5949
                  56.89
   35.3990
                  46.87
    7.2875
                  50.36
    2.3489 10000000000.00
<Date: Tue Jun 17 13:09:47 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: WEST OF GEROP. RIVER
                                                                         6 Ampl=OFF
<Place: EAST OF DALAMPELOS
<pre>
*****
#GEOSEC: 0066-B / 50.0/ 50.0/ 1.
61.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 561501.000/ 3916675.000/
                                                             0.000 DH=
                                                                                  0.000/\text{rms}=149.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +8.214e+000 +1.414e+001 +1.698e+001 +1.801e+001 +1.849e+001 +1.881e+001 +1.904e+001 +1.923e+001
+1.948e+001 +1.986e+001 +2.048e+001 +2.109e+001 +2.167e+001 +2.242e+001
+2.333e+001 +2.413e+001 +2.483e+001 +2.572e+001 +2.675e+001 +2.758e+001
+2.823e+001 +2.896e+001 +2.976e+001 +3.045e+001 +3.114e+001 +3.220e+001 +3.378e+001 +3.536e+001 +3.677e+001 +3.826e+001 +3.907e+001 +3.872e+001
+3.779e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.910e-001 +4.860e-001 +2.300e-001 +1.320e-001 +7.400e-002 +5.600e-002 +7.100e-002 +9.500e-002 +1.240e-001 +1.570e-001 +1.760e-001 +1.850e-001 +1.890e-001 +1.920e-001 +1.940e-001 +1.950e-001 +1.930e-001 +1.830e-001 +1.680e-001
+1.530e-001 +1.380e-001 +1.340e-001 +1.460e-001 +1.690e-001 +2.080e-001
+2.490e-001 +2.640e-001 +2.450e-001 +1.670e-001 +1.800e-002 -1.130e-001
-2.100e-001
   11.4146
                   2.00
  24.5750
                  34.79
   59.6746
                  38.84
                 150.00
   31.6858
    2.0000 10000000000.00
<Date: Tue Jun 17 13:38:34 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: FENCES</pre>
<Place: DALAMPELOS
*****
0.000/rms=326.00
+4.066e+001 +4.146e+001 +4.176e+001 +4.163e+001 +4.084e+001 +3.969e+001 +3.838e+001 +3.644e+001 +3.383e+001 +3.155e+001 +2.953e+001 +2.699e+001 +2.400e+001 +2.147e+001 +1.929e+001 +1.668e+001 +1.390e+001 +1.187e+001
+1.037e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.780e-001 +5.200e-001 +3.110e-001 +2.300e-001 +1.840e-001 +1.750e-001 +1.950e-001
+2.240e-001 +2.640e-001 +2.950e-001 +2.990e-001 +2.800e-001 +2.300e-001 +1.510e-001 +7.900e-002 +1.900e-002 -5.200e-002 -1.320e-001 -1.940e-001 -2.430e-001 -2.930e-001 -3.380e-001 -3.670e-001 -3.880e-001 -4.140e-001
-4.440e-001 -4.640e-001 -4.770e-001 -4.870e-001 -4.910e-001 -4.920e-001 -4.930e-001
  12.0191
                   2.00
   41.2793
                  45.38
  52.2497
5.5161
                  24.68
                  27.48
    2.0000 10000000000.00
<Date: Wed Jun 18 07:03:01 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: FENCES
<Place: DALAMPELOS
******
                            / 50.0/ 50.0/ 1.0/ 561139.000/ 3916394.000/
#GEOSEC: 0068-B
64.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                             0.000 DH =
                                                                                 0.000/\text{rms}=361.00
                                              Σελίδα 20
```

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1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +0.000e+000 +4.229e+000 +1.552e+001 +2.333e+001 +2.792e+001 +3.043e+001 +3.224e+001 +3.429e+001 +3.654e+001 +3.839e+001 +3.994e+001 +4.180e+001 +4.384e+001 +4.542e+001 +4.659e+001 +4.777e+001
+4.872e+001 +4.918e+001 +4.934e+001 +4.928e+001 +4.891e+001 +4.841e+001
+4.792e+001 +4.734e+001 +4.690e+001 +4.684e+001 +4.708e+001 +4.775e+001
+4.895e+001 +5.013e+001 +5.111e+001 +5.202e+001 +5.228e+001 +5.163e+001
+5.037e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.610e-001
+5.400e-001 +3.880e-001 +3.350e-001 +3.020e-001 +2.780e-001 +2.640e-001
+2.520e-001 +2.350e-001 +2.110e-001 +1.850e-001 +1.570e-001 +1.180e-001 +7.300e-002 +3.700e-002 +9.000e-003 -2.100e-002 -5.000e-002 -6.600e-002 -6.900e-002 -5.800e-002 -2.400e-002 +1.600e-002 +5.500e-002 +9.900e-002 +1.320e-001 +1.370e-001 +1.180e-001 +6.500e-002 -2.900e-002 -1.240e-001
-2.050e-001
   15.6824
                      2.00
   46.9240
                     20.00
   60.6122
                     59.72
   32.8465
                   150.00
    2.0000 10000000000.00
<Date: Wed Jun 18 07:43:14 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: POWER LINES</pre>
<Place: DALAMPELOS
<
*****
#GEOSEC: 0069-B / 50.0/ 50.0/ 1. 78.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         1.0/ 560965.000/ 3916317.000/
                                                                     0.000 DH =
                                                                                               0.000/rms=171.00
S [V/A]: +0.000e+000 +0.000e+000 +8.603e+000 +1.743e+001 +2.214e+001 +2.374e+001 +2.409e+001 +2.417e+001 +2.428e+001 +2.453e+001 +2.491e+001
+2.542e+001 +2.630e+001 +2.764e+001 +2.899e+001 +3.025e+001 +3.184e+001
+3.359e+001 +3.491e+001 +3.588e+001 +3.690e+001 +3.781e+001 +3.838e+001 +3.875e+001 +3.908e+001 +3.937e+001 +3.961e+001 +3.993e+001 +4.057e+001
+4.180e+001 +4.324e+001 +4.460e+001 +4.597e+001 +4.622e+001 +4.476e+001
+4.246e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.410e-001
+1.770e-001 +4.600e-002 +2.300e-002 +3.500e-002 +6.900e-002 +1.120e-001
+1.560e-001 +2.070e-001 +2.530e-001 +2.760e-001 +2.800e-001 +2.660e-001 +2.360e-001 +2.030e-001 +1.730e-001 +1.380e-001 +1.020e-001 +7.600e-002 +5.800e-002 +4.200e-002 +3.700e-002 +4.700e-002 +7.000e-002 +1.160e-001
+1.740e-001 +2.050e-001 +1.930e-001 +1.040e-001 -9.100e-002 -2.630e-001
-3.700e-001
   18.1266
   28.3629
                     20.09
   55.3806
                     62.95
   32.0194
                   150.00
    2.0000 10000000000.00
<Date: Wed Jun 18 08:09:05 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: IN OLIVE TREES</pre>
<Place: DALAMPELOS
*****
#GEOSEC: 0070-B / 50.0 / 50.0 / 1.64.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                           1.0/
                                                                    560622.000/ 3916381.000/
                                                                     0.000 DH=
                                                                                               0.000/rms=165.00
S [V/A]: +0.000e+000 +0.000e+000 +1.029e+001 +2.638e+001 +3.810e+001 +4.544e+001 +4.926e+001 +5.188e+001 +5.462e+001 +5.721e+001 +5.889e+001
+6.000e+001 +6.101e+001 +6.183e+001 +6.231e+001 +6.254e+001 +6.259e+001
+6.221e+001 +6.150e+001 +6.063e+001 +5.938e+001 +5.794e+001 +5.695e+001 +5.634e+001 +5.589e+001 +5.573e+001 +5.581e+001 +5.604e+001 +5.657e+001 +5.756e+001 +5.852e+001 +5.910e+001 +5.873e+001 +5.575e+001 +5.114e+001
+4.631e+001
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.430e-001
+5.240e-001 +3.590e-001 +2.940e-001 +2.400e-001 +1.840e-001 +1.410e-001 +1.090e-001 +7.800e-002 +5.300e-002 +3.400e-002 +1.600e-002 -1.100e-002 -5.000e-002 -8.300e-002 -1.050e-001 -1.170e-001 -1.080e-001 -8.600e-002 -6.100e-002 -3.100e-002 -1.000e-003 +2.000e-002 +4.000e-002 +6.800e-002 +9.200e-002 +8.200e-002 +2.100e-002 -1.350e-001 -3.410e-001 -4.390e-001
-4.760e-001
```

```
1D_Inversion_Results_TEM.txt
  16.8642
                   2.00
                  45.80
   78.3593
   42.5829
                 126.87
  24.0580
                  57.40
    2.1898 10000000000.00
<Date: Wed Jun 18 08:45:33 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: NEAR THE STREET</pre>
<Place: BETWEEN G-12 AND G-17
#GEOSEC: 0071-B / 50.0/ 50.0/ 1.0/ 560323.000/ 3916769.000/ 83.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=2014.00
S [V/A]: +0.000e+000 +2.317e+001 +4.562e+001 +6.360e+001 +8.636e+001 +1.168e+002 +1.468e+002 +1.757e+002 +2.131e+002 +2.523e+002 +2.750e+002 +2.847e+002 +2.859e+002 +2.777e+002 +2.665e+002 +2.554e+002 +2.406e+002
+2.847e+002 +2.839e+002 +2.777e+002 +2.863e+002 +2.334e+002 +2.406e+002 +2.228e+002 +2.078e+002 +1.951e+002 +1.794e+002 +1.608e+002 +1.452e+002 +1.319e+002 +1.163e+002 +9.979e+001 +8.815e+001 +7.955e+001 +7.078e+001 +6.281e+001 +5.765e+001 +5.406e+001 +5.040e+001 +4.672e+001 +4.373e+001
+4.097e+001
              -9.000e-001 -9.000e-001 -9.000e-001 -8.880e-001 +8.590e-001
Err[V/A]:
+8.340e-001 +8.140e-001 +7.880e-001 +7.180e-001 +5.520e-001 +3.340e-001
+1.370e-001 -5.300e-002 -1.850e-001 -2.480e-001 -2.820e-001 -3.120e-001 -3.380e-001 -3.560e-001 -3.730e-001 -3.970e-001 -4.270e-001 -4.470e-001
-4.600e-001 -4.690e-001 -4.710e-001 -4.680e-001 -4.610e-001 -4.450e-001
-4.160e-001 -3.850e-001 -3.580e-001 -3.350e-001 -3.330e-001 -3.580e-001
-3.870e-001
 100.0000
                   2.00
                 107.49
 200.0000
  18.4844
                  33.96
    9.0500
                  81.58
    2.0000 10000000000.00
<Date: Wed Jun 18 10:09:54 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: NEAR A CLIFF, NOT SQUARE</pre>
<Place: NORTH OF G-17
*****
#GEOSEC: 0072-B / 50.0/ 50.0/ 1.
66.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 560625.000/ 3916834.000/
                                                              0.000 DH=
                                                                                   0.000/rms=341.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +8.044e+000 +1.575e+001 +2.093e+001 +2.416e+001 +2.673e+001 +3.001e+001 +3.416e+001 +3.806e+001
+4.180e+001 +4.696e+001 +5.368e+001 +5.993e+001 +6.560e+001 +7.283e+001
+8.111e+001 +8.738e+001 +9.189e+001 +9.599e+001 +9.852e+001 +9.898e+001 +9.846e+001 +9.704e+001 +9.461e+001 +9.197e+001 +8.901e+001 +8.421e+001
+7.688e+001 +6.969e+001 +6.325e+001 +5.563e+001 +4.781e+001 +4.235e+001
+3.841e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.990e-001 +7.470e-001 +6.040e-001 +5.580e-001 +5.420e-001 +5.420e-001 +5.590e-001 +5.650e-001 +5.650e-001 +5.550e-001 +5.390e-001 +5.050e-001
+4.430e-001 +3.700e-001 +2.920e-001 +1.880e-001 +7.200e-002 -7.000e-003
-5.600e-002 -1.000e-001 -1.450e-001 -1.920e-001 -2.480e-001 -3.280e-001
-4.060e-001 -4.460e-001 -4.630e-001 -4.700e-001 -4.690e-001 -4.620e-001 -4.530e-001
    6.7305
                 2.00
129.79
 151.6678
   20.9453
                  93.90
    2.5140
                  20.00
   28.6109 10000000000.00
<Date: Wed Jun 18 10:41:38 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: NEAR A CLIFF
<Place: EAST OF 0071</pre>
******
#GEOSEC: 0073-B / 50.0/ 50.0/ 1.0/ 560893.000/ 3916712.000/ 64.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                 0.000/\text{rms} = 858.00
                                              Σελίδα 22
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +0.000e+000 +9.861e+000 +2.027e+001 +2.656e+001 +2.957e+001 +3.082e+001 +3.154e+001 +3.224e+001 +3.291e+001 +3.342e+001 +3.389e+001 +3.455e+001 +3.547e+001 +3.639e+001 +3.727e+001 +3.848e+001
+4.007e+001 +4.159e+001 +4.308e+001 +4.522e+001 +4.825e+001 +5.130e+001
+5.430e+001 +5.830e+001 +6.287e+001 +6.585e+001 +6.742e+001 +6.783e+001 +6.648e+001 +6.423e+001 +6.161e+001 +5.742e+001 +5.097e+001 +4.445e+001
+3.847e+001
                  +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.220e-001
Err[V/A]:
+3.190e-001 +1.780e-001 +1.320e-001 +1.050e-001 +9.100e-002 +9.000e-002
+9.800e-002 +1.140e-001 +1.360e-001 +1.540e-001 +1.680e-001 +1.840e-001 +2.050e-001 +2.270e-001 +2.500e-001 +2.850e-001 +3.290e-001 +3.610e-001 +3.770e-001 +3.680e-001 +3.070e-001 +2.120e-001 +1.050e-001 -2.700e-002 -1.520e-001 -2.340e-001 -3.030e-001 -3.910e-001 -4.650e-001 -4.910e-001
-4.980e-001
   10.6877
                          2.00
                      144.89
    55.8794
                        47.37
   43.6136
     2.4357
                        20.00
     3.0241 10000000000.00
<Date: Wed Jun 18 11:08:34 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                  6 Ampl=OFF
<Remark: 500M EAST OF DALAMPELOS</pre>
*****
#GEOSEC: 0074-B / 50.0 / 50.0 / 1.49.0 / 36/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                                  1.0/ 561082.000/ 3916797.000/
                                                                                0.000 DH =
                                                                                                              0.000/rms=272.00
S [V/A]: +0.000e+000 +0.000e+000 +9.383e+000 +2.463e+001 +3.538e+001 +4.193e+001 +4.546e+001 +4.800e+001 +5.086e+001 +5.399e+001 +5.656e+001
+5.886e+001 +6.201e+001 +6.622e+001 +7.024e+001 +7.389e+001 +7.856e+001
+8.400e+001 +8.848e+001 +9.225e+001 +9.669e+001 +1.011e+002 +1.034e+002 +1.041e+002 +1.031e+002 +9.971e+001 +9.535e+001 +9.053e+001 +8.333e+001 +7.358e+001 +6.504e+001 +5.804e+001 +5.041e+001 +4.326e+001 +3.873e+001 +3.577e+001
                  +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.380e-001
Err[V/A]:
+5.150e-001 +3.670e-001 +3.160e-001 +2.840e-001 +2.620e-001 +2.580e-001
+2.680e-001 +2.900e-001 +3.170e-001 +3.300e-001 +3.310e-001 +3.220e-001 +3.040e-001 +2.870e-001 +2.700e-001 +2.370e-001 +1.700e-001 +8.700e-002 +2.000e-003 -1.030e-001 -2.110e-001 -2.870e-001 -3.490e-001 -4.130e-001
 -4.580e-001 -4.750e-001 -4.790e-001 -4.770e-001 -4.630e-001 -4.370e-001
-3.990e-001
    11.9304
                      140.15
  106.4152
     9.2766
                        30.06
     3.6162
                        30.60
     2.0000 10000000000.00
<Date: Wed Jun 18 11:33:54 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                  6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
*****
#GEOSEC: 0075-C
                                         50.0/ 50.0/
                                                                    1.0/ 561203.000/ 3916866.000/
50.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr

S [V/A]: +0.000e+000 +3.783e+000 +2.204e+001 +3.330e+001 +4.237e+001

+4.863e+001 +5.162e+001 +5.312e+001 +5.416e+001 +5.476e+001 +5.516e+001

+5.566e+001 +5.662e+001 +5.846e+001 +6.072e+001 +6.322e+001 +6.700e+001
                                                                                                              0.000/rms=493.00
+7.222e+001 +7.694e+001 +8.095e+001 +8.545e+001 +8.966e+001 +9.224e+001 +9.378e+001 +9.469e+001 +9.392e+001 +9.126e+001 +8.733e+001 +8.070e+001 +7.160e+001 +6.387e+001 +5.763e+001 +5.077e+001 +4.399e+001 +3.919e+001
+3.555e+001
Err[V/A]:
                  -9.000e-001 -9.000e-001 -9.000e-001 -8.920e-001 +7.160e-001
+4.170e-001 +2.400e-001 +1.450e-001 +7.800e-002 +4.600e-002 +5.100e-002 +7.500e-002 +1.210e-001 +1.860e-001 +2.440e-001 +2.880e-001 +3.300e-001 +3.520e-001 +3.450e-001 +3.180e-001 +2.660e-001 +1.950e-001 +1.370e-001 +8.700e-002 +1.100e-002 -1.110e-001 -2.290e-001 -3.230e-001 -4.030e-001 -4.480e-001 -4.620e-001 -4.660e-001 -4.660e-001 -4.620e-001 -4.590e-001
-4.570e-001
```

```
1D_Inversion_Results_TEM.txt
  15.0089
                  2.00
  86.9415
                146.04
  11.1226
                 20.00
    3.4503
                 40.19
    2.0000 10000000000.00
<Date: Wed Jun 18 12:07:08 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: IN THE OLIVE TREES
<Place: 350M NW OF DALAMPELOS</pre>
#GEOSEC: 0076-B / 50.0/ 50.0/ 1.0/ 561450.000/ 3917062.000/ 54.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=1212.00
S [V/A]: +0.000e+000 +0.000e+000 +5.766e+000 +1.522e+001 +2.122e+001 +2.409e+001 +2.506e+001 +2.542e+001 +2.548e+001 +2.537e+001 +2.531e+001
+2.535e+001 +2.562e+001 +2.622e+001 +2.697e+001 +2.776e+001 +2.888e+001
+3.032e+001 +3.163e+001 +3.281e+001 +3.434e+001 +3.627e+001 +3.805e+001
+3.973e+001 +4.203e+001 +4.501e+001 +4.759e+001 +4.973e+001 +5.192e+001 +5.317e+001 +5.259e+001 +5.080e+001 +4.721e+001 +4.199e+001 +3.758e+001
+3.412e+001
             +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.960e-001
+3.480e-001 +1.430e-001 +5.500e-002 -2.000e-003 -1.700e-002 -1.000e-003
+3.100e-002 +8.300e-002 +1.380e-001 +1.780e-001 +2.040e-001 +2.240e-001 +2.380e-001 +2.440e-001 +2.490e-001 +2.560e-001 +2.690e-001 +2.830e-001
+2.980e-001 +3.140e-001 +3.210e-001 +3.070e-001 +2.710e-001 +1.820e-001
+1.800e-002 -1.550e-001 -2.900e-001 -3.920e-001 -4.430e-001 -4.550e-001
-4.580e-001
  12.1166
                   2.00
                150.00
  41.5138
  41.5138
                 20.60
    2.5419
                  20.00
    2.0000 10000000000.00
<Date: Wed Jun 18 12:57:31 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
<Place: 300M SW OF G-52
*****
#GEOSEC: 0077-B / 50.0/ 50.0/ 1.
48.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                  1.0/ 561665.000/ 3916979.000/
                                                            0.000 DH=
                                                                                0.000/rms=315.00
S [V/A]: +0.000e+000 +0.000e+000 +1.456e+001 +2.983e+001 +3.859e+001 +4.109e+001 +4.070e+001 +3.990e+001 +3.879e+001 +3.763e+001 +3.688e+001
+3.645e+001 +3.624e+001 +3.635e+001 +3.669e+001 +3.710e+001 +3.770e+001
+3.847e+001 +3.917e+001 +3.977e+001 +4.050e+001 +4.122e+001 +4.165e+001 +4.186e+001 +4.195e+001 +4.196e+001 +4.198e+001 +4.207e+001 +4.224e+001 +4.244e+001 +4.249e+001 +4.238e+001 +4.198e+001 +4.103e+001 +3.962e+001
+3.777e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.600e-001 +9.400e-002 -9.100e-002 -1.340e-001 -1.420e-001 -1.240e-001 -9.300e-002 -5.700e-002 -1.000e-002 +3.600e-002 +6.600e-002 +8.200e-002 +9.300e-002
+1.010e-001 +1.040e-001 +1.030e-001 +9.400e-002 +7.200e-002 +4.700e-002
+2.500e-002 +7.000e-003 +2.000e-003 +9.000e-003 +1.800e-002 +2.300e-002 +1.400e-002 -6.000e-003 -3.400e-002 -8.000e-002 -1.600e-001 -2.550e-001 -3.380e-001
  31.0186
                   2.00
                150.00
  40.0130
  11.5368
16.7337
                 20.00
                  52.40
    2.0000 10000000000.00
<Date: Wed Jun 18 13:22:23 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
******
                           / 50.0/ 50.0/ 1.0/ 561881.000/ 3916972.000/
#GEOSEC: 0078-B
43.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                            0.000 DH =
                                                                              0.000/\text{rms}=997.00
                                            Σελίδα 24
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +1.155e+001 +8.392e+000 +8.213e+000 +8.796e+000 +9.742e+000 +1.066e+001 +1.113e+001 +1.135e+001 +1.149e+001 +1.170e+001 +1.198e+001 +1.235e+001 +1.294e+001 +1.381e+001 +1.470e+001 +1.556e+001 +1.672e+001
+1.820e+001 +1.953e+001 +2.071e+001 +2.222e+001 +2.400e+001 +2.548e+001
+2.673e+001 +2.820e+001 +2.981e+001 +3.102e+001 +3.199e+001 +3.309e+001
+3.427e+001 +3.521e+001 +3.597e+001 +3.679e+001 +3.741e+001 +3.744e+001
+3.694e+001
Err[V/A]: +5.000e-001 +4.300e-001 -1.670e-001 -4.160e-001 +4.200e-001 +2.920e-001 +1.700e-001 +9.900e-002 +7.300e-002 +1.090e-001 +1.690e-001 +2.220e-001 +2.750e-001 +3.270e-001 +3.590e-001 +3.750e-001 +3.850e-001 +3.900e-001 +3.870e-001 +3.810e-001 +3.690e-001 +3.490e-001 +3.280e-001 +3.080e-001 +2.800e-001 +2.470e-001 +2.000e-001 +1.800e-001 +1.800e-001 +1.800e-001
+1.640e-001 +1.520e-001 +1.380e-001 +1.060e-001 +4.000e-002 -4.700e-002
-1.340e-001
   3.9193
37.7310
                        2.00
                     149.99
   37.7310
                      34.79
   10.4923
                      44.30
     2.0000 10000000000.00
<Date: Wed Jun 18 13:45:51 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                           6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
*****
                                                             1.0/ 562099.000/ 3916959.000/
#GEOSEC: 0079-B
                                      50.0/ 50.0/
49.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                          0.000 DH =
                                                                                                      0.000/rms=189.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +7.133e+000 +1.332e+001 +1.678e+001 +1.793e+001 +1.824e+001 +1.811e+001 +1.771e+001 +1.735e+001
+1.713e+001 +1.699e+001 +1.707e+001 +1.733e+001 +1.771e+001 +1.837e+001
+1.945e+001 +2.064e+001 +2.188e+001 +2.371e+001 +2.627e+001 +2.873e+001 +3.103e+001 +3.396e+001 +3.729e+001 +3.972e+001 +4.142e+001 +4.287e+001 +4.346e+001 +4.302e+001 +4.202e+001 +4.009e+001 +3.706e+001 +3.400e+001 +3.104e+001
                 -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.980e-001
Err[V/A]:
+5.680e-001 +2.170e-001 +4.300e-002 -6.900e-002 -1.080e-001 -9.800e-002
-6.700e-002 -1.400e-002 +5.800e-002 +1.190e-001 +1.710e-001 +2.340e-001 +3.050e-001 +3.590e-001 +4.010e-001 +4.430e-001 +4.760e-001 +4.870e-001 +4.800e-001 +4.510e-001 +3.900e-001 +3.190e-001 +2.430e-001 +1.340e-001
-2.000e-003 -1.150e-001 -2.010e-001 -2.910e-001 -3.750e-001 -4.280e-001
-4.600e-001
 18.1162
200.0000
                      29.90
                     102.20
     7.8758
                      66.21
     1.9685 10000000000.00
<Date: Wed Jun 18 14:19:09 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                           6 Ampl=OFF
<Remark: IN THE OLIVE TREES
<Place: 250M SW OF G-53</pre>
<****************
*****
#GEOSEC: 0080-C / 50.0/ 50.0/ 1 73.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                               1.0/ 562236.000/ 3917140.000/
                                                                            0.000 DH =
0.000/\text{rms}=1143.00
S [V/A]: +0.000e+000 +0.000e+000 +1.447e+001 +3.008e+001 +4.836e+001 +7.116e+001 +9.270e+001 +1.126e+002 +1.369e+002 +1.604e+002 +1.734e+002 +1.794e+002 +1.814e+002 +1.785e+002 +1.729e+002 +1.663e+002 +1.563e+002
+1.435e+002 +1.331e+002 +1.251e+002 +1.170e+002 +1.101e+002 +1.064e+002
+1.044e+002 +1.032e+002 +1.027e+002 +1.023e+002 +1.013e+002 +9.865e+001 +9.297e+001 +8.627e+001 +7.950e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.970e-001
+8.740e-001 +8.450e-001 +8.050e-001 +7.110e-001 +5.180e-001 +3.130e-001 +1.500e-001 -4.000e-003 -1.320e-001 -2.160e-001 -2.750e-001 -3.290e-001 -3.610e-001 -3.630e-001 -3.460e-001 -3.040e-001 -2.310e-001 -1.590e-001 -1.000e-001 -4.600e-002 -2.300e-002 -4.600e-002 -1.030e-001 -2.060e-001 -3.270e-001 -4.020e-001 -4.440e-001
   67.2915
                        6.82
 200.0000
                      79.16
```

```
1D_Inversion_Results_TEM.txt
                    101.64
   28.7930
     1.0000 10000000000.00
<Date: Thu Jun 19 07:10:14 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                          6 Ampl=OFF
<Remark: IN THE OLIVE TREES</pre>
*****
                                  / 50.0/ 50.0/
#GEOSEC: 0081-C
                                                            1.0/ 562488.000/ 3917030.000/
#GEOSEC: 0081-C / 50.0/ 50.0/ 1.0/ 562488.000/ 3917030.000/ 70.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +1.103e+001 +5.330e+001 +8.887e+001 +1.333e+002 +1.804e+002 +2.113e+002 +2.312e+002 +2.472e+002 +2.538e+002 +2.502e+002 +2.422e+002 +2.292e+002 +2.128e+002 +1.993e+002 +1.885e+002 +1.763e+002 +1.638e+002 +1.546e+002 +1.474e+002 +1.392e+002 +1.302e+002 +1.231e+002 +1.174e+002 +1.112e+002 +1.051e+002 +1.013e+002 +9.852e+001 +9.539e+001 +9.126e+001 +8.678e+001 +8.204e+001 +7.540e+001 +6.737e+001 +6.106e+001
                                                                                                     0.000/\text{rms}=383.00
+5.617e+001
                 -9.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.850e-001
Err[V/A]:
+7.770e-001 +6.020e-001 +4.410e-001 +2.410e-001 +1.000e-002 -1.500e-001 -2.390e-001 -2.950e-001 -3.220e-001 -3.290e-001 -3.280e-001 -3.210e-001 -3.090e-001 -2.990e-001 -2.930e-001 -2.950e-001 -2.950e-001 -2.960e-001
-2.890e-001 -2.680e-001 -2.300e-001 -1.970e-001 -1.810e-001 -1.910e-001 -2.450e-001 -3.090e-001 -3.610e-001 -4.030e-001 -4.260e-001 -4.300e-001
-4.290e-001
   40.4686
                        3.50
  500.0001
                      62.22
   57.4491
                    150.00
   20.9724 10000000000.00
<Date: Thu Jun 19 08:00:27 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                          6 Ampl=OFF
*****
                                       50.0/ 50.0/
                                                            1.0/ 562651.000/ 3917075.000/
#GEOSEC: 0082-B
0.000/rms=642.00
+1.707e+002 +1.579e+002 +1.477e+002 +1.360e+002 +1.237e+002 +1.145e+002 +1.076e+002 +1.005e+002 +9.405e+001 +9.014e+001 +8.751e+001 +8.481e+001 +8.168e+001 +7.854e+001 +7.529e+001 +7.067e+001 +6.495e+001 +6.038e+001
+5.688e+001
                 -9.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.960e-001
Err[V/A]:
+8.460e-001 +6.740e-001 +4.250e-001 +1.110e-001 -1.690e-001 -3.010e-001 -3.580e-001 -3.890e-001 -4.000e-001 -3.980e-001 -3.920e-001 -3.840e-001 -3.780e-001 -3.760e-001 -3.780e-001 -3.770e-001 -3.670e-001 -3.500e-001 -3.150e-001 -2.620e-001 -2.160e-001 -1.860e-001 -1.750e-001
-2.010e-001 -2.470e-001 -2.920e-001 -3.340e-001 -3.580e-001 -3.570e-001
-3.470e-001
   51.8232
  500.0001
                      68.35
   44.7231
                     150.00
   24.7919 10000000000.00
<Date: Thu Jun 19 08:30:32 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: HARDROCK FLOOR! NOT SQUARE</pre>
                                                                                          6 Ampl=OFF
******
#GEOSEC: 0083-B / 50.0/ 50.0/ 1.
24.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 562805.000/ 3917132.000/
                                                                          0.000 DH =
                                                                                                     0.000/rms=111.00
S [V/A]: +1.513e+001 +3.591e+001 +4.159e+001 +4.128e+001 +3.816e+001 +3.388e+001 +3.076e+001 +2.854e+001 +2.634e+001 +2.445e+001 +2.333e+001 +2.267e+001 +2.220e+001 +2.220e+001 +2.220e+001 +2.250e+001 +2.307e+001
```

+2.396e+001 +2.484e+001 +2.565e+001 +2.669e+001 +2.785e+001 +2.875e+001 +2.946e+001 +3.024e+001 +3.104e+001 +3.163e+001 +3.207e+001 +3.251e+001 +3.281e+001 +3.289e+001 +3.285e+001 +3.266e+001 +3.218e+001 +3.130e+001

```
1D_Inversion_Results_TEM.txt
```

```
+2.991e+001
Err[V/A]: -9.000e-001 -8.920e-001 -2.860e-001 +1.910e-001 -3.700e-001 -4.040e-001 -3.940e-001 -3.730e-001 -3.340e-001 -2.750e-001 -2.130e-001
-1.530e-001 -7.700e-002 +7.000e-003 +6.800e-002 +1.130e-001 +1.590e-001
+1.960e-001 +2.130e-001 +2.180e-001 +2.120e-001 +1.950e-001 +1.750e-001 +1.570e-001 +1.370e-001 +1.180e-001 +1.030e-001 +8.700e-002 +6.200e-002 +2.900e-002 +2.000e-003 -2.000e-002 -5.100e-002 -1.210e-001 -2.310e-001
-3.330e-001
   55.0421
                      5.85
   17.1456
54.2569
                    20.00
                    64.58
   26.9420 10000000000.00
<Date: Thu Jun 19 10:06:55 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
******
#GEOSEC: 0085-B / 50.0/ 50.0/ 1.0/ 563018.000/ 3917072.000/ 25.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +8.881e+000 +3.022e+001 +3.729e+001 +3.668e+001
                                                                                            0.000/\text{rms}=117.00
+3.151e+001 +2.730e+001 +2.439e+001 +2.169e+001 +1.943e+001 +1.808e+001
+1.720e+001 +1.645e+001 +1.591e+001 +1.572e+001 +1.569e+001 +1.581e+001
+1.607e+001 +1.635e+001 +1.662e+001 +1.696e+001 +1.740e+001 +1.784e+001 +1.832e+001 +1.908e+001 +2.019e+001 +2.125e+001 +2.219e+001 +2.326e+001
+2.411e+001 +2.441e+001 +2.440e+001 +2.419e+001 +2.384e+001 +2.342e+001
+2.276e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -5.510e-001 -3.130e-001 -4.670e-001 -4.710e-001 -4.570e-001 -4.250e-001 -3.740e-001 -3.210e-001
-2.680e-001 -1.960e-001 -1.090e-001 -3.900e-002 +1.100e-002 +5.900e-002
+9.200e-002 +1.060e-001 +1.110e-001 +1.180e-001 +1.370e-001 +1.670e-001 +2.000e-001 +2.440e-001 +2.840e-001 +2.950e-001 +2.780e-001 +2.210e-001 +1.190e-001 +3.100e-002 -2.400e-002 -5.900e-002 -8.900e-002 -1.530e-001
-2.300e-001
 100,0000
                      4.70
   11.8527
                    20.00
                   123.65
   31.6606
                    64.88
    5.3361
    3.0000 10000000000.00
<Date: Thu Jun 19 11:16:11 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark: WEST TO THE RIVER</pre>
*****
#GEOSEC: 0086-B / 50.0/ 50.0/ 1.0/ 563239.000/ 3917178.000/ 28.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +1.648e+001 +2.684e+001 +3.069e+001 +3.196e+001
                                                                                            0.000/rms=151.00
+3.128e+001 +2.999e+001 +2.860e+001 +2.677e+001 +2.469e+001 +2.317e+001
+2.208e+001 +2.100e+001 +2.011e+001 +1.961e+001 +1.933e+001 +1.916e+001
+1.919e+001 +1.941e+001 +1.970e+001 +2.022e+001 +2.094e+001 +2.159e+001 +2.211e+001 +2.264e+001 +2.298e+001 +2.297e+001 +2.275e+001 +2.220e+001
+2.118e+001 +2.002e+001 +1.885e+001 +1.725e+001 +1.536e+001 +1.390e+001
+1.281e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.690e-001 -4.690e-001 +6.000e-002 -1.610e-001 -2.480e-001 -2.910e-001 -3.180e-001 -3.220e-001 -3.030e-001
-2.740e-001 -2.290e-001 -1.680e-001 -1.170e-001 -7.500e-002 -2.200e-002
+3.900e-002 +8.600e-002 +1.220e-001 +1.560e-001 +1.750e-001 +1.700e-001 +1.490e-001 +1.040e-001 +3.200e-002 -3.600e-002 -9.800e-002 -1.760e-001 -2.640e-001 -3.300e-001 -3.760e-001 -4.120e-001 -4.310e-001 -4.290e-001
-4.210e-001
   49.4011
   15.8071
27.7902
                    25.24
                    65.90
    4.0581
                    88.79
   20.0000 10000000000.00
<Date: Thu Jun 19 11:43:27 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
                                                   Σελίδα 27
```

```
1D_Inversion_Results_TEM.txt
<Remark: 300M EAST OF THE RIVER</pre>
<Place: 600M SOUTH OF ROUMELI
*****
#GEOSEC: 0087-B / 50.0/ 50.0/ 1.
52.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 563448.000/ 3917197.000/
                                                          0.000 DH =
                                                                               0.000/\text{rms}=251.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.237e+001 +2.388e+001
+3.258e+001 +3.812e+001 +4.224e+001 +4.665e+001 +5.056e+001 +5.255e+001
+5.325e+001 +5.299e+001 +5.157e+001 +4.986e+001 +4.826e+001 +4.631e+001
+4.425e+001 +4.279e+001 +4.175e+001 +4.076e+001 +4.003e+001 +3.972e+001 +3.963e+001 +3.960e+001 +3.947e+001 +3.905e+001 +3.838e+001 +3.711e+001
+3.510e+001 +3.307e+001 +3.111e+001 +2.842e+001 +2.491e+001 +2.174e+001
+1.896e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.990e-001 +7.810e-001 +6.280e-001 +5.340e-001 +4.250e-001 +2.800e-001 +1.460e-001
+3.600e-002 -7.400e-002 -1.600e-001 -2.000e-001 -2.140e-001 -2.140e-001
-1.990e-001 -1.760e-001 -1.500e-001 -1.120e-001 -6.400e-002 -3.000e-002 -1.100e-002 -1.000e-002 -4.200e-002 -9.300e-002 -1.480e-001 -2.170e-001 -2.870e-001 -3.880e-001 -3.880e-001 -4.280e-001 -4.700e-001 -4.890e-001
-4.960e-001
  27.6556
                  8.10
                 20.60
 171.0377
  27.9963
                116.07
    8.8359
                 20.43
    3.0000 10000000000.00
<Date: Thu Jun 19 12:26:51 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                      6 Ampl=OFF
<Remark: 300M EAST OF THE MAIN ROAD
<Place: 550M SOUTH OF ROUMELI</pre>
*****
#GEOSEC: 0088-B / 50.0/ 50.0/ 1.61.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 563630.000/ 3917289.000/
                                                          0.000 DH =
                                                                               0.000/\text{rms}=136.00
    [V/A]: +1.364e+001 +7.914e+000 +6.344e+000 +6.080e+000 +6.399e+000
+7.082e+000 +7.688e+000 +8.178e+000 +8.731e+000 +9.366e+000 +9.916e+000
+1.041e+001 +1.106e+001 +1.189e+001 +1.263e+001 +1.330e+001 +1.418e+001
+1.532e+001 +1.640e+001 +1.746e+001 +1.897e+001 +2.104e+001 +2.305e+001 +2.496e+001 +2.747e+001 +3.041e+001 +3.260e+001 +3.417e+001 +3.553e+001
+3.623e+001 +3.604e+001 +3.527e+001 +3.349e+001 +3.024e+001 +2.677e+001
+2.352e+001
Err[V/A]: +5.000e-001 +5.000e-001 +4.400e-001 +1.800e-002 +3.270e-001 +4.130e-001 +3.920e-001 +3.550e-001 +3.240e-001 +3.120e-001 +3.120e-001
+3.170e-001 +3.260e-001 +3.320e-001 +3.360e-001 +3.410e-001 +3.510e-001
+3.700e-001 +3.940e-001 +4.190e-001 +4.500e-001 +4.820e-001 +4.980e-001 +4.990e-001 +4.790e-001 +4.230e-001 +3.510e-001 +2.710e-001 +1.610e-001 +2.600e-002 -9.400e-002 -2.050e-001 -3.370e-001 -4.440e-001 -4.820e-001
-4.950e-001
  10.1650
                  8.37
                 20.00
  21.7382
  96.0277
                109.59
                 38.27
    4.3093
    3.0000 10000000000.00
<Date: Thu Jun 19 12:52:30 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                      6 Ampl=OFF
*****
#GEOSEC: 0089-B / 50.0/ 50.0/ 1.74.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                1.0/ 563834.000/ 3917271.000/
                                                         0.000 DH=
                                                                               0.000/\text{rms}=328.00
```

```
1D_Inversion_Results_TEM.txt
+6.090e-001 +3.330e-001 +1.820e-001 +6.300e-002 -4.300e-002 -1.170e-001 -1.680e-001 -2.190e-001 -2.660e-001 -2.990e-001 -3.230e-001 -3.460e-001 -3.650e-001 -3.750e-001 -3.800e-001 -3.830e-001 -3.850e-001 -3.870e-001
-3.910e-001 -4.010e-001 -4.180e-001 -4.340e-001 -4.480e-001 -4.620e-001
-4.720e-001 -4.760e-001 -4.760e-001 -4.730e-001 -4.630e-001 -4.490e-001
 -4.310e-001
    91.3417
                                 19.55
  193.7725
                                31.15
     16.0953
                                44.99
       3.0000 10000000000.00
<Date: Thu Jun 19 13:28:03 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                                    6 Ampl=OFF
<Remark: SOME FENCES, OLIVE TREES</pre>
<Place: 650M SE OF ROUMELI
</pre>
                                                        50.0/ 50.0/
                                                                                         1.0/ 563925.000/ 3917414.000/
#GEOSEC: 0090-B
67.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                                                    0.000/\text{rms}=312.00
                                                                                                            0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +8.410e-001 +2.690e+000 +4.988e+000 +7.244e+000 +8.645e+000 +9.526e+000 +1.031e+001 +1.098e+001 +1.144e+001 +1.181e+001 +1.230e+001 +1.294e+001 +1.356e+001 +1.415e+001 +1.501e+001
+1.621e+001 +1.741e+001 +1.861e+001 +2.032e+001 +2.255e+001 +2.448e+001
+2.603e+001 +2.758e+001 +2.867e+001 +2.892e+001 +2.873e+001 +2.805e+001
+2.665e+001 +2.500e+001 +2.324e+001 +2.074e+001 +1.760e+001 +1.501e+001
+1.295e+001
Err[V/A]:
                        +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +9.000e-001
+8.310e-001 +6.450e-001 +4.840e-001 +3.440e-001 +2.520e-001 +2.180e-001
+2.140e-001 +2.280e-001 +2.510e-001 +2.740e-001 +2.990e-001 +3.340e-001 +3.790e-001 +4.150e-001 +4.430e-001 +4.640e-001 +4.600e-001 +4.240e-001 +3.630e-001 +2.570e-001 +1.30e-001 +1.00e-001 +3.630e-001 +2.570e-001 +1.30e-001 +1.00e-001 +3.630e-001 +3.640e-001 +3.640e-00
 -2.900e-001 -3.710e-001 -4.260e-001 -4.670e-001 -4.890e-001 -4.950e-001
-4.970e-001
    12.3480
42.5093
                                 15.41
                                 24.76
     60.6576
                                62.59
       3.0000
                                 83.26
     20.0000 10000000000.00
<Date: Thu Jun 19 13:56:06 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                                    6 Ampl=OFF
<Remark: SOME FENCES</pre>
*****
                                                                                        1.0/ 565719.000/ 3917370.000/
#GEOSEC: 0091-B / 50.0 / 50.0 / 1.48.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                                                                            0.000 DH =
                                                                                                                                                    0.000/rms=113.00
S [V/A]: +0.000e+000 +0.000e+000 +1.647e+001 +2.722e+001 +3.577e+001 +4.250e+001 +4.718e+001 +5.096e+001 +5.551e+001 +6.068e+001 +6.464e+001 +6.754e+001 +7.024e+001 +7.189e+001 +7.212e+001 +7.167e+001 +7.070e+001
+6.957e+001 +6.900e+001 +6.890e+001 +6.929e+001 +7.026e+001 +7.125e+001
+7.206e+001 +7.289e+001 +7.363e+001 +7.413e+001 +7.451e+001 +7.478e+001 +7.445e+001 +7.331e+001 +7.156e+001 +6.854e+001 +6.421e+001 +6.032e+001
+5.699e+001
                        +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +7.770e-001
Err[V/A]:
+5.680e-001 +4.790e-001 +4.410e-001 +4.090e-001 +3.640e-001 +3.110e-001 +2.520e-001 +1.650e-001 +6.000e-002 -1.500e-002 -5.700e-002 -7.600e-002 -6.200e-002 -2.800e-002 +9.000e-003 +4.800e-002 +7.600e-002 +8.000e-002 +7.200e-002 +5.700e-002 +4.400e-002 +3.800e-002 +2.900e-002 +1.000e-003 -6.000e-002 -1.300e-001 -1.940e-001 -2.590e-001 -3.090e-001 -3.330e-001
 -3.460e-001
     26.8711
  132.4790
                                39.39
     45.4318
                                31.00
     88.5662
                              131.48
     21.6412 10000000000.00
 <Date: Tue Jun 24 06:54:19 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                                    6 Ampl=OFF
<Remark: NEXT TO A LITTLE RIVER</pre>
<Place: ACHLADES
```

```
1D_Inversion_Results_TEM.txt
```

```
_*********************************
                                                        .
**********
*****
#GEOSEC: 0092-B / 50.0/ 50.0/ 1
44.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 565548.000/ 3917265.000/
                                                         0.000 DH=
                                                                            0.000/rms=344.00
S [V/A]: +0.000e+000 +0.000e+000 +2.366e+000 +2.244e+001 +3.667e+001
+4.320e+001 +4.521e+001 +4.626e+001 +4.742e+001 +4.889e+001 +5.026e+001 +5.154e+001 +5.327e+001 +5.545e+001 +5.747e+001 +5.932e+001 +6.181e+001
+6.511e+001 +6.821e+001 +7.107e+001 +7.456e+001 +7.771e+001 +7.878e+001
+7.823e+001 +7.591e+001 +7.184e+001 +6.817e+001 +6.500e+001 +6.107e+001
+5.625e+001 +5.193e+001 +4.810e+001 +4.354e+001 +3.877e+001 +3.543e+001
+3.302e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.800e-001 +4.250e-001 +1.870e-001 +1.380e-001 +1.350e-001 +1.480e-001 +1.610e-001
+1.710e-001 +1.840e-001 +1.970e-001 +2.080e-001 +2.190e-001 +2.350e-001
+2.570e-001 +2.710e-001 +2.700e-001 +2.330e-001 +1.350e-001 +1.100e-002 -1.020e-001 -2.060e-001 -2.690e-001 -2.910e-001 -3.040e-001 -3.280e-001 -3.680e-001 -3.990e-001 -4.170e-001 -4.250e-001 -4.190e-001 -4.020e-001
-3.810e-001
  36.5375
74.9260
                  8.56
                 55.66
                 38.65
 138.9567
 138.9567
                 28.24
  11.8967 10000000000.00
<Date: Tue Jun 24 07:19:41 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                   6 Ampl=OFF
<Remark: POWER LINES, NEXT LITTLE RIVER</pre>
<Place: ACHLADES
<
                           50.0/ 50.0/
#GEOSEC: 0093-C
                                               1.0/ 565309.000/ 3917304.000/
51.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         0.000 DH =
                                                                            0.000/\text{rms}=282.00
            +0.000e+000 +0.000e+000 +5.738e+000 +1.287e+001 +1.695e+001
+1.895e+001 +2.001e+001 +2.084e+001 +2.188e+001 +2.316e+001 +2.433e+001 +2.544e+001 +2.692e+001 +2.879e+001 +3.048e+001 +3.195e+001 +3.382e+001
+3.604e+001 +3.801e+001 +3.984e+001 +4.233e+001 +4.553e+001 +4.830e+001 +5.053e+001 +5.278e+001 +5.425e+001 +5.431e+001 +5.357e+001 +5.187e+001
+4.920e+001 +4.674e+001 +4.462e+001 +4.208e+001 +3.917e+001 +3.664e+001
+3.425e+001
Err[V/A]:
            +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.320e-001
+3.600e-001 +2.660e-001 +2.520e-001 +2.530e-001 +2.660e-001 +2.800e-001 +2.930e-001 +3.030e-001 +3.030e-001 +3.030e-001
+3.010e-001 +3.080e-001 +3.200e-001 +3.350e-001 +3.380e-001 +3.180e-001 +2.750e-001 +1.910e-001 +6.400e-002 -4.700e-002 -1.320e-001 -2.080e-001
-2.620e-001 -2.850e-001 -2.950e-001 -3.050e-001 -3.280e-001 -3.640e-001
-3.970e-001
  22.1132
65.8621
                 13.68
                 57.21
 155.1932
                 34.16
 155.1932
                 23.84
  14.3838 10000000000.00
<Date: Tue Jun 24 07:44:52 2008</p>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                   6 Ampl=OFF
<Remark: IN OLIVE TREES</pre>
*****
#GEOSEC: 0094-B
                                              1.0/ 565144.000/ 3917333.000/
                            50.0/ 50.0/
59.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/S
S [V/A]: +2.963e+000 +2.278e+000 +3.498e+000 +5.157e+000 +7.368e+000
                                                                            0.000/\text{rms}=144.00
+9.560e+000 +1.085e+001 +1.152e+001 +1.193e+001 +1.203e+001 +1.198e+001
+1.192e+001 +1.189e+001 +1.194e+001 +1.207e+001 +1.226e+001 +1.259e+001
+1.312e+001 +1.368e+001 +1.424e+001 +1.505e+001 +1.608e+001 +1.698e+001
+1.773e+001 +1.860e+001 +1.946e+001 +2.001e+001 +2.034e+001 +2.051e+001
+2.028e+001 +1.967e+001 +1.884e+001 +1.754e+001 +1.587e+001 +1.454e+001
+1.356e+001
            +5.000e-001 -6.150e-001 -8.980e-001 -8.970e-001 +8.660e-001
Err[V/A]:
+7.040e-001 +4.760e-001 +2.850e-001 +1.140e-001 +4.000e-003 -2.800e-002
-2.300e-002 +2.000e-003 +4.400e-002 +8.600e-002 +1.240e-001 +1.700e-001
```

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1D_Inversion_Results_TEM.txt
+2.200e-001 +2.570e-001 +2.830e-001 +3.050e-001 +3.120e-001 +3.010e-001 +2.790e-001 +2.420e-001 +1.880e-001 +1.370e-001 +8.400e-002 +1.000e-015 -1.220e-001 -2.300e-001 -3.080e-001 -3.700e-001 -4.000e-001 -3.980e-001
-3.850e-001
  12.4964
43.5376
18.2262
                   24.68
                   35.86
                   24.68
  10.9514
                   25.69
    3.0000 10000000000.00
<Date: Tue Jun 24 08:12:59 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: NORTH OF ACHLADES, S OF G-81</pre>
<Place: ACHLADES
*****
                                50.0/ 50.0/
                                                   1.0/ 564921.000/ 3917260.000/
#GEOSEC: 0095-B
52.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH=
                                                                                     0.000/rms = 66.00
S [V/A]: +8.735e+000 +6.338e+000 +6.483e+000 +7.193e+000 +8.148e+000
+8.876e+000 +9.085e+000 +9.060e+000 +8.892e+000 +8.760e+000 +8.780e+000 +8.923e+000 +9.251e+000 +9.812e+000 +1.044e+001 +1.108e+001 +1.200e+001
+1.322e+001 +1.432e+001 +1.526e+001 +1.633e+001 +1.738e+001 +1.807e+001
+1.851e+001 +1.891e+001 +1.918e+001 +1.923e+001 +1.917e+001 +1.897e+001
+1.861e+001 +1.826e+001 +1.794e+001 +1.753e+001 +1.704e+001 +1.661e+001
+1.622e+001
Err[V/A]: -
Err[V/A]: +5.000e-001 +3.800e-001 -3.590e-001 -5.390e-001 +4.600e-001 +2.310e-001 +4.700e-002 -5.400e-002 -8.400e-002 -2.400e-002 +6.400e-002
+1.470e-001 +2.320e-001 +3.120e-001 +3.670e-001 +4.000e-001 +4.270e-001
+4.370e-001 +4.230e-001 +3.920e-001 +3.340e-001 +2.560e-001 +1.940e-001 +1.460e-001 +9.500e-002 +4.000e-002 -4.000e-003 -4.000e-002 -7.500e-002 -1.030e-001 -1.170e-001 -1.240e-001 -1.320e-001 -1.430e-001 -1.550e-001
-1.660e-001
  10.3752
                   18.46
                  35.02
32.31
 200.0000
  10.5155
  17.2874
                   30.83
  10.1005 10000000000.00
<Date: Tue Jun 24 08:38:14 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: NORTH OF ACHLADES
<Place: ACHLADES
*****
#GEOSEC: 0096-В
                               50.0/ 50.0/
                                                    1.0/ 564697.000/ 3917294.000/
38.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                              0.000 DH =
                                                                                     0.000/\text{rms}=191.00
S [V/A]: +0.000e+000 +0.000e+000 +2.885e+000 +1.102e+001 +1.677e+001 +2.017e+001 +2.174e+001 +2.260e+001 +2.320e+001 +2.344e+001 +2.339e+001 +2.323e+001 +2.296e+001 +2.258e+001 +2.225e+001 +2.196e+001 +2.164e+001
+2.133e+001 +2.114e+001 +2.105e+001 +2.101e+001 +2.105e+001 +2.113e+001
+2.122e+001 +2.136e+001 +2.156e+001 +2.178e+001 +2.200e+001 +2.233e+001
+2.277e+001 +2.319e+001 +2.359e+001 +2.417e+001 +2.509e+001 +2.617e+001
+2.745e+001
Err[V/A]:
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.670e-001
+5.240e-001 +3.070e-001 +1.940e-001 +9.500e-002 +1.500e-002 -3.000e-002 -5.400e-002 -7.100e-002 -8.200e-002 -8.600e-002 -8.500e-002 -7.700e-002 -5.900e-002 -3.900e-002 -2.200e-002 -2.000e-003 +1.700e-002 +2.700e-002 +3.300e-002 +4.100e-002 +5.300e-002 +6.500e-002 +7.700e-002 +8.900e-002 +1.020e-001 +1.130e-001 +1.270e-001 +1.580e-001 +2.160e-001 +2.860e-001
+3.530e-001
   22.4541
                   29.23
   16.8517
                  20.00
   30.1833
                 150.00
 177.1283
                 150.00
    4.4286 10000000000.00
<Date: Tue Jun 24 09:04:48 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: NORTH-WEST OF ACHLADES</pre>
<Place: ACHLADES
<
```

## 1D\_Inversion\_Results\_TEM.txt

```
******
#GEOSEC: 0097-B
                                     50.0/ 50.0/
                                                           1.0/ 564419.000/ 3917317.000/
35.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                       0.000 \text{ DH} =
                                                                                               0.000/rms=231.00
               +0.000e+000 +0.000e+000 +3.603e+000 +1.747e+001 +2.759e+001
+3.360e+001 +3.639e+001 +3.782e+001 +3.858e+001 +3.819e+001 +3.706e+001
+3.575e+001 +3.398e+001 +3.200e+001 +3.051e+001 +2.940e+001 +2.826e+001 +2.722e+001 +2.657e+001 +2.616e+001 +2.583e+001 +2.567e+001 +2.570e+001
+2.585e+001 +2.616e+001 +2.665e+001 +2.710e+001 +2.746e+001 +2.778e+001 +2.780e+001 +2.741e+001 +2.674e+001 +2.555e+001 +2.389e+001 +2.253e+001
+2.154e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.790e-001 +5.510e-001 +3.160e-001 +1.790e-001 +3.400e-002 -1.120e-001 -1.980e-001 -2.400e-001 -2.610e-001 -2.600e-001 -2.450e-001 -2.250e-001 -1.940e-001 -1.560e-001 -1.210e-001 -9.000e-002 -5.200e-002 -9.000e-003 +2.500e-002 +5.200e-002 +7.800e-002 +9.500e-002 +7.900e-002 +3.700e-002 -4.400e-002 -1.290e-001 -2.010e-001 -2.690e-001 -3.040e-001 -2.950e-001
-2.710e-001
   34.5197
                     27.17
   15.1621
35.1368
                     20.00
                    92.25
72.69
    7.4296
   18.2278 10000000000.00
<Date: Tue Jun 24 09:40:24 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: NORTH-WEST OF ACHLADES</pre>
<Place: ACHLADES
*****
#GEOSEC: 0098-B / 50.0 / 50.0 / 1.40.0 / 36 / 50 / 22222 SPM=0 K= 0.000e+000 H=
                                                           1.0/ 564294.000/ 3917172.000/
                                                                       0.000 DH =
                                                                                               0.000/rms=287.00
               +0.000e+000 +0.000e+000 +5.245e+000 +1.732e+001 +2.618e+001
+3.171e+001 +3.448e+001 +3.605e+001 +3.714e+001 +3.735e+001 +3.685e+001
+3.609e+001 +3.496e+001 +3.363e+001 +3.260e+001 +3.183e+001 +3.104e+001 +3.033e+001 +2.990e+001 +2.963e+001 +2.939e+001 +2.921e+001 +2.909e+001 +2.812e+001 +2.829e+001 +2.812e+001
+2.798e+001 +2.790e+001 +2.780e+001 +2.751e+001 +2.663e+001 +2.516e+001
+2.327e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.660e-001 +5.520e-001 +3.440e-001 +2.220e-001 +9.500e-002 -3.000e-002 -1.080e-001
-1.500e-001 -1.730e-001 -1.760e-001 -1.660e-001 -1.490e-001 -1.250e-001 -9.500e-002 -7.100e-002 -5.400e-002 -3.800e-002 -2.700e-002 -2.400e-002 -2.500e-002 -3.100e-002 -3.800e-002 -4.000e-002 -3.800e-002 -3.000e-002 -2.000e-002 -2.100e-002 -3.900e-002 -1.050e-001 -2.400e-001 -3.710e-001
-4.480e-001
   34.4676
20.7357
                     29.36
                     20.00
   27.7690
                    98.27
                   144.77
   11.1481
   20.0000 10000000000.00
<Date: Tue Jun 24 10:08:04 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: NORTH-WEST OF ACHLADES</pre>
<Place: ACHLADES
*****
#GEOSEC: 0099-B / 50.0/ 50.0/ 1.58.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         1.0/ 564081.000/ 3917146.000/
                                                                       0.000 DH=
                                                                                               0.000/rms=146.00
                +0.000e+000 +0.000e+000 +3.293e+001 +5.596e+001 +7.266e+001
+7.879e+001 +7.878e+001 +7.785e+001 +7.675e+001 +7.572e+001 +7.489e+001 +7.409e+001 +7.289e+001 +7.112e+001 +6.935e+001 +6.765e+001 +6.538e+001
+6.255e+001 +6.008e+001 +5.792e+001 +5.525e+001 +5.220e+001 +4.976e+001
+4.777e+001 +4.546e+001 +4.294e+001 +4.095e+001 +3.919e+001 +3.690e+001
+3.394e+001 +3.126e+001 +2.888e+001 +2.602e+001 +2.301e+001 +2.090e+001
+1.942e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +6.850e-001 +1.560e-001 -4.100e-002 -7.500e-002 -6.900e-002 -6.200e-002 -6.700e-002 -7.900e-002 -1.010e-001 -1.300e-001 -1.540e-001 -1.730e-001 -1.940e-001
-2.150e-001 -2.300e-001 -2.410e-001 -2.520e-001 -2.590e-001 -2.610e-001
```

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1D_Inversion_Results_TEM.txt
-2.600e-001 -2.580e-001 -2.600e-001 -2.700e-001 -2.900e-001 -3.270e-001 -3.740e-001 -4.070e-001 -4.260e-001 -4.360e-001 -4.320e-001 -4.130e-001
-3.870e-001
  76.4711
                 23.63
  54.7041
                 34.09
  20.1981
                 67.49
                 91.30
    5.9348
  20.0000 10000000000.00
<Date: Tue Jun 24 10:48:42 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                     6 Ampl=OFF
<Remark: ŠOUTH-EAST OF 0089</pre>
<Place: ACHLADES
*****
#GEOSEC: 0100-C / 50.0/ 50.0/ 1. 76.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                1.0/ 565754.000/ 3918128.000/
                                                         0.000 DH=
                                                                             0.000/rms=325.00
S [V/A]: +0.000e+000 +0.000e+000 +5.877e+000 +1.172e+001 +1.671e+001
+1.991e+001 +2.125e+001 +2.189e+001 +2.252e+001 +2.337e+001 +2.436e+001
+2.545e+001 +2.706e+001 +2.912e+001 +3.069e+001 +3.167e+001 +3.224e+001 +3.211e+001 +3.171e+001 +3.142e+001 +3.129e+001 +3.148e+001 +3.181e+001 +3.210e+001 +3.235e+001 +3.240e+001 +3.222e+001 +3.191e+001 +3.127e+001
+3.011e+001 +2.875e+001 +2.731e+001 +2.523e+001 +2.242e+001 +1.981e+001
+1.744e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.360e-001 +4.890e-001 +2.560e-001 +1.690e-001 +1.580e-001 +2.020e-001 +2.580e-001
+3.020e-001 +3.310e-001 +3.140e-001 +2.490e-001 +1.600e-001 +4.400e-002
-4.940e-001
                 12.16
35.00
  22.0106
  47.7459
  19.4519
                 30.97
                 53.01
  30.0972
    3.3982 10000000000.00
<Date: Tue Jun 24 11:37:43 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                     6 Ampl=OFF
<Remark: NORTH-EAST OF G-81</pre>
*****
#GEOSEC: 0101-C / 50.0 / 50.0 / 1.63.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                1.0/ 565475.000/ 3918184.000/
H= 0.000 DH= 0.000/
                                                                             0.000/rms=127.00
            +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000
+8.220e-001 +3.372e+000 +5.151e+000 +6.786e+000 +8.167e+000 +9.131e+000
+9.907e+000 +1.088e+001 +1.211e+001 +1.326e+001 +1.433e+001 +1.577e+001 +1.761e+001 +1.927e+001 +2.078e+001 +2.275e+001 +2.518e+001 +2.733e+001
+2.923e+001 +3.151e+001 +3.373e+001 +3.473e+001 +3.476e+001 +3.378e+001
+3.167e+001 +2.964e+001 +2.794e+001 +2.605e+001 +2.411e+001 +2.260e+001
+2.127e+001
Err[V/A]: -1.000e-015 -1.000e-015 -1.000e-015 -1.000e-015 -9.000e-001 +9.000e-001 +9.000e-001 +8.980e-001 +8.140e-001 +6.250e-001 +5.260e-001
+4.860e-001 +4.740e-001 +4.770e-001 +4.820e-001 +4.870e-001 +4.890e-001
+4.870e-001 +4.820e-001 +4.750e-001 +4.650e-001 +4.540e-001 +4.410e-001 +4.200e-001 +3.650e-001 +2.400e-001 +8.400e-002 -6.900e-002 -2.220e-001 -3.160e-001 -3.440e-001 -3.460e-001 -3.370e-001 -3.320e-001 -3.460e-001
-3.660e-001
   9.4036
                 10.16
  66.4134
                 58.48
  66.5144
                 22.47
  66.5144
                 20.00
   7.0279 10000000000.00
<Date: Tue Jun 24 12:21:44 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
<Remark: NORTH-EAST OF G-81</pre>
<Place: WEST OF SIRIPIDIANA VILLAGE
*****
```

```
1D_Inversion_Results_TEM.txt
#GEOSEC: 0102-B / 50.0/ 50.0/ 1.0/ 565265.000/ 3918152.000/ 60.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                                   0.000/rms=134.00
                 +0.000e+000 +0.000e+000 +0.000e+000 +8.143e+000 +1.721e+001
     [V/A]:
+2.167e+001 +2.343e+001 +2.440e+001 +2.535e+001 +2.634e+001 +2.719e+001
+2.803e+001 +2.923e+001 +3.088e+001 +3.249e+001 +3.397e+001 +3.585e+001 +3.797e+001 +3.960e+001 +4.082e+001 +4.206e+001 +4.306e+001 +4.354e+001 +4.370e+001 +4.362e+001 +4.318e+001 +4.256e+001 +4.178e+001 +4.051e+001
+3.860e+001 +3.676e+001 +3.508e+001 +3.300e+001 +3.048e+001 +2.812e+001
+2.574e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +5.910e-001 +3.190e-001 +2.290e-001 +1.870e-001 +1.760e-001 +1.890e-001 +2.110e-001 +2.400e-001 +2.720e-001 +2.930e-001 +2.820e-001
+2.550e-001 +2.220e-001 +1.880e-001 +1.420e-001 +8.700e-002 +4.300e-002 +9.000e-003 -2.800e-002 -7.000e-002 -1.070e-001 -1.450e-001 -1.950e-001 -2.480e-001 -2.810e-001 -3.000e-001 -3.230e-001 -3.660e-001 -4.190e-001
-4.580e-001
   24.2300
                      13.10
   56.3988
                      59.06
   56.3988
15.7675
                      21.91
                      74.82
     4.8609 10000000000.00
<Date: Tue Jun 24 12:46:00 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                        6 Ampl=OFF
<Remark: NORTH OF G-81</pre>
#GEOSEC: 0103-C / 50.0 / 50.0 / 1.58.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                              1.0/ 565081.000/ 3918206.000/
                                                                          0.000 DH =
                                                                                                   0.000/\text{rms}=116.00
                +0.000e+000 +0.000e+000 +8.906e+000 +2.565e+001 +3.689e+001
     [V/A]:
+4.255e+001 +4.479e+001 +4.611e+001 +4.736e+001 +4.851e+001 +4.926e+001
+4.987e+001 +5.066e+001 +5.182e+001 +5.311e+001 +5.449e+001 +5.657e+001
+5.942e+001 +6.203e+001 +6.426e+001 +6.674e+001 +6.887e+001 +6.974e+001 +6.967e+001 +6.853e+001 +6.582e+001 +6.278e+001 +5.982e+001 +5.604e+001
+5.172e+001 +4.822e+001 +4.525e+001 +4.154e+001 +3.713e+001 +3.345e+001
+3.040e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.260e-001 +4.050e-001 +2.220e-001 +1.630e-001 +1.260e-001 +9.700e-002 +8.400e-002 +8.300e-002 +9.600e-002 +1.250e-001 +1.580e-001 +1.880e-001 +2.190e-001
+2.410e-001 +2.420e-001 +2.250e-001 +1.830e-001 +1.090e-001 +3.000e-002 -4.500e-002 -1.380e-001 -2.290e-001 -2.820e-001 -3.110e-001 -3.310e-001 -3.470e-001 -3.610e-001 -3.780e-001 -4.040e-001 -4.330e-001 -4.500e-001
-4.600e-001
   44.8356
                      17.06
   70.9228
                      62.92
37.81
  200.0000
                      76.96
   11.1132
     3.5516 10000000000.00
<Date: Tue Jun 24 13:12:52 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                        6 Ampl=OFF
<Remark: NORTH-WEST OF G-81</pre>
0.000/\text{rms}=203.00
+2.791e+001 +3.019e+001 +3.156e+001 +3.288e+001 +3.408e+001 +3.494e+001 +3.571e+001 +3.675e+001 +3.811e+001 +3.935e+001 +4.040e+001 +4.167e+001 +4.307e+001 +4.423e+001 +4.528e+001 +4.671e+001 +4.856e+001 +5.017e+001
+5.146e+001 +5.273e+001 +5.352e+001 +5.358e+001 +5.334e+001 +5.295e+001
+5.272e+001 +5.278e+001 +5.282e+001 +5.237e+001 +5.035e+001 +4.728e+001
+4.403e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.760e-001 +5.330e-001 +3.320e-001 +2.460e-001 +1.900e-001 +1.520e-001 +1.420e-001 +1.490e-001 +1.630e-001 +1.770e-001 +1.800e-001 +1.750e-001 +1.650e-001 +1.560e-001 +1.570e-001 +1.600e-001 +1.800e-001 +1.890e-001 +1.810e-001 +1.570e-001 +1.070e-001 +3.600e-002 -1.300e-002 -3.500e-002 -3.200e-002
```

```
1D_Inversion_Results_TEM.txt
-6.000e-003 +6.000e-003 -1.900e-002 -1.140e-001 -2.680e-001 -3.660e-001
-4.180e-001
  19.3693
                    3.58
  47.5625
                  38.12
  71.5680
                  83.79
   28.0205
                 120.72
    5.6325 10000000000.00
<Date: Tue Jul 01 07:46:40 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: LITTLE STREAM AT EAST</pre>
<Place: SKEPASTI
<
*****
#GEOSEC: 0105-B / 50.0/ 50.0/ 1.52.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                  1.0/ 564704.000/ 3918282.000/
                                                             0.000 \text{ DH} =
                                                                                   0.000/\text{rms}=257.00
S [V/A]: +0.000e+000 +0.000e+000 +1.244e+001 +2.792e+001 +3.792e+001
+4.265e+001 +4.417e+001 +4.475e+001 +4.494e+001 +4.470e+001 +4.429e+001
+4.393e+001 +4.361e+001 +4.357e+001 +4.386e+001 +4.432e+001 +4.513e+001
+4.630e+001 +4.735e+001 +4.824e+001 +4.928e+001 +5.044e+001 +5.148e+001 +5.256e+001 +5.430e+001 +5.715e+001 +6.023e+001 +6.339e+001 +6.755e+001
+7.179e+001 +7.387e+001 +7.429e+001 +7.348e+001 +7.207e+001 +7.167e+001
+7.245e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.680e-001 +3.200e-001 +1.300e-001 +5.500e-002 +1.000e-015 -4.000e-002 -5.300e-002 -4.800e-002 -2.400e-002 +1.900e-002 +5.600e-002 +8.400e-002 +1.110e-001
+1.270e-001 +1.290e-001 +1.240e-001 +1.160e-001 +1.170e-001 +1.320e-001 +1.600e-001 +2.100e-001 +2.770e-001 +3.230e-001 +3.430e-001 +3.200e-001 +2.240e-001 +9.900e-002 -6.000e-003 -7.700e-002 -6.100e-002 +2.500e-002
+1.240e-001
   36.9094
                   3.60
                  55.11
   46.8855
 113.7496
                 100.00
 100.0000
                 100.00
   38.7162 10000000000.00
<Date: Tue Jul 01 08:18:27 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: SOUTH-WEST OF SKEPASTI</pre>
<Place: SKEPASTI
<
*****
#GEOSEC: 0106 / 50.0/ 50.0/ 1.43.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 564556.000/ 3918371.000/
                                                             0.000 DH =
                                                                                   0.000/\text{rms}=205.00
    [V/A]: +0.000e+000 +0.000e+000 +2.809e+000 +1.893e+001 +3.016e+001
+3.544e+001 +3.711e+001 +3.782e+001 +3.838e+001 +3.882e+001 +3.911e+001
+3.942e+001 +3.994e+001 +4.083e+001 +4.185e+001 +4.289e+001 +4.430e+001 +4.608e+001 +4.767e+001 +4.916e+001 +5.125e+001 +5.417e+001 +5.708e+001 +5.991e+001 +6.364e+001 +6.796e+001 +7.102e+001 +7.306e+001 +7.469e+001
+7.561e+001 +7.611e+001 +7.680e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.740e-001 +4.220e-001 +1.760e-001 +1.010e-001 +6.600e-002 +4.700e-002 +4.800e-002 +6.100e-002 +8.700e-002 +1.250e-001 +1.540e-001 +1.710e-001 +1.830e-001 +1.930e-001 +2.330e-001 +2.330e-001 +2.330e-001 +2.330e-001 +2.330e-001 +2.330e-001 +2.330e-001
+3.250e-001 +3.200e-001 +2.810e-001 +2.230e-001 +1.630e-001 +9.400e-002
+4.900e-002 +5.200e-002 +7.300e-002
                  5.36
44.91
   29.7920
   48.0034
 154.0078
                 100.00
 100.0000
                  64.89
   50.9325 10000000000.00
<Date: Tue Jul 01 08:49:42 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: SOME POWER LINES</pre>
*****
#GEOSEC: 0107-B / 50.0 / 50.0 / 1.0 / 564291.000 / 3918311.000 / 29.0 /36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000
                                                                                  0.000/\text{rms}=180.00
S [V/A]: +0.000e+000 +0.000e+000 +6.326e+000 +1.493e+001 +2.211e+001
                                              Σελίδα 35
```

```
1D_Inversion_Results_TEM.txt
+2.756e+001 +3.094e+001 +3.339e+001 +3.610e+001 +3.904e+001 +4.136e+001 +4.325e+001 +4.543e+001 +4.767e+001 +4.929e+001 +5.046e+001 +5.165e+001 +5.271e+001 +5.339e+001 +5.385e+001 +5.430e+001 +5.469e+001 +5.490e+001
+5.497e+001 +5.490e+001 +5.460e+001 +5.422e+001 +5.386e+001 +5.353e+001
+5.344e+001 +5.368e+001 +5.409e+001 +5.472e+001 +5.538e+001 +5.575e+001
+5.595e+001
Err[V/A]:
             +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.670e-001
+6.470e-001 +4.970e-001 +4.240e-001 +3.710e-001 +3.290e-001 +3.010e-001
+2.770e-001 +2.460e-001 +2.070e-001 +1.720e-001 +1.450e-001 +1.150e-001
+8.500e-002 +6.600e-002 +5.400e-002 +4.100e-002 +2.800e-002 +1.500e-002 +2.000e-003 -1.600e-002 -3.500e-002 -4.400e-002 -4.100e-002 -2.300e-002
+1.100e-002 +4.100e-002 +5.800e-002 +6.200e-002 +4.800e-002 +3.200e-002
+1.900e-002
   23.7108
                   6.56
                  50.87
   73.1215
  47.0416
                  22.91
   51.1673
                 100.00
   65.6399 10000000000.00
<Date: Tue Jul 01 09:23:59 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: NE OF ROUMELI</pre>
<Place: ROUMELI
*****
                               50.0/ 50.0/
                                                  1.0/ 564070.000/ 3918336.000/
#GEOSEC: 0108-B
27.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                             0.000 \text{ DH} =
                                                                                  0.000/\text{rms}=641.00
             +0.000e+000 +0.000e+000 +4.684e+000 +1.110e+001 +1.512e+001
+1.687e+001 +1.710e+001 +1.671e+001 +1.575e+001 +1.429e+001 +1.305e+001 +1.207e+001 +1.108e+001 +1.024e+001 +9.795e+000 +9.578e+000 +9.487e+000
+9.621e+000 +9.914e+000 +1.029e+001 +1.094e+001 +1.194e+001 +1.302e+001
+1.412e+001 +1.573e+001 +1.796e+001 +2.001e+001 +2.188e+001 +2.409e+001
+2.604e+001 +2.669e+001 +2.634e+001 +2.484e+001 +2.220e+001 +1.982e+001
+1.794e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -7.650e-001 -2.480e-001 -4.800e-002 -2.120e-001 -3.280e-001 -3.900e-001 -4.040e-001
-3.950e-001 -3.590e-001 -2.820e-001 -1.920e-001 -1.070e-001 +3.000e-003
+1.260e-001 +2.170e-001 +2.870e-001 +3.650e-001 +4.410e-001 +4.930e-001 +5.270e-001 +5.560e-001 +5.700e-001 +5.610e-001 +5.280e-001 +4.380e-001 +2.480e-001 +1.800e-002 -1.920e-001 -3.640e-001 +4.420e-001 +4.590e-001
+4.640e-001
 11.1698
296.3511
133.3356
                  33.23
                  89.55
                   2.26
 100.0000
                   2.26
    1.0000 10000000000.00
<Date: Tue Jul 01 09:46:29 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: ĀLMOST NORTH OF ROUMELI</pre>
<Place: ROUMELI
<****************
*****
                                                 1.0/ 563911.000/ 3918396.000/
#GEOSEC: 0109-B / 50.0/ 50.0/ 1.0
29.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                            0.000 DH =
                                                                                  0.000/\text{rms}=230.00
S [V/A]: +9.175e+000 +5.519e+000 +4.949e+000 +5.208e+000 +5.843e+000 +6.518e+000 +6.868e+000 +7.026e+000 +7.120e+000 +7.210e+000 +7.334e+000 +7.482e+000 +7.729e+000 +8.097e+000 +8.472e+000 +8.848e+000 +9.398e+000
+1.019e+001 +1.101e+001 +1.185e+001 +1.308e+001 +1.478e+001 +1.639e+001
+1.786e+001 +1.969e+001 +2.178e+001 +2.348e+001 +2.501e+001 +2.701e+001
+2.953e+001 +3.169e+001 +3.351e+001 +3.567e+001 +3.827e+001 +4.085e+001
+4.367e+001
Err[V/A]:
             +5.000e-001 +4.980e-001 +7.500e-002 -3.940e-001 +4.790e-001
+3.510e-001 +2.030e-001 +1.100e-001 +6.400e-002 +7.900e-002 +1.150e-001
+1.510e-001 +1.960e-001 +2.390e-001 +2.730e-001 +3.040e-001 +3.480e-001 +4.020e-001 +4.480e-001 +4.840e-001 +5.200e-001 +5.410e-001 +5.390e-001 +5.190e-001 +4.820e-001 +4.380e-001 +4.160e-001 +4.110e-001 +4.120e-001
+4.030e-001 +3.820e-001 +3.570e-001 +3.380e-001 +3.520e-001 +4.050e-001
+4.630e-001
    8.8608
                  17.33
```

```
1D_Inversion_Results_TEM.txt
                  70.88
 100.0000
 100.0000
                  38.70
                  45.42
   42.4785
 100.0000 10000000000.00
<Date: Tue Jul 01 10:06:12 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: ALMOST NORTH OF ROUMELI</pre>
                                                                          6 Ampl=OFF
<Place: ROUMELI <
*****
#GEOSEC: 0110-B
                               50.0/ 50.0/
                                                   1.0/ 563717.000/ 3918357.000/
24.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                   0.000/rms = 92.00
                                                              0.000 DH =
              +0.000e+000 +0.000e+000 +8.172e+000 +1.439e+001 +1.743e+001
+1.797e+001 +1.750e+001 +1.692e+001 +1.624e+001 +1.566e+001 +1.540e+001
+1.539e+001 +1.557e+001 +1.606e+001 +1.667e+001 +1.732e+001 +1.825e+001 +1.952e+001 +2.072e+001 +2.186e+001 +2.339e+001 +2.535e+001 +2.713e+001
+2.875e+001 +3.083e+001 +3.327e+001 +3.517e+001 +3.664e+001 +3.817e+001
+3.946e+001 +4.008e+001 +4.017e+001 +3.954e+001 +3.744e+001 +3.445e+001
+3.116e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +5.060e-001 -1.800e-002 -1.740e-001 -2.050e-001 -1.870e-001 -1.240e-001 -4.600e-002
+2.500e-002 +1.040e-001 +1.820e-001 +2.340e-001 +2.680e-001 +2.990e-001
+3.270e-001 +3.450e-001 +3.570e-001 +3.680e-001 +3.780e-001 +3.810e-001 +3.790e-001 +3.660e-001 +3.350e-001 +2.970e-001 +2.550e-001 +1.970e-001 +1.240e-001 +5.100e-002 -3.100e-002 -1.680e-001 -3.380e-001 -4.370e-001
-4.790e-001
 17.0247
148.2407
58.3943
                  26.66
                  42.38
45.96
   20.1478
                  77.28
    3.0000 10000000000.00
<Date: Tue Jul 01 10:37:08 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: N OF ROUMELI, N OF STREAM
                                                                          6 Ampl=OFF
<Place: ROUMELI</pre>
*****
#GEOSEC: 0111-B / 50.0/ 50.0/ 1 24.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 563464.000/ 3918349.000/
                                                                                   0.000/\text{rms}=489.00
                                                              0.000 DH=
             +0.000e+000 +0.000e+000 +1.974e+001 +3.124e+001 +3.732e+001
+3.886e+001 +3.848e+001 +3.775e+001 +3.674e+001 +3.566e+001 +3.500e+001 +3.469e+001 +3.467e+001 +3.519e+001 +3.606e+001 +3.707e+001 +3.867e+001 +4.097e+001 +4.320e+001 +4.527e+001 +4.779e+001 +5.012e+001 +5.102e+001
+5.082e+001 +4.940e+001 +4.664e+001 +4.394e+001 +4.147e+001 +3.825e+001
+3.423e+001 +3.069e+001 +2.764e+001 +2.409e+001 +2.047e+001 +1.799e+001
+1.626e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.930e-001 +4.950e-001 +4.900e-002 -9.000e-002 -1.290e-001 -1.380e-001 -1.190e-001 -7.900e-002
-3.400e-002 +3.100e-002 +1.080e-001 +1.650e-001 +2.070e-001 +2.500e-001
+2.890e-001 +3.070e-001 +3.040e-001 +2.640e-001 +1.610e-001 +3.400e-002 -8.600e-002 -2.060e-001 -2.900e-001 -3.310e-001 -3.590e-001 -3.960e-001 -4.370e-001 -4.610e-001 -4.730e-001 -4.780e-001 -4.690e-001
-4.570e-001
 36.6273
400.0000
                  45.75
                  22.36
23.75
 147.0182
    7.3672
                  34.72
    3.0000 10000000000.00
<Date: Tue Jul 01 11:41:41 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                          6 Ampl=OFF
<Remark: NEAR SHEAPERT</pre>
<Place: ROUMELI
<***************
*****
#GEOSEC: 0112-B / 50.0/ 50.0/ 1.24.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 563346.000/ 3918411.000/
                                                              0.000 DH =
                                                                                   0.000/rms=618.00
S [V/A]: +0.000e+000 +0.000e+000 +1.551e+001 +3.066e+001 +3.947e+001
+4.247e+001 +4.293e+001 +4.303e+001 +4.331e+001 +4.385e+001 +4.446e+001
                                              Σελίδα 37
```

```
1D_Inversion_Results_TEM.txt
+4.504e+001 +4.579e+001 +4.657e+001 +4.712e+001 +4.751e+001 +4.790e+001 +4.831e+001 +4.867e+001 +4.898e+001 +4.926e+001 +4.917e+001 +4.842e+001 +4.712e+001 +4.464e+001 +4.072e+001 +3.698e+001 +3.360e+001 +2.947e+001
+2.498e+001 +2.163e+001 +1.907e+001 +1.636e+001 +1.376e+001 +1.200e+001
+1.074e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.640e-001 +1.720e-001 +3.500e-002 +2.300e-002 +4.500e-002 +6.900e-002 +8.200e-002
Err[V/A]:
+8.700e-002 +8.500e-002 +7.400e-002 +6.100e-002 +5.100e-002 +4.300e-002 +4.200e-002 +4.300e-002 +3.800e-002 +1.300e-002 -5.400e-002 -1.400e-001 -2.270e-001 -3.250e-001 -4.050e-001 -4.440e-001 -4.630e-001 -4.770e-001 -4.840e-001 -4.870e-001 -4.870e-001 -4.830e-001 -4.790e-001
-4.730e-001
   43.5943
                    41.32
 106.6917
                    15.20
   20.3486
17.0018
                    20.25
                    13.92
    3.0000 10000000000.00
<Date: Tue Jul 01 12:43:34 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                 6 Ampl=OFF
<Remark: IN VILLAGE, FENCES, POWER LINE</pre>
<Place: ROUMELI
*****
                                                         1.0/ 563177.000/ 3918343.000/
H= 0.000 DH= 0.000/
#GEOSEC: 0113-C / 50.0/ 50.0/ 1.
35.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                           0.000/\text{rms}=210.00
              +0.000e+000 +8.057e+000 +4.115e+001 +6.308e+001 +8.119e+001
S [V/A]:
+9.093e+001 +9.336e+001 +9.381e+001 +9.376e+001 +9.351e+001 +9.323e+001
+9.292e+001 +9.252e+001 +9.208e+001 +9.181e+001 +9.169e+001 +9.174e+001 +9.205e+001 +9.252e+001 +9.305e+001 +9.379e+001 +9.464e+001 +9.516e+001
+9.534e+001 +9.506e+001 +9.380e+001 +9.190e+001 +8.961e+001 +8.603e+001
+8.098e+001 +7.620e+001 +7.180e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 +7.060e-001 +2.900e-001 +8.000e-002 +1.500e-002 -7.000e-003 -1.500e-002 -2.000e-002 -2.300e-002 -2.300e-002 -2.300e-002 -3.000e-003 +9.000e-003
+2.400e-002 +3.500e-002 +4.200e-002 +4.400e-002 +3.800e-002 +2.200e-002 +1.000e-015 -3.900e-002 -9.500e-002 -1.470e-001 -1.920e-001 -2.440e-001
-2.980e-001 -3.360e-001 -3.660e-001
   90.6804
                    77.46
                    14.24
   90.6804
                    52.00
73.85
   94.9964
   33.9089
   11.0087 10000000000.00
<Date: Tue Jul 01 13:19:21 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: IN VILLAGE, FENCES</pre>
<place: ROUMELI</pre>
*****
#GEOSEC: 0114-B / 50.0/ 50.0/ 1.
34.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         1.0/ 562762.000/ 3918416.000/
                                                                    0.000 DH=
                                                                                           0.000/rms=227.00
    [V/A]: +0.000e+000 +0.000e+000 +2.179e+000 +1.869e+001 +3.007e+001
+3.528e+001 +3.681e+001 +3.734e+001 +3.754e+001 +3.737e+001 +3.706e+001
+3.676e+001 +3.644e+001 +3.616e+001 +3.606e+001 +3.605e+001 +3.616e+001
+3.639e+001 +3.665e+001 +3.691e+001 +3.725e+001 +3.761e+001 +3.784e+001 +3.795e+001 +3.795e+001 +3.770e+001 +3.728e+001 +3.676e+001 +3.591e+001
+3.463e+001 +3.329e+001 +3.189e+001 +2.980e+001 +2.679e+001 +2.385e+001
+2.113e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.760e-001 +4.110e-001 +1.510e-001 +6.200e-002 +5.000e-003 -3.400e-002 -5.000e-002 -5.100e-002 -4.300e-002 -2.600e-002 -8.000e-003 +7.000e-003 +2.300e-002
+3.700e-002 +4.600e-002 +5.000e-002 +4.900e-002 +4.100e-002 +2.800e-002 +1.100e-002 -1.500e-002 -5.100e-002 -8.300e-002 -1.120e-001 -1.500e-001
-2.000e-001 -2.500e-001 -3.020e-001 -3.720e-001 -4.410e-001 -4.760e-001
-4.910e-001
   36.1588
                    56.49
   36.1588
                    17.39
                    25.57
   34.8664
   12.8928
                    54.16
```

```
1D_Inversion_Results_TEM.txt
```

```
3.0185 10000000000.00
<Date: Tue Jul 01 13:53:43 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                   6 Ampl=OFF
<Remark: 800M SOUTH OF PANORMOS</pre>
<Place: PANORMOS
******
#GEOSEC: 0115-B / 50.0/ 50.0/ 1.0
39.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 562939.000/ 3918324.000/
                                                                   0.000 DH =
                                                                                             0.000/\text{rms}=325.00
S [V/A]: +0.000e+000 +0.000e+000 +2.351e+001 +4.363e+001 +6.094e+001 +7.327e+001 +7.892e+001 +8.149e+001 +8.243e+001 +8.138e+001 +7.952e+001 +7.770e+001 +7.555e+001 +7.347e+001 +7.203e+001 +7.093e+001 +6.963e+001
+6.815e+001 +6.694e+001 +6.596e+001 +6.485e+001 +6.374e+001 +6.294e+001
+6.234e+001 +6.165e+001 +6.078e+001 +5.986e+001 +5.879e+001 +5.699e+001
+5.424e+001 +5.154e+001 +4.909e+001 +4.605e+001 +4.245e+001 +3.918e+001
+3.594e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.290e-001
+5.220e-001 +2.830e-001 +1.370e-001 +4.000e-003 -9.700e-002 -1.400e-001
-1.500e-001 -1.410e-001 -1.210e-001 -1.080e-001 -1.030e-001 -1.020e-001 -1.030e-001 -1.020e-001 -9.800e-002 -7.800e-002 -6.900e-002 -6.400e-002 -6.500e-002 -8.000e-002 -1.080e-001 -1.450e-001 -1.980e-001 -2.550e-001 -2.910e-001 -3.100e-001 -3.310e-001 -3.680e-001 -4.150e-001
-4.520e-001
   76.3298
24.5230
                    51.12
                    11.45
   85.4210
                    36.83
   29.9564
                    88.79
    8.0299 10000000000.00
<Date: Tue Jul 01 14:29:27 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                   6 Ampl=OFF
<Remark: 900M SOUTH-EAST OF PANORMOS</pre>
*****
#GEOSEC: 0116-D / 50.0 / 50.0 / 1.0 31.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 562523.000/ 3918515.000/
                                                                                             0.000/\text{rms}=297.00
                                                                    0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +9.181e+000 +2.531e+001 +3.646e+001 +4.240e+001 +4.479e+001 +4.601e+001 +4.685e+001 +4.725e+001 +4.725e+001
    [V/A]:
+4.715e+001 +4.702e+001 +4.693e+001 +4.689e+001 +4.687e+001 +4.678e+001
+4.655e+001 +4.622e+001 +4.586e+001 +4.531e+001 +4.454e+001 +4.382e+001 +4.313e+001 +4.220e+001 +4.094e+001 +3.971e+001 +3.845e+001 +3.658e+001 +3.393e+001 +3.136e+001 +2.896e+001 +2.591e+001 +2.240e+001 +1.964e+001 +1.745e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.310e-001
+4.260e-001 +2.220e-001 +1.360e-001 +6.900e-002 +1.800e-002 -7.000e-003 -1.500e-002 -1.200e-002 -7.000e-003 -4.000e-003 -7.000e-003 -1.700e-002 -3.300e-002 -4.800e-002 -6.000e-002 -7.500e-002 -9.000e-002 -1.020e-001 -1.140e-001 -1.320e-001 -1.620e-001 -1.960e-001 -2.350e-001 -2.910e-001
-3.570e-001 -4.030e-001 -4.320e-001 -4.570e-001 -4.730e-001 -4.800e-001
-4.850e-001
   45.3471
                    44.08
   45.3471
                     2.49
   43.8136
                    19.89
   18.0684
                    60.75
     3.0000 10000000000.00
<Date: Wed Jul 02 09:20:36 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                   6 Ampl=OFF
<Remark: 700M SOUTH OF PANORMOS</pre>
<Place: PANORMOS
*****
                                   50.0/ 50.0/ 1.0/ 562060.000/ 3918469.000/
7 30.0/ 30.0/ 1.0/ 362060.000/ 3918469.000/ 23.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +8.093e+000 +8.885e+000 +1.162e+001 +1.458e+001 +1.823e+001 +2.176e+001 +2.399e+001 +2.525e+001 +2.610e+001 +2.634e+001 +2.618e+001 +2.597e+001 +2.577e+001 +2.573e+001 +2.590e+001 +2.619e+001 +2.668e+001 +2.737e+001 +2.738e+001 +2.848e+001 +2.907e+001 +2.970e+001 +3.024e+001
                                                                                             0.000/rms=308.00
+3.072e+001 +3.130e+001 +3.182e+001 +3.200e+001 +3.187e+001 +3.134e+001
```

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1D_Inversion_Results_TEM.txt
+3.024e+001 +2.899e+001 +2.770e+001 +2.585e+001 +2.325e+001 +2.072e+001
+1.836e+001
Err[V/A]:
              +1.680e-001 -7.010e-001 -8.410e-001 -8.210e-001 +7.310e-001
+5.600e-001 +3.930e-001 +2.520e-001 +1.120e-001 +1.000e-003 -4.500e-002
-4.900e-002 -2.500e-002 +1.700e-002 +5.800e-002 +8.700e-002 +1.120e-001 +1.260e-001 +1.250e-001 +1.180e-001 +1.100e-001 +1.060e-001 +1.060e-001 +1.060e-001 +5.400e-002 +1.000e-003 -5.700e-002 -1.300e-001 -2.070e-001 -2.630e-001 -3.110e-001 -3.740e-001 -4.390e-001 -4.750e-001
-4.910e-001
   26.0444
                  32.80
   26.0444
                   8.72
 100.0498
                  23.04
   18.5268
                  70.46
    3.0569 10000000000.00
<Date: Wed Jul 02 10:11:17 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                           6 Ampl=OFF
<Remark: 900M SW OF PANORMOS, POWERLINE</pre>
<Place: PANORMOS
#GEOSEC: 0118-D
#GEOSEC: 0118-D / 50.0/ 50.0/ 1 25.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 562328.000/ 3918486.000/
                                                               0.000 DH =
                                                                                    0.000/rms=147.00
             +0.000e+000 +1.730e+001 +4.020e+001 +5.176e+001 +5.800e+001
+5.876e+001 +5.724e+001 +5.556e+001 +5.357e+001 +5.152e+001 +5.014e+001 +4.917e+001 +4.820e+001 +4.740e+001 +4.692e+001 +4.665e+001 +4.648e+001
+4.652e+001 +4.670e+001 +4.695e+001 +4.724e+001 +4.736e+001 +4.708e+001
+4.647e+001 +4.526e+001 +4.338e+001 +4.166e+001 +4.016e+001 +3.839e+001
+3.642e+001 +3.481e+001 +3.338e+001 +3.151e+001 +2.916e+001 +2.711e+001
+2.537e+001
Err[V/A]:
              -9.000e-001 -9.000e-001 -9.000e-001 -7.720e-001 +3.090e-001
-5.200e-002 -1.620e-001 -1.840e-001 -1.800e-001 -1.610e-001 -1.380e-001
-1.180e-001 -9.500e-002 -6.800e-002 -4.800e-002 -3.000e-002 -9.000e-003 +1.400e-002 +3.000e-002 +3.600e-002 +2.400e-002 -1.400e-002 -6.500e-002 -1.150e-001 -1.700e-001 -2.140e-001 -2.330e-001 -2.390e-001 -2.410e-001
-2.460e-001 -2.590e-001 -2.800e-001 -3.120e-001 -3.480e-001 -3.710e-001
-3.850e-001
   54.7726
                  28.95
    4.0592
                   1.00
                  19.37
  69.6357
  41.3310
   14.6683 10000000000.00
<Date: Wed Jul 02 10:45:25 2008
<Time Range=6 Currrent= 1.00 Stack= 5 Filter=50 Deff=</pre>
                                                                           5 Ampl=OFF
<Remark: 800M SW OF PANORMOS, POWERLINE</pre>
#GEOSEC: 0119-B
                               50.0/ 50.0/
                                                    1.0/ 561697.000/ 3918376.000/
18.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                    0.000/\text{rms}=245.00
S [V/A]: +6.070e+001 +5.483e+001 +5.221e+001 +5.062e+001 +4.903e+001 +4.754e+001 +4.653e+001 +4.586e+001 +4.524e+001 +4.487e+001 +4.478e+001
+4.483e+001 +4.505e+001 +4.547e+001 +4.601e+001 +4.662e+001 +4.757e+001
+4.897e+001 +5.034e+001 +5.159e+001 +5.308e+001 +5.442e+001 +5.497e+001
+5.492e+001 +5.418e+001 +5.248e+001 +5.045e+001 +4.821e+001 +4.483e+001 +4.020e+001 +3.614e+001 +3.282e+001 +2.922e+001 +2.592e+001 +2.391e+001
+2.268e+001
              +3.780e-001 +2.730e-001 +1.940e-001 +1.630e-001 -1.420e-001
Err[V/A]:
-1.210e-001 -1.010e-001 -8.200e-002 -5.600e-002 -2.300e-002 -1.000e-003 +1.600e-002 +3.500e-002 +5.700e-002 +7.900e-002 +9.900e-002 +1.250e-001 +1.510e-001 +1.640e-001 +1.630e-001 +1.410e-001 +8.700e-002 +2.400e-002 -3.700e-002 -1.110e-001 -1.920e-001 -2.580e-001 -3.170e-001 -3.820e-001
-4.320e-001 -4.520e-001 -4.550e-001 -4.450e-001 -4.100e-001 -3.540e-001
-2.850e-001
                  57.27
   45.9898
 192.9748
                  31.13
  14.6816
                  45.85
  14.6816
                    1.00
    3.6250 10000000000.00
```

```
1D_Inversion_Results_TEM.txt
<Date: Wed Jul 02 11:34:25 2008</pre>
<Time Range=6 Currrent= 1.00 Stack= 5 Filter=50 Deff=
<Remark: 700M EAST OF SPRINGS,POWERLINE</pre>
                                                                                             5 Ampl=OFF
<Place: PANORMOS
*****
#GEOSEC: 0120-C / 50.0/ 50.0/ 1.
33.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               1.0/ 561834.000/ 3918378.000/
                                                                             0.000 DH=
                                                                                                        0.000/\text{rms}=215.00
S [V/A]: +0.000e+000 +0.000e+000 +1.075e+001 +2.468e+001 +3.864e+001
+5.071e+001 +5.685e+001 +5.933e+001 +5.988e+001 +5.883e+001 +5.756e+001 +5.637e+001 +5.473e+001 +5.260e+001 +5.070e+001 +4.918e+001 +4.757e+001
+4.622e+001 +4.549e+001 +4.507e+001 +4.463e+001 +4.396e+001 +4.303e+001
+4.191e+001 +4.015e+001 +3.775e+001 +3.569e+001 +3.388e+001 +3.158e+001
+2.858e+001 +2.567e+001 +2.290e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.880e-001 +6.980e-001 +4.030e-001 +1.690e-001 -1.300e-002 -1.030e-001 -1.290e-001
-1.460e-001 -1.690e-001 -1.940e-001 -2.010e-001 -1.900e-001 -1.590e-001 -1.130e-001 -7.700e-002 -5.900e-002 -6.300e-002 -1.010e-001 -1.520e-001 -2.010e-001 -2.500e-001 -2.890e-001 -3.100e-001 -3.290e-001 -3.670e-001 -4.260e-001 -4.670e-001 -4.870e-001
    59.8354
                       34.60
    17.3363
                       11.74
    84.2302
                       20.26
    22.2186
                       42.01
     6.6274 100000000000.00
<Date: Wed Jul 02 12:10:48 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                             5 Ampl=OFF
<Remark: 700M EAST OF SPRINGS,POWERLINE</pre>
<Place: PANORMOS
<***************************
******
#GEOSEC: 0121 / 50.0/ 50.0/ 1.0/ 561502.000/ 3918532.000/ 14.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +1.083e+001 +2.944e+001 +3.719e+001 +3.978e+001
                                                                 1.0/ 561502.000/ 3918532.000/
                                                                                                        0.000/\text{rms} = 95.00
+3.841e+001 +3.635e+001 +3.460e+001 +3.269e+001 +3.080e+001 +2.948e+001
+2.856e+001 +2.769e+001 +2.702e+001 +2.670e+001 +2.660e+001 +2.665e+001
+2.694e+001 +2.737e+001 +2.786e+001 +2.864e+001 +2.976e+001 +3.084e+001 +3.181e+001 +3.296e+001 +3.394e+001 +3.413e+001 +3.364e+001 +3.211e+001
+2.919e+001 +2.618e+001 +2.343e+001
Err[V/A]: -9.000e-001 -9.000e-001 -7.040e-001 +1.010e-001 -2.180e-001 -2.780e-001 -2.800e-001 -2.660e-001 -2.420e-001 -2.150e-001 -1.850e-001 -1.420e-001 -9.000e-002 -4.500e-002 -1.000e-002 +3.000e-002 +7.500e-002 +1.080e-001 +1.360e-001 +1.680e-001 +1.970e-001 +2.100e-001 +2.050e-001 +1.710e-001 +8.200e-002 -3.800e-002 -1.680e-001 -3.160e-001 -4.660e-001 -4.660e-001 -4.820e-002
 -4.240e-001 -4.660e-001 -4.830e-001
   35.0303
15.7869
                       15.58
                       10.13
    36.6517
                       82.24
    36.6517
                         1.98
     3.0000 10000000000.00
<Date: Wed Jul 02 12:40:35 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                             5 Ampl=OFF
<Remark: 500M E OF SPRINGS, NEXT RIVER</pre>
<Place: PANORMOS
<pre>

<
 *****
                                       50.0/ 50.0/
#GEOSEC: 0122-A
                                                                 1.0/ 561411.000/ 3918613.000/
13.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                              0.000 DH =
                                                                                                        0.000/\text{rms} = 46.00
S [V/A]: +0.000e+000 +0.000e+000 +1.386e+001 +2.442e+001 +2.959e+001 +3.040e+001 +2.977e+001 +2.906e+001 +2.823e+001 +2.745e+001 +2.691e+001
+2.657e+001 +2.629e+001 +2.618e+001 +2.627e+001 +2.648e+001 +2.689e+001
+2.756e+001 +2.824e+001 +2.889e+001 +2.974e+001 +3.075e+001 +3.159e+001
+3.231e+001 +3.316e+001 +3.409e+001 +3.474e+001 +3.515e+001 +3.537e+001 +3.513e+001 +3.513e+001 +3.513e+001 +3.513e+001 +3.513e+001 +3.446e+001 +3.354e+001 

Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +5.010e-001 -9.000e-003 -1.310e-001 -1.490e-001 -1.390e-001 -1.180e-001 -9.700e-002 -7.300e-002 -3.900e-002 +2.000e-003 +3.800e-002 +6.800e-002 +1.010e-001
+1.310e-001 +1.490e-001 +1.580e-001 +1.610e-001 +1.600e-001 +1.550e-001
                                                          Σελίδα 41
```

```
1D_Inversion_Results_TEM.txt
+1.500e-001 +1.410e-001 +1.220e-001 +9.500e-002 +6.100e-002 +3.000e-003
-7.700e-002 -1.490e-001 -2.100e-001
                19.19
  28,6990
  17.5377
                 8.57
  48.6706
                58.86
  30.0963
                68.31
  10.7890 10000000000.00
<Date: Wed Jul 02 13:30:25 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                  5 Ampl=OFF
<Remark: 400M E OF SPRINGS, NEXT RIVER</pre>
<Place: GLYKIA VRISI
<
*****
0.000/\text{rms}=139.00
+3.470e+001 +3.265e+001 +3.076e+001 +2.871e+001 +2.692e+001 +2.592e+001
+2.539e+001 +2.513e+001 +2.527e+001 +2.568e+001 +2.618e+001 +2.694e+001
+2.792e+001 +2.880e+001 +2.958e+001 +3.056e+001 +3.169e+001 +3.254e+001 +3.313e+001 +3.360e+001 +3.375e+001 +3.362e+001 +3.343e+001 +3.320e+001
+3.306e+001 +3.299e+001 +3.282e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -6.870e-001 +1.370e-001 -2.220e-001 -3.140e-001 -3.250e-001 -2.990e-001 -2.360e-001 -1.670e-001 -9.900e-002 -1.800e-002 +6.200e-002 +1.130e-001 +1.430e-001 +1.640e-001 +1.760e-001 +1.800e-001 +1.810e-001 +1.780e-001 +1.640e-001 +1.390e-001
+1.040e-001 +5.200e-002 -3.000e-003 -3.200e-002 -3.900e-002 -3.000e-002
-1.700e-002 -2.500e-002 -4.500e-002
                14.54
10.27
  31.9611
  15.1391
  67.5119
                46.21
  26.7088
                72.95
  34.3146 10000000000.00
<Date: Wed Jul 02 14:30:55 2008
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=</pre>
                                                                  5 Ampl=OFF
<Remark: 170M E OF SPRINGS, NEXT RIVER</pre>
<Place: GLYKIA VRISI
<****************************
                                              1.0/ 561019.000/ 3918234.000/
#GEOSEC: 0124-B
                           50.0/ 50.0/
30.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                       0.000 DH =
                                                                          0.000/\text{rms}=248.00
            +0.000e+000 +8.850e+000 +3.869e+001 +5.662e+001 +6.941e+001
+7.500e+001 +7.571e+001 +7.494e+001 +7.283e+001 +6.874e+001 +6.413e+001 +5.971e+001 +5.432e+001 +4.887e+001 +4.523e+001 +4.289e+001 +4.090e+001
+3.966e+001 +3.930e+001 +3.934e+001 +3.966e+001 +4.022e+001 +4.079e+001
+4.138e+001 +4.235e+001 +4.396e+001 +4.576e+001 +4.761e+001 +4.996e+001
+5.169e+001 +5.086e+001 +4.774e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 +5.940e-001 +1.760e-001 -1.200e-002 -1.030e-001 -1.970e-001 -3.010e-001 -3.650e-001
-3.940e-001 -4.030e-001 -3.840e-001 -3.430e-001 -2.880e-001 -2.020e-001
-9.500e-002 -2.100e-002 +2.400e-002 +5.600e-002 +7.600e-002 +9.100e-002 +1.130e-001 +1.520e-001 +2.100e-001 +2.530e-001 +2.670e-001 +2.200e-001 +2.300e-002 -2.600e-001 -4.360e-001
  66.4620
                31.33
  14.7935
74.7526
20.2809
                15.14
                93.63
47.39
   3,0000 10000000000.00
<Date: Thu Jul 03 08:00:09 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff= <Remark: 80M S OF SALTY SPRING
                                                                  5 Ampl=OFF
*****
                            50.0/ 50.0/
#GEOSEC: 0125-D
                                                     561137.000/ 3918351.000/
                                              1.0/
28.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                       0.000 DH =
                                                                          0.000/rms=150.00
            +0.000e+000 +1.929e+001 +5.420e+001 +7.722e+001 +9.356e+001
+9.586e+001 +9.030e+001 +8.405e+001 +7.644e+001 +6.836e+001 +6.227e+001
+5.752e+001 +5.228e+001 +4.706e+001 +4.338e+001 +4.077e+001 +3.818e+001
                                         Σελίδα 42
```

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1D_Inversion_Results_TEM.txt
+3.602e+001 +3.485e+001 +3.426e+001 +3.402e+001 +3.433e+001 +3.497e+001 +3.572e+001 +3.679e+001 +3.818e+001 +3.944e+001 +4.068e+001 +4.251e+001
+4.519e+001 +4.786e+001 +5.037e+001
                -9.000e-001 -9.000e-001 -9.000e-001 -8.740e-001 +4.970e-001
Err[V/A]:
-1.260e-001 -3.390e-001 -3.860e-001 -4.010e-001 -4.070e-001 -4.090e-001 -4.080e-001 -4.030e-001 -3.900e-001 -3.690e-001 -3.420e-001 -2.940e-001 -2.210e-001 -1.480e-001 -8.100e-002 +1.000e-015 +7.900e-002 +1.280e-001 +1.540e-001 +1.710e-001 +1.850e-001 +2.020e-001 +2.260e-001 +2.660e-001
+3.110e-001 +3.350e-001 +3.470e-001
   78.7026
13.5677
                     26.90
                      13.87
   39.5674
                      21.66
   39.5674
                       4.67
 100.0000 10000000000.00
<Date: Thu Jul 03 08:35:20 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
<Remark: 120M EAST OF SALTY SPRING</pre>
<Place: GLYKIA VRISI
#GEOSEC: 0126 / 50.0/ 50.0/ 1 14.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                             1.0/ 560780.000/ 3918513.000/
                                                                          0.000 DH =
                                                                                                  0.000/\text{rms}=263.00
                +0.000e+000 +0.000e+000 +0.000e+000 +8.896e+000 +1.743e+001
+2.145e+001 +2.317e+001 +2.441e+001 +2.601e+001 +2.808e+001 +2.996e+001 +3.164e+001 +3.362e+001 +3.561e+001 +3.685e+001 +3.751e+001 +3.783e+001
+3.762e+001 +3.708e+001 +3.641e+001 +3.538e+001 +3.385e+001 +3.232e+001
+3.086e+001 +2.901e+001 +2.705e+001 +2.580e+001 +2.509e+001 +2.478e+001
+3.080e+001 +2.901e+001 +2.703e+001 +2.380e+001 +2.309e+001 +2.478e+001 +2.524e+001 +2.632e+001 +2.776e+001  
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.990e-001  
+5.600e-001 +3.520e-001 +3.220e-001 +3.320e-001 +3.460e-001 +3.480e-001  
+3.350e-001 +2.970e-001 +2.280e-001 +1.550e-001 +8.800e-002 +1.200e-002  
-5.900e-002 -1.050e-001 -1.380e-001 -1.800e-001 -2.320e-001 -2.730e-001  
-2.990e-001 -3.080e-001 -2.810e-001 -2.210e-001 -1.350e-001 +4.000e-003  
+1.760e-001 +3.050e-001 +4.020e-001
   26.2916
                       6.51
                       5.08
   18.3841
                      29.43
   86.4627
   17.5396
                      78.43
 100.0000 10000000000.00
<Date: Thu Jul 03 09:17:39 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
<Remark: 240M NORTH OF SWEET SPRING</pre>
*****
#GEOSEC: 0127-B / 50.0/ 50.0/ 1. 40.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                             1.0/ 561448.000/ 3917729.000/
                                                                                                  0.000/rms=127.00
                                                                         0.000 DH =
                +0.000e+000 +0.000e+000 +3.853e+000 +1.800e+001 +3.107e+001
+4.245e+001 +5.043e+001 +5.654e+001 +6.300e+001 +6.862e+001 +7.148e+001 +7.273e+001 +7.321e+001 +7.291e+001 +7.238e+001 +7.186e+001 +7.123e+001 +7.056e+001 +7.010e+001 +6.978e+001 +6.944e+001 +6.906e+001 +6.865e+001
+6.811e+001 +6.712e+001 +6.531e+001 +6.324e+001 +6.105e+001 +5.792e+001
+5.395e+001 +5.056e+001 +4.772e+001 +4.440e+001 +4.084e+001 +3.807e+001
+3.575e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.970e-001 +7.960e-001 +6.720e-001 +5.770e-001 +4.540e-001 +2.960e-001 +1.660e-001
+7.900e-002 +1.000e-002 -3.200e-002 -4.600e-002 -4.900e-002 -4.700e-002
-4.200e-002 -3.500e-002 -3.000e-002 -2.700e-002 -3.100e-002 -4.500e-002 -6.700e-002 -1.050e-001 -1.610e-001 -2.100e-001 -2.500e-001 -2.910e-001 -3.230e-001 -3.390e-001 -3.460e-001 -3.490e-001 -3.520e-001 -3.590e-001
-3.690e-001
   13.5155
                       2.98
  400.0000
                      25.46
   52.4352
                      64.07
   55.4863
                      52.37
   13.9312 10000000000.00
<Date: Thu Jul 03 10:36:34 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
                                                      Σελίδα 43
```

```
#GEOSEC: 0128-B / 50.0/ 50.0/ 1.
21.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 561620.000/ 3917868.000/
                                                                                       0.000/\text{rms} = 68.00
S [V/A]: +0.000e+000 +0.000e+000 +7.200e+000 +1.675e+001 +2.108e+001
+2.167e+001 +2.132e+001 +2.098e+001 +2.076e+001 +2.076e+001 +2.097e+001 +2.128e+001 +2.185e+001 +2.273e+001 +2.365e+001 +2.455e+001 +2.575e+001
+2.724e+001 +2.853e+001 +2.964e+001 +3.099e+001 +3.252e+001 +3.378e+001 +3.485e+001 +3.612e+001 +3.749e+001 +3.840e+001 +3.897e+001 +3.929e+001
+3.910e+001 +3.852e+001 +3.776e+001 +3.660e+001 +3.505e+001 +3.369e+001
+3.249e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +5.720e-001 +5.000e-003 -9.400e-002 -7.900e-002 -2.900e-002 +3.000e-002 +7.900e-002 +1.180e-001 +1.640e-001 +2.080e-001 +2.370e-001 +2.530e-001 +2.630e-001
+2.650e-001 +2.600e-001 +2.510e-001 +2.390e-001 +2.250e-001 +2.150e-001 +2.060e-001 +1.900e-001 +1.590e-001 +1.200e-001 +7.600e-002 +1.400e-002
-5.900e-002 -1.140e-001 -1.520e-001 -1.860e-001 -2.140e-001 -2.300e-001 -2.420e-001
  22.6686
                   15.11
    8.6129
                    1.93
   57.2893
                   36.75
   48.8298
                   88.48
  16.7377 10000000000.00
<Date: Thu Jul 03 11:16:53 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: 500M NORTH OF G-52
<Place: PANORMOS
*****
#GEOSEC: 0129-B / 50.0/ 50.0/ 1.0/ 561780.000/ 3917814.000/ 19.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +2.574e+001 +4.682e+001 +5.439e+001 +5.450e+001
                                                                                       0.000/\text{rms}=249.00
+4.977e+001 +4.570e+001 +4.299e+001 +4.067e+001 +3.920e+001 +3.879e+001
+3.897e+001 +3.974e+001 +4.134e+001 +4.317e+001 +4.499e+001 +4.748e+001
+5.056e+001 +5.319e+001 +5.549e+001 +5.835e+001 +6.172e+001 +6.461e+001 +6.715e+001 +7.040e+001 +7.435e+001 +7.759e+001 +8.019e+001 +8.266e+001
+8.375e+001 +8.284e+001 +8.090e+001 +7.772e+001 +7.409e+001 +7.193e+001
+7.110e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.900e-001 -4.400e-001 -1.740e-001 -3.590e-001 -3.550e-001 -3.070e-001 -2.220e-001 -1.080e-001 -1.100e-002
+6.500e-002 +1.450e-001 +2.180e-001 +2.610e-001 +2.820e-001 +2.930e-001
+2.920e-001 +2.860e-001 +2.790e-001 +2.720e-001 +2.650e-001 +2.620e-001 +2.610e-001 +2.600e-001 +2.540e-001 +2.360e-001 +2.000e-001 +1.210e-001 -6.000e-003 -1.170e-001 -1.860e-001 -2.190e-001 -1.940e-001 -1.220e-001
-3.800e-002
   54.8178
                   17.42
                    2.42
    6.9880
                  100.00
 127.1128
 100.0000
                  100.00
   32.8957 10000000000.00
<Date: Thu Jul 03 12:12:55 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                             6 Ampl=OFF
*****
#GEOSEC: 0130-B / 50.0/ 50.0/ 1.
21.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 562017.000/ 3917796.000/
                                                               0.000 DH =
                                                                                       0.000/\text{rms}=129.00
S [V/A]: +0.000e+000 +0.000e+000 +9.540e+000 +1.536e+001 +1.874e+001
+1.976e+001 +1.957e+001 +1.917e+001 +1.872e+001 +1.842e+001 +1.847e+001
```

#GEOSEC: 0130-B / 50.0/ 50.0/ 1.0/ 562017.000/ 3917796.000/ 21.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rms=129. S [V/A]: +0.000e+000 +0.000e+000 +9.540e+000 +1.536e+001 +1.874e+001 +1.976e+001 +1.957e+001 +1.917e+001 +1.872e+001 +1.842e+001 +1.847e+001 +1.872e+001 +1.929e+001 +2.028e+001 +2.134e+001 +2.237e+001 +2.376e+001 +2.545e+001 +2.688e+001 +2.806e+001 +2.943e+001 +3.083e+001 +3.180e+001 +3.244e+001 +3.297e+001 +3.318e+001 +3.299e+001 +3.256e+001 +3.171e+001 +3.033e+001 +2.898e+001 +2.777e+001 +2.634e+001 +2.488e+001 +2.392e+001 +2.333e+001 Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.950e-001 +5.530e-001

```
1D_Inversion_Results_TEM.txt
+7.400e-002 -9.400e-002 -1.260e-001 -1.000e-001 -2.500e-002 +5.400e-002 +1.220e-001 +1.970e-001 +2.630e-001 +2.990e-001 +3.170e-001 +3.230e-001 +3.150e-001 +2.970e-001 +2.760e-001 +2.440e-001 +1.990e-001 +1.570e-001 +1.170e-001 +6.300e-002 -5.000e-003 -6.400e-002 -1.160e-001 -1.760e-001
-2.310e-001 -2.620e-001 -2.730e-001 -2.680e-001 -2.380e-001 -1.930e-001
-1.440e-001
    20.0081
                         17.46
    19.8427
                           1.00
    19.8427
                           3.34
    60.0995
                         67.07
    13.4400 10000000000.00
<Date: Thu Jul 03 12:47:23 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                      6 Ampl=OFF
<Remark: ON BARSUKOV'S 25M-LOOP PROFILE</pre>
<Place: PANORMOS
*****
                                       / 50.0/ 50.0/ 1.0/ 562212.000/ 3917821.000/
#GEOSEC: 0131-B
18.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +1.790e+001 +3.129e+001 +3.610e+001 +3.742e+001 +3.675e+001 +3.592e+001 +3.538e+001 +3.494e+001 +3.472e+001 +3.471e+001 +3.485e+001 +3.513e+001 +3.556e+001 +3.595e+001 +3.623e+001 +3.645e+001
                                                                                                                   0.000/rms=215.00
+3.645e+001 +3.622e+001 +3.583e+001 +3.512e+001 +3.400e+001 +3.285e+001 +3.177e+001 +3.036e+001 +2.872e+001 +2.746e+001 +2.647e+001 +2.539e+001 +2.437e+001 +2.369e+001 +2.321e+001 +2.267e+001 +2.198e+001 +2.117e+001
+2.018e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.850e-001 -4.830e-001 +5.500e-002 -1.010e-001 -1.070e-001 -8.200e-002 -4.900e-002 -1.300e-002 +1.400e-002 +3.400e-002 +5.000e-002 +6.100e-002 +5.600e-002 +4.400e-002 +1.800e-002 -2.000e-002 -5.700e-002 -9.000e-002 -1.310e-001 -1.760e-001 -2.080e-001 -2.290e-001 -2.450e-001 -2.500e-001 -2.440e-001 -2.310e-001 -2.080e-001 -1.760e-001 -1.510e-001 -1.360e-001 -1.390e-001 -1.830e-001 -2.610e-001
-3.340e-001
    34.6607
                         18.70
    29.9671
                           1.10
    29.9671
                           2.22
    36.8010
                         36.29
    14.9362 10000000000.00
<Date: Thu Jul 03 13:14:49 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: EASTERN OF BARSUKOV'S PROFILE
                                                                                                      6 Ampl=OFF
<Place: PANORMOS
<
******
#GEOSEC: 0132-A / 50.0/ 50.0/ 1.0/ 562520.000/ 3917914.000/ 20.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +6.001e+001 +3.637e+001 +2.497e+001 +1.869e+001 +1.380e+001 +1.048e+001 +8.863e+000 +8.006e+000 +7.362e+000 +6.969e+000 +6.810e+000
                                                                                                                   0.000/\text{rms}=258.00
+6.755e+000 +6.746e+000 +6.795e+000 +6.869e+000 +6.947e+000 +7.059e+000 +7.194e+000 +7.303e+000 +7.397e+000 +7.515e+000 +7.688e+000 +7.900e+000 +8.158e+000 +8.611e+000 +9.368e+000 +1.018e+001 +1.098e+001 +1.199e+001
+1.295e+001 +1.339e+001 +1.349e+001
Err[V/A]: +5.000e-001 +5.000e-001 +5.000e-001 +5.000e-001 -5.000e-001
-4.960e-001 -4.740e-001 -4.200e-001 -3.140e-001 -1.790e-001 -8.800e-002 -3.300e-002 +1.200e-002 +5.000e-002 +7.000e-002 +8.200e-002 +9.000e-002 +8.900e-002 +8.800e-002 +8.800e-002 +9.900e-002 +1.370e-001 +1.910e-001 +2.540e-001 +3.400e-001 +4.280e-001 +4.730e-001 +4.740e-001 +4.160e-001
+2.720e-001 +1.200e-001 -1.200e-002
      9.3643
                           1.11
      7.1613
                         15.85
     7.1613
                           2.37
                           9.33
      8.6767
    37.1754 10000000000.00
<Date: Thu Jul 03 14:14:50 2008
<Time Range=5 Currrent= 1.90 Stack= 5 Filter=50 Deff=</pre>
                                                                                                      6 Ampl=OFF
<Remark: 900M WESTERN OF ROUMELI</pre>
<Place: ROUMELI
<
```

## 1D\_Inversion\_Results\_TEM.txt

```
******
#GEOSEC: 0133-A
                                        50.0/ 50.0/
                                                                1.0/ 562733.000/ 3917961.000/
23.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                             0.000 \text{ DH} =
                                                                                                       0.000/rms=154.00
                +0.000e+000 +0.000e+000 +1.505e+001 +3.388e+001 +4.414e+001
+4.422e+001 +4.094e+001 +3.812e+001 +3.543e+001 +3.335e+001 +3.226e+001 +3.163e+001 +3.115e+001 +3.090e+001 +3.091e+001 +3.106e+001 +3.142e+001 +3.203e+001 +3.265e+001 +3.320e+001 +3.387e+001 +3.465e+001 +3.538e+001
+3.618e+001 +3.748e+001 +3.947e+001 +4.127e+001 +4.259e+001 +4.322e+001
+4.181e+001 +3.895e+001 +3.583e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +5.960e-001 -2.120e-001 -3.630e-001 -3.570e-001 -3.010e-001 -2.180e-001 -1.530e-001 -1.080e-001 -6.200e-002 -1.600e-002 +1.900e-002 +4.700e-002 +7.800e-002 +1.030e-001 +1.130e-001 +1.140e-001 +1.110e-001 +1.170e-001 +1.390e-001
+1.720e-001 +2.200e-001 +2.540e-001 +2.360e-001 +1.550e-001 -3.100e-002 -2.770e-001 -4.000e-001 -4.520e-001
   63.6185
                        7.23
   24.3934
                      22.98
   46.9131
                      72.30
                      47.25
   31.4218
     3.0000 10000000000.00
<Date: Thu Jul 03 14:54:30 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                            6 Ampl=OFF
<Remark: 700M WEST OF ROUMELI VILLAGE</pre>
<Place: ROUMELI
*****
#GEOSEC: 0134-C / 50.0/ 50.0/ 1.0/ 562291.000/ 3917906.000/ 26.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +4.686e+001 +5.396e+001 +5.395e+001 +5.169e+001 +4.786e+001
                                                                                                       0.000/rms=208.00
+4.310e+001 +3.925e+001 +3.617e+001 +3.275e+001 +2.954e+001 +2.755e+001
+2.634e+001 +2.546e+001 +2.517e+001 +2.547e+001 +2.608e+001 +2.724e+001 +2.909e+001 +3.093e+001 +3.264e+001 +3.475e+001 +3.698e+001 +3.851e+001 +3.951e+001 +4.033e+001 +4.069e+001 +4.056e+001 +4.020e+001 +3.957e+001 +3.873e+001 +3.804e+001 +3.744e+001 +3.663e+001 +3.544e+001 +3.412e+001
+3.272e+001
Err[V/A]:
                 -6.770e-001 -2.270e-001 +1.320e-001 +2.780e-001 -3.510e-001
-3.870e-001 -4.020e-001 -4.070e-001 -3.980e-001 -3.620e-001 -3.050e-001 -2.320e-001 -1.230e-001 +1.200e-002 +1.180e-001 +1.950e-001 +2.710e-001 +3.290e-001 +3.500e-001 +3.470e-001 +3.190e-001 +2.620e-001 +2.030e-001
+1.480e-001 +8.200e-002 +9.000e-003 -4.200e-002 -7.400e-002 -9.600e-002 -1.050e-001 -1.080e-001 -1.150e-001 -1.390e-001 -1.890e-001 -2.440e-001
-2.920e-001
   65.1981
                        7.90
   18.5626
                       13.62
   18.8025
                        6.30
  100.0000
                      68.39
22.1861 10000000000.00
<Date: Fri Jul 04 07:50:43 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                            6 Ampl=OFF
<Remark: FENCES IN LOOP, NEAR STREET</pre>
<Place: ROUMELI
*****
0.000/rms=251.00
+2.424e+001 +2.406e+001 +2.408e+001 +2.422e+001 +2.437e+001 +2.455e+001 +2.471e+001 +2.479e+001 +2.481e+001 +2.482e+001 +2.483e+001 +2.489e+001 +2.501e+001 +2.527e+001 +2.576e+001 +2.633e+001 +2.696e+001 +2.788e+001
+2.918e+001 +3.043e+001 +3.166e+001 +3.332e+001 +3.537e+001 +3.679e+001
+3.727e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.820e-001 +2.280e-001 -2.390e-001 -2.990e-001 -2.820e-001 -2.350e-001 -1.690e-001 -1.110e-001 -6.600e-002 -1.900e-002 +2.000e-002 +3.800e-002 +4.200e-002 +3.600e-002 +2.400e-002 +1.200e-002 +4.000e-003 +2.000e-003 +9.000e-003 +2.400e-002 +4.400e-002 +7.400e-002 +1.140e-001 +1.730e-001 +2.030e-001 +2.030e-001
+2.330e-001 +2.560e-001 +2.740e-001 +2.840e-001 +2.550e-001 +1.550e-001
```

```
1D_Inversion_Results_TEM.txt
+2.400e-002
     42.3453
20.1514
                                    5.07
                                 16.39
     28.1950
                                 59.17
     28.1950
                                 16.05
     96.1926 10000000000.00
 <Date: Fri Jul 04 08:17:29 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                                        6 Ampl=OFF
<Remark: FENCES IN LOOP, 170M W OF G-63</pre>
<Place: ROUMELI
<pre>
*****
#GEOSEC: 0136-B / 50.0 / 50.0 / 1.21.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                                                               1.0/ 563133.000/ 3918035.000/
                                                                                                                 0.000 DH=
                                                                                                                                                        0.000/rms=150.00
S [V/A]: +0.000e+000 +0.000e+000 +1.144e+001 +2.025e+001 +2.363e+001 +2.345e+001 +2.262e+001 +2.202e+001 +2.154e+001 +2.127e+001 +2.125e+001
+2.135e+001 +2.159e+001 +2.197e+001 +2.233e+001 +2.263e+001 +2.297e+001
+2.331e+001 +2.356e+001 +2.379e+001 +2.410e+001 +2.455e+001 +2.500e+001 +2.543e+001 +2.599e+001 +2.658e+001 +2.697e+001 +2.721e+001 +2.743e+001 +2.770e+001 +2.807e+001 +2.860e+001 +2.960e+001 +3.136e+001 +3.326e+001
+3.500e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.980e-001 +3.640e-001 -1.190e-001 -1.750e-001 -1.420e-001 -8.800e-002 -3.000e-002 +1.500e-002
+4.500e-002 +7.100e-002 +8.900e-002 +9.100e-002 +8.600e-002 +7.700e-002 +6.700e-002 +6.500e-002 +7.000e-002 +8.100e-002 +9.900e-002 +1.130e-001
+1.190e-001 +1.150e-001 +9.600e-002 +7.300e-002 +5.500e-002 +4.700e-002 +6.500e-002 +1.050e-001 +1.580e-001 +2.320e-001 +3.080e-001 +3.380e-001
+3.430e-001
     26.8890
                                    3.63
     20.2573
                                 18.01
     31.6690
                                 99.89
     31.6690
                                 25.09
100.0000 10000000000.00
<Date: Fri Jul 04 09:14:03 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                                        6 Ampl=OFF
<Remark: NEXT TO G-63, IN VILLAGE</pre>
<Place: ROUMELI
*****
#GEOSEC: 0137-B / 50.0/ 50.0/ 1.0/ 563556.000/ 3918127.000/ 28.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +2.712e+000 +1.305e+001 +1.772e+001 +2.010e+001 +2.090e+001 +2.090e+0
                                                                                                                                                        0.000/rms=143.00
+1.997e+001 +2.009e+001 +2.044e+001 +2.087e+001 +2.132e+001 +2.191e+001
+2.262e+001 +2.320e+001 +2.369e+001 +2.426e+001 +2.488e+001 +2.536e+001 +2.572e+001 +2.602e+001 +2.603e+001 +2.567e+001 +2.510e+001 +2.413e+001 +2.284e+001 +2.180e+001 +2.102e+001 +2.023e+001 +1.954e+001 +1.907e+001
+1.862e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.280e-001 +3.840e-001 +8.200e-002 -1.900e-002 -5.900e-002 -7.500e-002 -5.900e-002 -2.700e-002 +8.000e-003 +5.600e-002 +1.030e-001 +1.320e-001 +1.470e-001 +1.520e-001 +1.510e-001 +1.440e-001 +1.370e-001 +1.280e-001 +1.180e-001 +1.040e-001 +8.200e-002 +3.600e-002 -4.400e-002 -1.200e-001 -1.800e-001 -2.300e-001
-2.540e-001 -2.470e-001 -2.250e-001 -1.880e-001 -1.530e-001 -1.520e-001 -1.680e-001
     20.8501
                                  30.16
     53.3389
                                  13.97
                                 19.49
     30.0857
     30.0857
                                 16.96
     11.5004 10000000000.00
<Date: Fri Jul 04 09:58:28 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                                        6 Ampl=OFF
<Remark: IN ROUMELI VILLAGE</pre>
<Place: ROUMELI
 *****
                                                    / 50.0/ 50.0/ 1.0/ 563725.000/ 3917991.000/
#GEOSEC: 0138-B
45.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                  0.000 DH =
                                                                                                                                                     0.000/\text{rms} = 81.00
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +4.282e+000 +3.956e+000 +5.668e+000 +7.835e+000 +1.068e+001 +1.362e+001 +1.551e+001 +1.667e+001 +1.764e+001 +1.831e+001 +1.866e+001 +1.889e+001 +1.915e+001 +1.949e+001 +1.981e+001 +2.010e+001 +2.048e+001
+2.094e+001 +2.135e+001 +2.173e+001 +2.224e+001 +2.291e+001 +2.354e+001
+2.416e+001 +2.505e+001 +2.627e+001 +2.745e+001 +2.860e+001 +3.011e+001
+3.187e+001 +3.312e+001 +3.387e+001 +3.417e+001 +3.347e+001 +3.196e+001
+3.007e+001
Err[V/A]:
                 +5.000e-001 -6.810e-001 -8.910e-001 -8.870e-001 +8.410e-001
+6.930e-001 +5.140e-001 +3.680e-001 +2.340e-001 +1.350e-001 +9.300e-002
+7.900e-002 +8.000e-002 +8.900e-002 +9.500e-002 +1.000e-001 +1.060e-001 +1.110e-001 +1.170e-001 +1.240e-001 +1.360e-001 +1.520e-001 +1.700e-001 +1.880e-001 +2.130e-001 +2.440e-001 +2.670e-001 +2.790e-001 +2.780e-001 +2.460e-001 +1.870e-001 +1.080e-001 -2.000e-002 -1.880e-001 -3.130e-001
-3.940e-001
   15.3554
                        5.42
   23.6722
                      35.00
   37.7194
                      44.95
   50.1158
                     100.00
     4.1019 10000000000.00
<Date: Fri Jul 04 10:26:24 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                           6 Ampl=OFF
<Remark: IN ROUMELI VILLAGE</pre>
*****
#GEOSEC: 0139-C / 50.0/ 50.0/ 1.34.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                              1.0/ 564084.000/ 3918031.000/
                                                                           0.000 DH=
                                                                                                       0.000/rms=311.00
S [V/A]: +0.000e+000 +1.699e+000 +2.894e+001 +4.519e+001 +5.674e+001 +6.283e+001 +6.493e+001 +6.574e+001 +6.593e+001 +6.536e+001 +6.447e+001
+6.357e+001 +6.254e+001 +6.169e+001 +6.136e+001 +6.140e+001 +6.184e+001
+6.287e+001 +6.411e+001 +6.542e+001 +6.731e+001 +6.982e+001 +7.213e+001 +7.417e+001 +7.658e+001 +7.884e+001 +7.980e+001 +7.968e+001 +7.806e+001 +7.398e+001 +6.891e+001 +6.359e+001 +5.626e+001 +4.741e+001 +4.034e+001
+3.477e+001
                 -9.000e-001 -9.000e-001 -9.000e-001 -8.950e-001 +6.610e-001
Err[V/A]:
+2.870e-001 +1.220e-001 +5.000e-002 -1.000e-002 -6.000e-002 -8.500e-002 -9.100e-002 -7.800e-002 -4.600e-002 -1.100e-002 +2.000e-002 +5.800e-002 +9.800e-002 +1.270e-001 +1.470e-001 +1.670e-001 +1.830e-001 +1.900e-001 +1.850e-001 +1.610e-001 +1.030e-001 +2.800e-002 -5.800e-002 -1.790e-001
 -3.110e-001 -3.950e-001 -4.420e-001 -4.750e-001 -4.900e-001 -4.950e-001
-4.970e-001
   63.1169
   80.3178
                      80.79
     7.7353
                       17.60
   11.5662
                      17.48
     1.5614 10000000000.00
<Date: Fri Jul 04 10:57:54 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                           6 Ampl=OFF
<Remark: IN ROUMELI VILLAGE</pre>
*****
                                      50.0/ 50.0/
                                                                1.0/ 564560.000/ 3917920.000/
62.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +2.455e+001 +1.714e+001 +1.469e+001 +1.384e+001 +1.344e+001 +1.313e+001 +1.263e+001 +1.199e+001 +1.099e+001 +9.730e+000 +8.732e+000
                                                                                                       0.000/rms=978.00
+8.010e+000 +7.326e+000 +6.805e+000 +6.577e+000 +6.513e+000 +6.575e+000
+6.820e+000 +7.166e+000 +7.575e+000 +8.236e+000 +9.279e+000 +1.043e+001 +1.168e+001 +1.363e+001 +1.656e+001 +1.954e+001 +2.243e+001 +2.611e+001 +2.982e+001 +3.190e+001 +3.277e+001 +3.271e+001 +3.139e+001 +2.967e+001
+2.805e+001
Err[V/A]:
                 +5.000e-001 +4.950e-001 +4.070e-001 +2.360e-001 -1.200e-001
-1.560e-001 -2.550e-001 -3.360e-001 -4.070e-001 -4.330e-001 -4.330e-001 -4.330e-001 -4.130e-001 -3.580e-001 -2.490e-001 -1.230e-001 -1.300e-002 +1.100e-001 +2.340e-001 +3.270e-001 +3.990e-001 +4.810e-001 +5.680e-001 +6.300e-001 +6.760e-001 +7.180e-001 +7.450e-001 +7.460e-001 +7.210e-001 +6.430e-001 +4.740e-001 +2.770e-001 +9.800e-002 -9.800e-002 -2.550e-001 -3.200e-001
-3.510e-001
```

```
1D_Inversion_Results_TEM.txt
                 22.22
85.77
    8.2547
 200.0000
                  37.11
 156.4119
 156.4119
                 14.34
    1.0000 10000000000.00
<Date: Fri Jul 04 11:30:13 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                        6 Ampl=OFF
<Remark: EASTERN OF ROUMELI VILLAGE</pre>
<Place: ROUMELI
#GEOSEC: 0141-B / 50.0/ 50.0/ 1 57.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                  1.0/ 564339.000/ 3917893.000/
                                                            0.000 DH =
                                                                                 0.000/rms=663.00
    [V/A]: +0.000e+000 +6.689e+000 +1.014e+001 +1.183e+001 +1.289e+001
+1.308e+001 +1.258e+001 +1.185e+001 +1.077e+001 +9.546e+000 +8.724e+000 +8.225e+000 +7.872e+000 +7.783e+000 +7.946e+000 +8.229e+000 +8.772e+000
+9.674e+000 +1.068e+001 +1.177e+001 +1.342e+001 +1.586e+001 +1.834e+001
+2.077e+001 +2.401e+001 +2.788e+001 +3.087e+001 +3.321e+001 +3.553e+001
+3.700e+001 +3.683e+001 +3.566e+001 +3.334e+001 +3.011e+001 +2.742e+001
+2.521e+001
Err[V/A]:
             -9.000e-001 -9.000e-001 -8.560e-001 -5.880e-001 +2.450e-001
-8.\overline{400}e^{-002} -2.750e^{-001} -3.650e^{-001} -4.100e^{-001} -4.110e^{-001} -3.690e^{-001}
-2.920e-001 -1.500e-001 +4.000e-002 +1.820e-001 +2.840e-001 +3.900e-001 +4.890e-001 +5.570e-001 +6.040e-001 +6.500e-001 +6.850e-001 +6.950e-001 +6.860e-001 +6.510e-001 +5.810e-001 +5.040e-001 +4.230e-001 +2.890e-001
+7.500e-002 -1.300e-001 -2.700e-001 -3.650e-001 -4.100e-001 -4.260e-001
-4.350e-001
 9.6897
285.0710
                  19.59
                 99.85
 130.2786
                 11.68
 130.2786
                  13.45
    2.2887\ 100000000000.00
<Date: Fri Jul 04 11:56:01 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                        6 Ampl=OFF
<Remark: EASTERN OF ROUMELI VILLAGE</pre>
<Place: ROUMELI
<****************************
#GEOSEC: 0142-B
                            / 50.0/ 50.0/
                                                1.0/ 564801.000/ 3917916.000/
49.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                            0.000 DH =
                                                                                 0.000/\text{rms}=248.00
S [V/A]: +0.000e+000 +0.000e+000 +3.724e+000 +1.268e+001 +1.852e+001 +2.184e+001 +2.375e+001 +2.522e+001 +2.703e+001 +2.916e+001 +3.099e+001 +3.256e+001 +3.441e+001 +3.634e+001 +3.765e+001 +3.849e+001 +3.911e+001
+3.931e+001 +3.912e+001 +3.872e+001 +3.801e+001 +3.683e+001 +3.556e+001 +3.424e+001 +3.235e+001 +2.980e+001 +2.750e+001 +2.539e+001 +2.270e+001
+1.958e+001 +1.709e+001 +1.508e+001 +1.284e+001 +1.058e+001 +8.968e+000
+7.763e+000
Err[V/A]:
             +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.440e-001
+5.150e-001 +3.900e-001 +3.580e-001 +3.440e-001 +3.340e-001 +3.230e-001
+3.070e-001 +2.760e-001 +2.260e-001 +1.730e-001 +1.220e-001 +5.900e-002 -5.000e-003 -5.000e-002 -8.500e-002 -1.250e-001 -1.770e-001 -2.230e-001 -2.650e-001 -3.160e-001 -3.690e-001 -4.060e-001 -4.330e-001 -4.580e-001
-4.760e-001 -4.850e-001 -4.890e-001 -4.920e-001 -4.940e-001 -4.950e-001
-4.960e-001
 24.6120
193.7436
                  14.31
                 17.89
  19.7292
                  33.49
    4.4253
                  19.29
    1.0000 10000000000.00
<Date: Fri Jul 04 12:21:59 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                        6 Ampl=OFF
<Remark: 470M NE OF G-81</pre>
*****
#GEOSEC: 0143-C / 50.0/ 50.0/ 1.0/ 565013.000/ 3917822.000/ 53.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                0.000/\text{rms}=119.00
S [V/A]: +0.000e+000 +1.440e-001 +1.596e+001 +2.403e+001 +2.786e+001
                                             Σελίδα 49
```

```
1D_Inversion_Results_TEM.txt
+2.802e+001 +2.675e+001 +2.529e+001 +2.345e+001 +2.152e+001 +2.019e+001 +1.926e+001 +1.841e+001 +1.774e+001 +1.742e+001 +1.730e+001 +1.733e+001 +1.761e+001 +1.807e+001 +1.863e+001 +1.956e+001 +2.101e+001 +2.257e+001
+2.419e+001 +2.656e+001 +2.978e+001 +3.268e+001 +3.516e+001 +3.782e+001
+3.977e+001 +4.013e+001 +3.952e+001 +3.790e+001 +3.531e+001 +3.290e+001
+3.080e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.810e-001 +3.740e-001 -1.230e-001 -2.800e-001 -3.280e-001 -3.420e-001 -3.290e-001 -3.000e-001
-2.620e-001 -2.060e-001 -1.340e-001 -7.200e-002 -2.200e-002 +4.200e-002
+1.160e-001 +1.800e-001 +2.340e-001 +3.000e-001 +3.720e-001 +4.260e-001 +4.630e-001 +4.950e-001 +5.060e-001 +4.850e-001 +4.350e-001 +3.240e-001 +1.390e-001 -3.200e-002 -1.600e-001 -2.660e-001 -3.350e-001 -3.670e-001
-3.860e-001
   28.3715
                   7.31
26.19
   14.7373
 200.0000
                  125.60
    5.6735 10000000000.00
<Date: Fri Jul 04 13:18:57 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
<Remark: 200M NW OF G-81
<Place: SIRIPIDIANA
*****
#GEOSEC: 0144-B / 50.0/ 50.0/ 1.50.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 565291.000/ 3917871.000/
                                                                 0.000 DH=
                                                                                       0.000/\text{rms} = 65.00
              +0.000e+000 +3.144e+000 +1.290e+001 +1.808e+001 +2.180e+001
S [V/A]:
+2.446e+001 +2.603e+001 +2.706e+001 +2.802e+001 +2.878e+001 +2.921e+001
+2.947e+001 +2.970e+001 +2.985e+001 +2.986e+001 +2.978e+001 +2.954e+001 +2.910e+001 +2.859e+001 +2.808e+001 +2.734e+001 +2.633e+001 +2.532e+001
+2.434e+001 +2.299e+001 +2.129e+001 +1.989e+001 +1.872e+001 +1.741e+001
+1.612e+001 +1.525e+001 +1.466e+001 +1.412e+001 +1.378e+001 +1.375e+001
+1.395e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.680e-001 +6.160e-001 +3.860e-001 +2.780e-001 +2.150e-001 +1.550e-001 +1.020e-001 +7.000e-002
+5.100e-002 +3.400e-002 +1.200e-002 -9.000e-003 -3.000e-002 -5.800e-002
-8.900e-002 -1.130e-001 -1.330e-001 -1.610e-001 -2.000e-001 -2.380e-001
-2.710e-001 -3.080e-001 -3.390e-001 -3.520e-001 -3.530e-001 -3.410e-001 -3.110e-001 -2.740e-001 -2.320e-001 -1.640e-001 -6.100e-002 +4.900e-002
+1.520e-001
   24.0866
35.7429
                    8.05
                   21.17
   17.8383
                   35.57
                   59.04
    7.2654
 100.0000 10000000000.00
<Date: Fri Jul 04 13:51:31 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
<Remark: NEAR G-81, FENCES, POWER LINES</pre>
<Place: SIRIPIDIANÁ
<
*****
#GEOSEC: 0145-B / 50.0/ 50.0/ 1.
54.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 565519.000/ 3917766.000/
                                                                0.000 DH =
                                                                                       0.000/rms=195.00
S [V/A]: +0.000e+000 +0.000e+000 +1.539e+001 +2.560e+001 +3.139e+001
+3.341e+001 +3.354e+001 +3.317e+001 +3.244e+001 +3.142e+001 +3.051e+001 +2.976e+001 +2.891e+001 +2.806e+001 +2.749e+001 +2.711e+001 +2.676e+001 +2.654e+001 +2.648e+001 +2.651e+001 +2.665e+001 +2.694e+001 +2.728e+001
+2.766e+001 +2.825e+001 +2.916e+001 +3.015e+001 +3.122e+001 +3.283e+001
+3.512e+001 +3.733e+001 +3.936e+001 +4.188e+001 +4.446e+001 +4.593e+001
+4.642e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.970e-001 +5.750e-001 +1.320e-001 -2.900e-002 -9.000e-002 -1.290e-001 -1.540e-001 -1.610e-001
-1.580e-001 -1.480e-001 -1.270e-001 -1.040e-001 -8.400e-002 -5.700e-002
-2.600e-002 -1.000e-003 +1.900e-002 +4.000e-002 +6.500e-002 +8.500e-002 +1.040e-001 +1.350e-001 +1.770e-001 +2.180e-001 +2.550e-001 +2.970e-001 +3.350e-001 +3.500e-001 +3.470e-001 +3.140e-001 +2.340e-001 +1.270e-001
+1.700e-002
   31.6015
                   17.20
                   31.39
   22.2653
```

```
1D_Inversion_Results_TEM.txt
   51.3509
                 119.92
 100.0000
                 104.40
    1.6644 10000000000.00
<Date: Fri Jul 04 14:24:33 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                            6 Ampl=OFF
<Remark: 250M EAST OF G-81, POWER LINES</pre>
<Place: SIRIPIDIANA
*****
#GEOSEC: 0146-B / 50.0/ 50.0/ 1.0 67.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 565669.000/ 3917813.000/
                                                               0.000 \, DH =
                                                                                     0.000/rms=187.00
              +0.000e+000 +0.000e+000 +1.486e+001 +2.394e+001 +2.989e+001
    [V/A]:
+3.337e+001 +3.510e+001 +3.612e+001 +3.682e+001 +3.698e+001 +3.663e+001
+3.604e+001 +3.509e+001 +3.383e+001 +3.272e+001 +3.181e+001 +3.077e+001
+2.975e+001 +2.908e+001 +2.864e+001 +2.827e+001 +2.802e+001 +2.795e+001 +2.799e+001 +2.817e+001 +2.864e+001 +2.930e+001 +3.013e+001 +3.152e+001
+3.368e+001 +3.590e+001 +3.801e+001 +4.060e+001 +4.308e+001 +4.431e+001
+4.470e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.960e-001 +6.630e-001 +3.480e-001 +2.180e-001 +1.450e-001 +6.300e-002 -2.100e-002 -8.200e-002 -1.230e-001 -1.550e-001 -1.780e-001 -1.850e-001 -1.820e-001 -1.690e-001 -1.440e-001 -1.160e-001 -9.000e-002 -5.900e-002 -2.700e-002 -2.000e-003
+2.100e-002 +5.700e-002 +1.100e-001 +1.650e-001 +2.170e-001 +2.800e-001
+3.410e-001 +3.700e-001 +3.680e-001 +3.240e-001 +2.200e-001 +1.090e-001
+1.200e-002
   34.5895
                   30.31
   19.2108
                   27.73
                 77.63
127.20
   51.0888
 100.0000
    2.8751 10000000000.00
<Date: Fri Jul 04 14:55:43 2008</pre>
<Time Range=6 Currrent= 3.60 Stack= 5 Filter=50 Deff=</pre>
                                                                            6 Ampl=OFF
*****
#GEOSEC: 0147-B / 50.0/ 50.0/ 1.0/ 563677.000/ 3914933.000/ 41.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +6.025e+001 +4.729e+001 +4.182e+001 +3.919e+001 +3.749e+001
                                                                                     0.000/\text{rms} = 96.00
+3.659e+001 +3.612e+001 +3.576e+001 +3.521e+001 +3.441e+001 +3.364e+001 +3.301e+001 +3.233e+001 +3.170e+001 +3.133e+001 +3.109e+001 +3.084e+001 +3.058e+001 +3.034e+001 +3.010e+001 +2.973e+001 +2.923e+001 +2.874e+001 +2.828e+001 +2.768e+001 +2.638e+001 +2.588e+001 +2.528e+001
+2.453e+001 +2.379e+001 +2.300e+001
Err[V/A]: +4.980e-001 +4.680e-001 +3.820e-001 +2.750e-001 -1.600e-001 -8.500e-002 -6.500e-002 -7.100e-002 -9.300e-002 -1.160e-001 -1.240e-001 -1.180e-001 -1.030e-001 -7.900e-002 -6.000e-002 -4.900e-002 -4.200e-002 -4.400e-002 -5.100e-002 -6.100e-002 -7.500e-002 -9.100e-002 -1.050e-001 -1.320e-001 -1.320e-001 -1.380e-001
-1.140e-001 -1.220e-001 -1.270e-001 -1.280e-001 -1.300e-001 -1.380e-001
-1.620e-001 -2.010e-001 -2.410e-001
   35.7845
                   14.07
   26.4569
                   44.58
   26.4569
                    6.48
   17.2883 57.04
12.9405 10000000000.00
<Date: Mon Jul 07 07:44:49 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                            6 Ampl=OFF
<Remark: NEAR STREET, POWER LINES</pre>
<Place: PERAMA
******
0.000/\text{rms}=241.00
```

```
1D_Inversion_Results_TEM.txt
+3.416e+001 +3.408e+001 +3.379e+001 +3.331e+001 +3.277e+001 +3.246e+001
+3.231e+001
Err[V/A]:
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +5.820e-001
-7.400e-002 -2.340e-001 -2.590e-001 -2.470e-001 -2.050e-001 -1.560e-001
-1.060e-001 -3.700e-002 +4.400e-002 +1.040e-001 +1.490e-001 +1.970e-001
+2.390e-001 +2.620e-001 +2.720e-001 +2.730e-001 +2.670e-001 +2.560e-001 +2.450e-001 +2.270e-001 +2.010e-001 +1.350e-001 +8.100e-002 +1.300e-002 -3.800e-002 -6.800e-002 -8.000e-002 -6.700e-002 -4.400e-002
-2.200e-002
 21.3425
200.0000
                  38.47
                  42.66
                   4.52
 200.0000
   26.3378 10000000000.00
<Date: Mon Jul 07 08:52:14 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NEAR IRAKLIS FACTORY
                                                                        6 Ampl=OFF
<Place: PERAMA
*****
                               50.0/ 50.0/ 1.
= 0.000e+000 H=
#GEOSEC: 0149-B
                                                  1.0/ 563094.000/ 3915118.000/
53.0/36/5/0/22222 SPM=0 K=
                                                                                 0.000/rms = 80.00
                                                             0.000 DH =
             +1.207e+001 +9.636e+000 +1.001e+001 +1.103e+001 +1.239e+001
+1.357e+001 +1.402e+001 +1.408e+001 +1.386e+001 +1.347e+001 +1.319e+001
+1.304e+001 +1.301e+001 +1.316e+001 +1.344e+001 +1.378e+001 +1.433e+001 +1.511e+001 +1.590e+001 +1.665e+001 +1.767e+001 +1.896e+001 +2.010e+001
+2.109e+001 +2.232e+001 +2.372e+001 +2.482e+001 +2.573e+001 +2.680e+001
+2.798e+001 +2.887e+001 +2.956e+001 +3.025e+001 +3.075e+001 +3.081e+001
+3.056e+001
Err[V/A]: +5.000e-001 +2.490e-001 -3.690e-001 -5.100e-001 +4.520e-001 +2.670e-001 +9.300e-002 -2.500e-002 -1.040e-001 -1.230e-001 -9.500e-002
-4.700e-002 +2.000e-002 +9.000e-002 +1.470e-001 +1.890e-001 +2.310e-001
+2.720e-001 +2.990e-001 +3.160e-001 +3.270e-001 +3.310e-001 +3.260e-001 +3.160e-001 +2.990e-001 +2.740e-001 +2.540e-001 +2.370e-001 +2.180e-001 +1.950e-001 +1.720e-001 +1.480e-001 +1.070e-001 +4.300e-002 -2.600e-002
-9.000e-002
  14.1277
                  27.51
 200.0000
                  28.39
  35.7740
35.6846
                  93.68
                  55.74
   19.5204 10000000000.00
<Date: Mon Jul 07 09:35:36 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NEAR IRAKLIS FACTORY
                                                                        6 Ampl=OFF
<Place: PERAMA
******
#GEOSEC: 0150-B / 50.0/50.0/150.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                  1.0/ 562873.000/ 3915175.000/
                                                             0.000 \text{ DH} =
                                                                                 0.000/rms=420.00
             +0.000e+000 +0.000e+000 +1.092e+001 +2.205e+001 +2.785e+001
+2.956e+001 +2.968e+001 +2.953e+001 +2.925e+001 +2.877e+001 +2.826e+001
+2.776e+001 +2.714e+001 +2.657e+001 +2.630e+001 +2.629e+001 +2.658e+001
+2.737e+001 +2.836e+001 +2.942e+001 +3.088e+001 +3.255e+001 +3.371e+001
+3.440e+001 +3.478e+001 +3.452e+001 +3.378e+001 +3.273e+001 +3.090e+001
+2.812e+001 +2.549e+001 +2.324e+001 +2.071e+001 +1.830e+001 +1.678e+001
+1.580e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -6.200e-001 -1.270e-001 -7.000e-003 -4.000e-002 -6.300e-002 -8.900e-002 -1.090e-001
-1.190e-001 -1.120e-001 -7.800e-002 -2.800e-002 +2.600e-002 +9.800e-002
+1.770e-001 +2.280e-001 +2.540e-001 +2.590e-001 +2.260e-001 +1.690e-001 +1.040e-001 +1.600e-002 -8.700e-002 -1.720e-001 -2.480e-001 -3.370e-001 -4.100e-001 -4.410e-001 -4.500e-001 -4.460e-001 -4.210e-001 -3.790e-001
-3.250e-001
   28.6305
                100.00
    2.2605
2.2497
                  17.08
                   5.81
    2.2497
                   5.81
    1.0000 10000000000.00
<Date: Mon Jul 07 10:10:39 2008</pre>
```

```
1D_Inversion_Results_TEM.txt
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                              6 Ampl=OFF
<Remark: POWER LINES</pre>
<Place: PERAMA
******
#GEOSEC: 0151-D / 50.0 / 50.0 / 1.71.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 561951.000/ 3915410.000/
                                                                 0.000 DH =
                                                                                       0.000/\text{rms}=220.00
S [V/A]:
              +0.000e+000 +0.000e+000 +0.000e+000 +8.415e+000 +1.549e+001
+1.892e+001 +2.005e+001 +2.044e+001 +2.047e+001 +2.020e+001 +1.989e+001
+1.963e+001 +1.933e+001 +1.906e+001 +1.886e+001 +1.870e+001 +1.850e+001 +1.829e+001 +1.812e+001 +1.803e+001 +1.799e+001 +1.809e+001 +1.832e+001
+1.867e+001 +1.928e+001 +2.033e+001 +2.147e+001 +2.265e+001 +2.430e+001
+2.627e+001 +2.758e+001 +2.809e+001 +2.757e+001 +2.521e+001 +2.220e+001
+1.930e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.960e-001 +5.080e-001 +2.050e-001 +7.100e-002 -2.500e-002 -7.400e-002 -8.700e-002
-8.600e-002 -7.600e-002 -6.300e-002 -5.800e-002 -5.800e-002 -5.800e-002
-5.400e-002 -4.400e-002 -2.600e-002 +6.000e-003 +5.400e-002 +1.040e-001
+1.520e-001 +2.140e-001 +2.860e-001 +3.360e-001 +3.670e-001 +3.730e-001 +3.190e-001 +1.990e-001 +2.300e-002 -2.440e-001 -4.400e-001 -4.880e-001
-4.970e-001
   19.4391
                   19.24
                   41.86 47.27
   16.8520
  75.7508
75.7508
                   31.93
    1.0000 10000000000.00
<Date: Mon Jul 07 10:44:21 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
<Remark: POWER LINE
<Place: AGGELIANA
*****
#GEOSEC: 0152-B / 50.0/ 50.0/ 1.0/ 562147.000/ 3915278.000/ 68.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +0.000e+000 +1.740e+000 +9.752e+000 +1.483e+001
                                                                                       0.000/\text{rms}=119.00
+1.705e+001 +1.767e+001 +1.782e+001 +1.773e+001 +1.746e+001 +1.721e+001
+1.704e+001 +1.690e+001 +1.684e+001 +1.687e+001 +1.695e+001 +1.709e+001 +1.732e+001 +1.755e+001 +1.778e+001 +1.810e+001 +1.850e+001 +1.883e+001
+1.910e+001 +1.934e+001 +1.944e+001 +1.931e+001 +1.902e+001 +1.842e+001
+1.740e+001 +1.630e+001 +1.520e+001 +1.372e+001 +1.193e+001 +1.049e+001
+9.361e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.530e-001 +3.600e-001 +1.160e-001 +1.600e-002 -4.700e-002 -7.500e-002 -7.300e-002
-5.700e-002 -3.200e-002 -2.000e-003 +2.200e-002 +3.800e-002 +5.400e-002
+7.200e-002 +8.400e-002 +9.300e-002 +1.030e-001 +1.060e-001 +1.000e-001 +8.400e-002 +5.000e-002 -1.000e-002 -7.400e-002 -1.360e-001 -2.150e-001 -3.030e-001 -3.670e-001 -4.100e-001 -4.460e-001 -4.690e-001 -4.770e-001
-4.810e-001
   17.0774
                   16.22
   17.6501
                   41.31
   12.4933
                   22.65
                   18.04
    3.0000
    1.0000 10000000000.00
<Date: Mon Jul 07 11:05:33 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
<Remark: 300M EAST OF AGGELIANA VILLAGE</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0153-C
                                 50.0/ 50.0/
                                                      1.0/ 562334.000/ 3915224.000/
61.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/0 S [V/A]: +5.984e+000 +4.524e+000 +5.353e+000 +6.677e+000 +8.445e+000
                                                                                       0.000/\text{rms} = 76.00
+1.012e+001 +1.098e+001 +1.134e+001 +1.143e+001 +1.129e+001 +1.113e+001 +1.102e+001 +1.094e+001 +1.097e+001 +1.111e+001 +1.127e+001 +1.156e+001 +1.198e+001 +1.241e+001 +1.281e+001 +1.337e+001 +1.47e+001 +1.470e+001 +1.525e+001 +1.594e+001 +1.669e+001 +1.720e+001 +1.753e+001 +1.75e+001 +1.75e+001 +1.75e+001 +1.75e+001 +1.75e+001 +1.75e+001 +1.528e+001
+1.446e+001
```

```
1D_Inversion_Results_TEM.txt
Err[V/A]: +5.000e-001 +9.000e-003 -7.780e-001 -8.230e-001 +7.470e-001 +5.320e-001 +3.010e-001 +1.320e-001 -5.000e-003 -7.100e-002 -7.300e-002 -5.400e-002 -1.400e-002 +4.500e-002 +8.500e-002 +1.170e-001 +1.550e-001
+1.890e-001 +2.100e-001 +2.240e-001 +2.380e-001 +2.490e-001 +2.520e-001
+2.480e-001 +2.330e-001 +1.970e-001 +1.530e-001 +1.040e-001 +3.700e-002 -3.900e-002 -9.400e-002 -1.340e-001 -1.800e-001 -2.400e-001 -3.030e-001
-3.580e-001
   11.5892
                    23.04
   26.3494
                    44.78
   26.3494
                    21.98
     5.6243
                    58.63
    1.7152 10000000000.00
<Date: Mon Jul 07 11:35:16 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                   6 Ampl=OFF
<Remark: 570M EAST OF AGGELIANA VILLAGE</pre>
<Place: AGGELIANA
******
#GEOSEC: 0154-B / 50.0/ 50.0/ 1.
58.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          1.0/ 562662.000/ 3915230.000/
                                                                     0.000 DH =
                                                                                             0.000/\text{rms}=372.00
    [V/A]:
               +0.000e+000 +0.000e+000 +7.752e+000 +1.447e+001 +1.820e+001
+1.937e+001 +1.928e+001 +1.884e+001 +1.814e+001 +1.735e+001 +1.681e+001
+1.651e+001 +1.635e+001 +1.639e+001 +1.661e+001 +1.692e+001 +1.741e+001
+1.817e+001 +1.893e+001 +1.970e+001 +2.080e+001 +2.228e+001 +2.368e+001 +2.493e+001 +2.637e+001 +2.758e+001 +2.793e+001 +2.770e+001 +2.691e+001
+2.561e+001 +2.437e+001 +2.317e+001 +2.138e+001 +1.863e+001 +1.589e+001
+1.344e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.160e-001 +1.070e-001 -9.000e-002 -1.660e-001 -1.950e-001 -1.830e-001 -1.430e-001 -9.000e-002 -2.300e-002 +4.700e-002 +1.020e-001 +1.400e-001 +1.800e-001
+2.220e-001 +2.530e-001 +2.790e-001 +3.090e-001 +3.350e-001 +3.420e-001 +3.260e-001 +2.660e-001 +1.380e-001 +5.000e-003 -1.030e-001 -1.930e-001 -2.520e-001 -2.920e-001 -3.430e-001 -4.220e-001 -4.830e-001 -4.970e-001
-5.000e-001
 17.5837
124.3272
                    34.60
                    38.12
   16.4051
                    18.17
    4.6098
                    31.89
    1.0000 10000000000.00
<Date: Mon Jul 07 12:13:44 2008
<Time Range=6 Currrent= 1.90 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark: 870M EAST OF AGGELIANA VILLAGE</pre>
*****
#GEOSEC: 0155-B / 50.0/ 50.0/ 1.
57.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         1.0/ 562775.000/ 3915068.000/
                                                                                             0.000/rms=131.00
                                                                     0.000 DH =
               +0.000e+000 +0.000e+000 +3.535e+000 +1.449e+001 +2.110e+001
+2.364e+001 +2.423e+001 +2.435e+001 +2.439e+001 +2.442e+001 +2.451e+001 +2.470e+001 +2.507e+001 +2.574e+001 +2.650e+001 +2.728e+001 +2.838e+001 +2.984e+001 +3.116e+001 +3.231e+001 +3.365e+001 +3.494e+001 +3.566e+001
+3.594e+001 +3.584e+001 +3.521e+001 +3.438e+001 +3.350e+001 +3.224e+001 +3.057e+001 +2.904e+001 +2.764e+001 +2.585e+001 +2.374e+001 +2.198e+001
+2.047e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.200e-001 +2.850e-001 +7.700e-002 +2.100e-002 +7.000e-003 +1.400e-002 +3.800e-002
+6.500e-002 +1.020e-001 +1.470e-001 +1.810e-001 +2.060e-001 +2.270e-001
+2.430e-001 +2.450e-001 +2.350e-001 +2.050e-001 +1.470e-001 +8.300e-002 +2.300e-002 -4.800e-002 -1.160e-001 -1.590e-001 -1.890e-001 -2.240e-001 -2.630e-001 -2.940e-001 -3.170e-001 -3.420e-001 -3.660e-001 -3.860e-001
-4.030e-001
   25.0604
                    23.57
                    64.06
   49.0827
                    51.80
    8.9753
    3.1049
                    38.34
    1.1485 10000000000.00
<Date: Mon Jul 07 12:51:44 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
                                                   Σελίδα 54
```

## 1D\_Inversion\_Results\_TEM.txt

```
<Remark: NEAR WELLS
<Place: AGGELIANA
*****
#GEOSEC: 0156-C / 50.0/ 50.0/ 1. 41.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 563019.000/ 3915327.000/
                                                              0.000 DH =
                                                                                     0.000/\text{rms}=626.00
S [V/A]: +0.000e+000 +0.000e+000 +1.264e+001 +2.247e+001 +2.710e+001
+2.771e+001 +2.688e+001 +2.584e+001 +2.443e+001 +2.280e+001 +2.155e+001
+2.058e+001 +1.957e+001 +1.866e+001 +1.808e+001 +1.772e+001 +1.745e+001
+1.736e+001 +1.747e+001 +1.768e+001 +1.808e+001 +1.873e+001 +1.938e+001 +2.001e+001 +2.086e+001 +2.195e+001 +2.293e+001 +2.382e+001 +2.494e+001
+2.620e+001 +2.719e+001 +2.800e+001 +2.904e+001 +3.046e+001 +3.189e+001
+3.316e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +4.850e-001 -4.500e-002 -2.010e-001 -2.520e-001 -2.800e-001 -2.890e-001 -2.830e-001 -2.680e-001 -2.380e-001 -1.950e-001 -1.530e-001 -1.110e-001 -5.700e-002
+8.000e-003 +6.000e-002 +1.020e-001 +1.470e-001 +1.860e-001 +2.090e-001
+2.230e-001 +2.370e-001 +2.490e-001 +2.560e-001 +2.560e-001 +2.470e-001 +2.260e-001 +2.080e-001 +2.030e-001 +2.170e-001 +2.490e-001 +2.650e-001
+2.660e-001
  19.5671
                  62.30
 200.0000
                  65.72
  25.4326
                  99.62
 100.0000
                 100.00
    8.1718 10000000000.00
<Date: Mon Jul 07 14:06:45 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: NEAR WELLS
<Place: AGGELIANA
<**************************
*****
#GEOSEC: 0157-B / 50.0/ 50.0/ 1.0 70.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 562946.000/ 3914898.000/
                                                              0.000 DH =
                                                                                     0.000/\text{rms}=192.00
    [V/A]: +0.000e+000 +0.000e+000 +1.416e+001 +2.475e+001 +3.019e+001
+3.158e+001 +3.137e+001 +3.099e+001 +3.058e+001 +3.032e+001 +3.036e+001
+3.065e+001 +3.132e+001 +3.257e+001 +3.399e+001 +3.545e+001 +3.750e+001
+4.012e+001 +4.235e+001 +4.420e+001 +4.632e+001 +4.843e+001 +4.991e+001 +5.097e+001 +5.205e+001 +5.297e+001 +5.346e+001 +5.374e+001 +5.401e+001 +5.46e+001 +5.512e+001 +5.596e+001 +5.724e+001 +5.856e+001 +5.860e+001
+5.702e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +5.400e-001 +6.700e-002 -5.800e-002 -7.400e-002 -5.500e-002 -1.400e-002 +3.700e-002 +8.700e-002 +1.490e-001 +2.160e-001 +2.620e-001 +2.900e-001 +3.090e-001
+3.110e-001 +2.960e-001 +2.730e-001 +2.370e-001 +1.930e-001 +1.590e-001 +1.320e-001 +1.020e-001 +6.900e-002 +4.500e-002 +3.300e-002 +3.400e-002 +5.700e-002 +8.900e-002 +1.150e-001 +1.200e-001 +5.300e-002 -9.900e-002
-2.580e-001
   31.9213
                   30.59
 200.0000
                   30.12
 200.0000
                   1.19
   58.8632 10000000000.00
<Date: Mon Jul 07 14:33:31 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                           6 Ampl=OFF
<Remark: ŠE OF WELL-10</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0158-B / 50.0/ 50.0/ 1.0/ 563205.000/ 3914846.000/ 57.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +0.000e+000 +6.974e+000 +1.646e+001 +2.185e+001
                                                                                     0.000/rms=105.00
+2.388e+001 +2.434e+001 +2.440e+001 +2.434e+001 +2.423e+001 +2.419e+001
+2.428e+001 +2.457e+001 +2.517e+001 +2.590e+001 +2.665e+001 +2.774e+001
+2.917e+001 +3.046e+001 +3.160e+001 +3.301e+001 +3.455e+001 +3.571e+001 +3.658e+001 +3.746e+001 +3.821e+001 +3.861e+001 +3.882e+001 +3.892e+001
+3.890e+001 +3.882e+001 +3.875e+001 +3.867e+001 +3.841e+001 +3.772e+001
+3.639e+001
Err[V/A]: +5.000e-001 - 9.000e-001 - 9.000e-001 - 9.000e-001 + 7.200e-001
+2.250e-001 +5.400e-002 +2.000e-003 -1.700e-002 -1.500e-002 +1.000e-002
```

```
1D_Inversion_Results_TEM.txt
+4.300e-002 +8.800e-002 +1.410e-001 +1.790e-001 +2.050e-001 +2.280e-001 +2.440e-001 +2.480e-001 +2.440e-001 +2.300e-001 +2.050e-001 +1.770e-001 +1.500e-001 +1.160e-001 +7.800e-002 +4.900e-002 +2.700e-002 +6.000e-003 -8.000e-003 -1.200e-002 -1.200e-002 -2.100e-002 -7.400e-002 -1.770e-001
-2.830e-001
  25.1333
67.4777
                   27.57
                   46.44
   67.4777
                   14.33
   28.9317
                  160.43
    8.8197 10000000000.00
<Date: Mon Jul 07 15:05:02 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                             6 Ampl=OFF
<Remark: OLIVE TREES
*****
                                50.0/ 50.0/
                                                      1.0/ 563371.000/ 3914879.000/
#GEOSEC: 0159-C
53.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      0.000/rms=140.00
                                                               0.000 \, DH =
S [V/A]: +0.000e+000 +0.000e+000 +5.599e+000 +1.249e+001 +1.660e+001 +1.841e+001 +1.894e+001 +1.909e+001 +1.919e+001 +1.932e+001 +1.954e+001
+1.989e+001 +2.051e+001 +2.151e+001 +2.257e+001 +2.358e+001 +2.492e+001
+2.646e+001 +2.765e+001 +2.853e+001 +2.945e+001 +3.033e+001 +3.100e+001
+3.157e+001 +3.230e+001 +3.311e+001 +3.366e+001 +3.399e+001 +3.421e+001 +3.433e+001 +3.445e+001 +3.465e+001 +3.509e+001 +3.574e+001 +3.614e+001
+3.605e+001
Err[V/A]:
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.350e-001
+2.770e-001 +9.700e-002 +4.100e-002 +2.900e-002 +4.900e-002 +9.200e-002
+1.390e-001 +1.940e-001 +2.490e-001 +2.810e-001 +2.940e-001 +2.910e-001 +2.660e-001 +2.310e-001 +1.970e-001 +1.610e-001 +1.340e-001 +1.260e-001
+1.270e-001 +1.240e-001 +1.080e-001 +8.100e-002 +5.400e-002 +2.700e-002
+1.900e-002 +3.200e-002 +5.500e-002 +8.000e-002 +7.700e-002 +2.100e-002
-5.400e-002
   20.3660
                   20.15
                   32.92
   58.8600
   58.8600
                    6.26
                   50.69
   32.6057
   39.8862 10000000000.00
<Date: Mon Jul 07 15:51:29 2008</pre>
<Time Range=6 Currrent= 2.80 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: POWER LINES</pre>
<Place: PERAMA
<pre>
*****
                                50.0/ 50.0/
                                                              563562.000/ 3914735.000/
                                                      1.0/
46.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                      0.000/rms=158.00
S [V/A]: +0.000e+000 +5.141e+000 +2.171e+001 +3.181e+001 +3.948e+001 +4.388e+001 +4.501e+001 +4.484e+001 +4.379e+001 +4.208e+001 +4.058e+001 +3.933e+001 +3.792e+001 +3.653e+001 +3.558e+001 +3.497e+001 +3.446e+001
+3.424e+001 +3.437e+001 +3.468e+001 +3.532e+001 +3.633e+001 +3.731e+001
+3.819e+001 +3.923e+001 +4.032e+001 +4.111e+001 +4.178e+001 +4.268e+001
+4.403e+001 +4.553e+001 +4.716e+001
Frr[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 +6.490e-001 +2.730e-001 +4.900e-002 -7.000e-002 -1.490e-001 -1.880e-001 -1.980e-001 -1.960e-001 -1.840e-001 -1.590e-001 -1.310e-001 -1.010e-001 -5.700e-002 -2.000e-003 +4.400e-002 +8.000e-002 +1.180e-001 +1.470e-001 +1.580e-001 +1.550e-001 +1.420e-001 +1.230e-001 +1.130e-001 +1.160e-001 +1.350e-001 +1.760e-001 +2.190e-001 +2.590e-001
   43.5318
                   21.05
   25.8259
                   30.97
 133.7985
                   46.87
   32.3619
                  136.52
    1.0000 10000000000.00
<Date: Mon Jul 07 16:14:58 2008</pre>
<Time Range=5 Currrent= 3.10 Stack= 5 Filter=50 Deff=</pre>
                                                                             6 Ampl=OFF
<Remark: POWER LINES, FENCES</pre>
<Place: PERAMA
*****
```

```
1D_Inversion_Results_TEM.txt
#GEOSEC: 0161-C / 50.0/ 50.0/ 1.0/ 563458.000/ 3916768.000/ 30.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                                             0.000/rms = 73.00
S [V/A]: +0.000e+000 +2.599e+001 +4.146e+001 +4.768e+001 +4.952e+001 +4.753e+001 +4.442e+001 +4.138e+001 +3.753e+001 +3.338e+001 +3.041e+001
+2.832e+001 +2.629e+001 +2.463e+001 +2.372e+001 +2.325e+001 +2.300e+001 +2.309e+001 +2.344e+001 +2.393e+001 +2.474e+001 +2.594e+001 +2.714e+001 +2.827e+001 +2.978e+001 +3.160e+001 +3.305e+001 +3.419e+001 +3.533e+001
+3.616e+001 +3.631e+001 +3.599e+001 +3.499e+001 +3.295e+001 +3.058e+001
+2.813e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.650e-001 -4.790e-001 +1.400e-002 -2.580e-001 -3.490e-001 -3.870e-001 -4.100e-001 -4.120e-001 -3.960e-001 -3.690e-001 -3.190e-001 -2.430e-001 -1.670e-001 -1.020e-001 -2.400e-002
+5.700e-002 +1.170e-001 +1.610e-001 +2.040e-001 +2.450e-001 +2.680e-001
+2.800e-001 +2.830e-001 +2.700e-001 +2.450e-001 +2.100e-001 +1.510e-001 +6.500e-002 -2.100e-002 -1.040e-001 -2.120e-001 -3.280e-001 -4.050e-001
-4.490e-001
   42.5430
                        14.12
    14.2309
                        21.36
                        63.01
  134.0584
                        80.85
    18.8482
     3.0583 10000000000.00
<Date: Tue Jul 08 07:37:32 2008</pre>
<Time Range=6 Currrent= 3.50 Stack= 5 Filter=50 Deff=
                                                                                                 6 Ampl=OFF
<Remark: FENCES
<Place: SOLOCHIANA</pre>
#GEOSEC: 0162-B / 50.0/ 50.0/ 1.0/ 563675.000/ 3916722.000/ 29.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +1.453e+001 +3.779e+001 +4.845e+001 +5.280e+001
                                                                                                             0.000/\text{rms} = 76.00
+5.138e+001 +4.818e+001 +4.505e+001 +4.116e+001 +3.692e+001 +3.382e+001
+3.155e+001 +2.925e+001 +2.725e+001 +2.605e+001 +2.532e+001 +2.475e+001 +2.445e+001 +2.446e+001 +2.463e+001 +2.501e+001 +2.568e+001 +2.642e+001 +2.717e+001 +2.824e+001 +2.963e+001 +3.085e+001 +3.191e+001 +3.318e+001
+3.451e+001 +3.538e+001 +3.585e+001 +3.597e+001 +3.531e+001 +3.406e+001
+3.257e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -7.440e-001 +1.640e-001 -2.280e-001 -3.360e-001 -3.720e-001 -3.920e-001 -3.960e-001 -3.860e-001 -3.670e-001 -3.300e-001 -2.720e-001 -2.120e-001 -1.590e-001 -9.400e-002
\begin{array}{c} -2.500 e-002 \ +2.600 e-002 \ +6.400 e-002 \ +1.060 e-001 \ +1.490 e-001 \ +1.800 e-001 \ +2.020 e-001 \ +2.210 e-001 \ +2.330 e-001 \ +2.330 e-001 \ +2.250 e-001 \ +2.050 e-001 \ +1.660 e-001 \ +1.180 e-001 \ +6.000 e-002 \ -3.300 e-002 \ -1.540 e-001 \ -2.480 e-001 \end{array}
-3.150e-001
   44.5620
                        16.19
   14.1606
56.3695
35.9988
                        18.82
                        78.32
                        82.60
     8.6291 10000000000.00
<Date: Tue Jul 08 08:00:58 2008</pre>
<Time Range=6 Currrent= 3.50 Stack= 5 Filter=50 Deff=
                                                                                                 6 Ampl=OFF
<Remark: FENCES</pre>
#GEOSEC: 0163-C / 50.0 / 50.0 / 1.0 / 563891.000 / 3916743.000 / 31.0 / 36/5 / 0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000 / S [V/A]: +0.000e+000 +0.000e+000 +1.618e+001 +2.623e+001 +3.142e+001
                                                                                                             0.000/\text{rms} = 51.00
+3.257e+001 +3.183e+001 +3.069e+001 +2.897e+001 +2.680e+001 +2.505e+001
+2.369e+001 +2.227e+001 +2.098e+001 +2.015e+001 +1.961e+001 +1.913e+001 +1.879e+001 +1.866e+001 +1.863e+001 +1.870e+001 +1.890e+001 +1.915e+001
+1.942e+001 +1.982e+001 +2.041e+001 +2.097e+001 +2.152e+001 +2.224e+001
+2.305e+001 +2.360e+001 +2.390e+001 +2.395e+001 +2.352e+001 +2.279e+001
+2.194e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.950e-001 +4.930e-001 +2.000e-003 -1.750e-001 -2.460e-001 -2.970e-001 -3.250e-001 -3.280e-001 -3.150e-001 -2.850e-001 -2.410e-001 -1.980e-001 -1.590e-001 -1.120e-001 -6.200e-002 -2.400e-002 +5.000e-003 +3.400e-002 +6.500e-002 +8.700e-002
+1.050e-001 +1.270e-001 +1.520e-001 +1.700e-001 +1.800e-001 +1.790e-001
```

```
1D_Inversion_Results_TEM.txt
+1.550e-001 +1.110e-001 +5.300e-002 -3.400e-002 -1.400e-001 -2.160e-001
-2.700e-001
  27.4450
                 15.98
  10.9199
                 12.74
  26.6164
                 52.25
  30.4677
                 78.82
    5.5463 10000000000.00
<Date: Tue Jul 08 08:26:53 2008</pre>
<Time Range=6 Currrent= 3.50 Stack= 5 Filter=50 Deff=
                                                                      6 Ampl=OFF
<Remark: FENCES
<Place: SOLOCHIANA
<
*****
#GEOSEC: 0164-C / 50.0/ 50.0/ 1.31.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                1.0/ 564102.000/ 3916749.000/
                                                          0.000 DH=
                                                                               0.000/\text{rms} = 42.00
    [V/A]: +0.000e+000 +1.041e+000 +1.691e+001 +2.371e+001 +2.608e+001
+2.550e+001 +2.437e+001 +2.341e+001 +2.235e+001 +2.136e+001 +2.071e+001
+2.027e+001 +1.987e+001 +1.955e+001 +1.936e+001 +1.923e+001 +1.907e+001
+1.889e+001 +1.874e+001 +1.861e+001 +1.848e+001 +1.838e+001 +1.835e+001 +1.839e+001 +1.850e+001 +1.873e+001 +1.897e+001 +1.921e+001 +1.951e+001
+1.985e+001 +2.008e+001 +2.022e+001 +2.028e+001 +2.016e+001 +1.984e+001
+1.940e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.350e-001 +1.970e-001 -1.710e-001 -2.350e-001 -2.350e-001 -2.160e-001 -1.840e-001 -1.540e-001 -1.250e-001 -9.400e-002 -6.600e-002 -5.100e-002 -4.600e-002 -4.600e-002
-4.600e-002 -4.600e-002 -4.300e-002 -3.400e-002 -1.600e-002 +4.000e-003 +2.300e-002 +4.600e-002 +6.900e-002 +8.200e-002 +8.700e-002 +8.600e-002 +7.500e-002 +5.700e-002 +3.400e-002 -5.000e-003 -6.400e-002 -1.250e-001
-1.800e-001
  23.6069
                 10.33
  14.6761
                  8.37
                 57.52
68.25
  18.4325
  27.4743
    9.4051 10000000000.00
<Date: Tue Jul 08 08:45:38 2008</pre>
<Time Range=6 Currrent= 3.50 Stack= 5 Filter=50 Deff=</pre>
                                                                      6 Ampl=OFF
<Remark: NEXT TO STREAM</pre>
*****
#GEOSEC: 0165-A / 50.0/ 50.0/ 1.0
33.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 564315.000/ 3916758.000/
                                                          0.000 DH =
                                                                               0.000/rms = 84.00
S [V/A]: +0.000e+000 +0.000e+000 +6.297e+000 +1.576e+001 +2.178e+001
+2.466e+001 +2.551e+001 +2.565e+001 +2.524e+001 +2.435e+001 +2.340e+001
+2.258e+001 +2.162e+001 +2.069e+001 +2.003e+001 +1.958e+001 +1.914e+001 +1.879e+001 +1.861e+001 +1.853e+001 +1.853e+001 +1.866e+001 +1.884e+001 +1.904e+001 +1.932e+001 +1.961e+001 +1.979e+001 +1.986e+001 +1.984e+001
+1.966e+001 +1.938e+001 +1.905e+001 +1.855e+001 +1.783e+001 +1.709e+001
+1.635e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.880e-001 +3.290e-001 +1.010e-001 -1.900e-002 -1.210e-001 -1.910e-001 -2.200e-001
-2.240e-001 -2.140e-001 -1.890e-001 -1.640e-001 -1.400e-001 -1.080e-001
-7.100e-002 -4.100e-002 -1.500e-002 +1.500e-002 +4.600e-002 +6.600e-002
+7.600e-002 +7.700e-002 +6.300e-002 +3.900e-002 +1.200e-002 -2.500e-002 -6.700e-002 -1.010e-001 -1.290e-001 -1.670e-001 -2.150e-001 -2.590e-001
-2.970e-001
  22.9473
                 20.27
  10.4890
                 10.22
                 38.43
47.51
  24.4436
  17.7354
   7.5761 10000000000.00
<Date: Tue Jul 08 09:01:30 2008</pre>
*****
#GEOSEC: 0166-C
                           / 50.0/ 50.0/ 1.0/ 564523.000/ 3916834.000/
```

```
1D_Inversion_Results_TEM.txt
35.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +0.000e+000 +2.371e+001 +5.254e+001 +6.833e+001 +7.716e+001
+7.781e+001 +7.509e+001 +7.203e+001 +6.807e+001 +6.349e+001 +5.993e+001
                                                                                                                 0.000/rms = 66.00
+5.716e+001 +5.419e+001 +5.141e+001 +4.954e+001 +4.824e+001 +4.693e+001
+4.574e+001 +4.495e+001 +4.437e+001 +4.372e+001 +4.297e+001 +4.230e+001 +4.162e+001 +4.061e+001 +3.914e+001 +3.768e+001 +3.624e+001 +3.429e+001 +3.182e+001 +2.966e+001 +2.774e+001 +2.532e+001 +2.242e+001 +1.993e+001
+1.778e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -7.890e-001 +3.190e-001 -8.800e-002 -2.180e-001 -2.590e-001 -2.820e-001 -2.930e-001 -2.890e-001 -2.780e-001 -2.540e-001 -2.190e-001 -1.880e-001 -1.640e-001 -1.370e-001 -1.110e-001 -9.500e-002 -8.600e-002 -8.200e-002 -8.800e-002 -1.020e-001 -1.220e-001 -1.530e-001 -1.970e-001 -2.350e-001 -2.670e-001 -3.030e-001
-3.400e-001 -3.680e-001 -3.920e-001 -4.210e-001 -4.520e-001 -4.730e-001
-4.850e-001
   70.8483
                         24.69
    22.4834
                          7.54
                         62.85
    30.7850
     6.6708
                         44.16
     1.6083 10000000000.00
<Date: Tue Jul 08 09:22:57 2008</pre>
<Time Range=6 Currrent= 3.40 Stack= 5 Filter=50 Deff=
                                                                                                     6 Ampl=OFF
<Remark: NEXT TO STREAM</pre>
*****
0.000/rms=150.00
+1.884e+001 +1.943e+001 +1.974e+001 +2.005e+001 +2.037e+001 +2.064e+001
+2.086e+001 +2.113e+001 +2.141e+001 +2.159e+001 +2.170e+001 +2.176e+001
+2.179e+001 +2.113e+001 +2.141e+001 +2.133e+001 +2.170e+001 +2.170e+001 +2.170e+001 +2.183e+001 +2.189e+001 +2.205e+001 +2.234e+001 +2.263e+001 +2.290e+001 +2.315e+001 +2.328e+001 +2.321e+001 +2.302e+001 +2.270e+001 +2.233e+001 +2.214e+001 +2.211e+001 +2.225e+001 +2.261e+001 +2.295e+001
+2.311e+001
                   +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.940e-001
Err[V/A]:
+2.880e-001 +1.280e-001 +9.100e-002 +7.800e-002 +7.400e-002 +7.200e-002 +7.000e-002 +6.700e-002 +5.500e-002 +3.900e-002 +2.500e-002 +1.200e-002 +9.000e-003 +1.600e-002 +2.900e-002 +5.100e-002 +7.100e-002 +7.800e-002 +7.200e-002 +4.700e-002 +1.000e-003 -3.900e-002 -6.600e-002 -7.900e-002 -6.400e-002 -2.900e-002 +1.000e-002 +5.600e-002 +8.400e-002 +6.500e-002
+2.700e-002
17.1228
                           3.34
    22.8637
                         49.02
                         19.79
    29.4356
   19.1770 10000000000.00
<Date: Tue Jul 08 09:42:08 2008</pre>
<Time Range=6 Currrent= 3.30 Stack= 5 Filter=50 Deff=
                                                                                                     6 Ampl=OFF
<Remark: NEXT TO STREAM
*****
                                          50.0/ 50.0/ 1.0/ 564988.000/ 3916967.000/
38.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                   0.000 DH=
                                                                                                                 0.000/rms=135.00
S [V/A]: +0.000e+000 +0.000e+000 +1.603e+000 +1.305e+001 +2.032e+001 +2.332e+001 +2.423e+001 +2.462e+001 +2.492e+001 +2.516e+001 +2.533e+001 +2.547e+001 +2.569e+001 +2.596e+001 +2.619e+001 +2.639e+001 +2.658e+001
+2.676e+001 +2.685e+001 +2.690e+001 +2.692e+001 +2.687e+001 +2.676e+001 +2.659e+001 +2.630e+001 +2.583e+001 +2.536e+001 +2.491e+001 +2.433e+001 +2.367e+001 +2.316e+001 +2.276e+001 +2.233e+001 +2.187e+001 +2.141e+001
+2.083e+001
Err[V/A]:
                   +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.620e-001
+3.640e-001 +1.470e-001 +8.400e-002 +5.500e-002 +4.100e-002 +3.700e-002 +4.100e-002 +4.800e-002 +5.100e-002 +4.600e-002 +3.700e-002 +2.600e-002 +1.700e-002 +9.000e-003 -2.000e-003 -1.800e-002 -3.500e-002 -5.200e-002 -7.400e-002 -9.800e-002 -1.150e-001 -1.250e-001 -1.310e-001 -1.300e-001 -1.220e-001 -1.130e-001 -1.040e-001 -1.150e-001 -1.560e-001
-2.070e-001
```

```
1D_Inversion_Results_TEM.txt
  13.5029
                  1.00
  27.4264
                 60.11
  19.6913
                 30.29
  15.7386
                 38.92
  17.4045 10000000000.00
<Date: Tue Jul 08 10:08:58 2008</pre>
<Time Range=6 Currrent= 3.10 Stack= 5 Filter=50 Deff= <Remark: NEXT TO STREAM
                                                                      6 Ampl=OFF
<Place: ACHLADES
#GEOSEC: 0169-B / 50.0/ 50.0/ 1 40.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 565171.000/ 3917046.000/
                                                           0.000 DH =
                                                                              0.000/rms=465.00
S [V/A]: +0.000e+000 +0.000e+000 +8.577e+000 +2.197e+001 +2.792e+001
+2.830e+001 +2.756e+001 +2.716e+001 +2.715e+001 +2.755e+001 +2.807e+001 +2.856e+001 +2.918e+001 +2.988e+001 +3.050e+001 +3.106e+001 +3.177e+001
+3.246e+001 +3.277e+001 +3.278e+001 +3.247e+001 +3.186e+001 +3.136e+001
+3.103e+001 +3.080e+001 +3.070e+001 +3.066e+001 +3.055e+001 +3.028e+001
+2.978e+001 +2.924e+001 +2.874e+001 +2.811e+001 +2.739e+001 +2.680e+001
+2.627e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +5.690e-001 -5.100e-002 -1.130e-001 -5.200e-002 +3.000e-002 +8.800e-002 +1.100e-001
Err[V/A]:
+1.150e-001 +1.150e-001 +1.150e-001 +1.210e-001 +1.240e-001 +1.150e-001 +7.800e-002 +2.700e-002 -2.300e-002 -7.100e-002 -9.200e-002 -8.200e-002 -5.900e-002 -2.900e-002 -1.200e-002 -1.800e-002 -3.600e-002 -6.500e-002
-9.500e-002 -1.120e-001 -1.200e-001 -1.240e-001 -1.270e-001 -1.320e-001
-1.390e-001
  27.1867
34.2490
                 11.04
                 52.97
  34.2490
                  1.01
                200.00
  24.1841
  50.0000 10000000000.00
<Date: Tue Jul 08 10:32:54 2008
<Time Range=6 Currrent= 2.50 Stack= 5 Filter=50 Deff=
<Remark: NEXT TO STREAM</pre>
                                                                      6 Ampl=OFF
<Place: ACHLADES
<****************************
                                               1.0/ 563251.000/ 3916812.000/
#GEOSEC: 0170-B
                            50.0/ 50.0/
29.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          0.000 DH =
                                                                              0.000/\text{rms}=186.00
             +0.000e+000 +6.281e+000 +2.989e+001 +4.094e+001 +4.506e+001
+4.260e+001 +3.856e+001 +3.496e+001 +3.098e+001 +2.715e+001 +2.459e+001 +2.284e+001 +2.115e+001 +1.975e+001 +1.895e+001 +1.851e+001 +1.823e+001
+1.825e+001 +1.854e+001 +1.899e+001 +1.981e+001 +2.115e+001 +2.262e+001 +2.415e+001 +2.631e+001 +2.905e+001 +3.116e+001 +3.259e+001 +3.350e+001
+3.317e+001 +3.196e+001 +3.050e+001 +2.847e+001 +2.601e+001 +2.397e+001
+2.220e+001
             -9.000e-001 -9.000e-001 -9.000e-001 -8.180e-001 +1.310e-001
Err[V/A]:
-3.450e-001 -4.300e-001 -4.460e-001 -4.440e-001 -4.300e-001 -4.070e-001
-3.770e-001 -3.290e-001 -2.580e-001 -1.880e-001 -1.240e-001 -4.200e-002
+5.200e-002 +1.300e-001 +1.950e-001 +2.690e-001 +3.480e-001 +4.020e-001 +4.350e-001 +4.500e-001 +4.200e-001 +3.460e-001 +2.360e-001 +6.100e-002
-1.390e-001 -2.560e-001 -3.140e-001 -3.530e-001 -3.800e-001 -4.020e-001
-4.210e-001
 100.0000
  13.6908
                 28.51
 200,0000
                 60.16
 100.0000
                 34.46
    3.0000 10000000000.00
<Date: Tue Jul 08 11:52:14 2008</pre>
<Time Range=6 Currrent= 2.20 Stack= 5 Filter=50 Deff= <Remark: NEXT TO THE MAIN ROAD
                                                                      6 Ampl=OFF
*****
#GEOSEC: 0171-A / 50.0/ 50.0/ 1.0/ 561260.000/ 3914381.000/ 91.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                              0.000/\text{rms}=116.00
S [V/A]: +0.000e+000 +0.000e+000 +7.620e+000 +2.287e+001 +3.244e+001
                                           Σελίδα 60
```

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1D_Inversion_Results_TEM.txt
+3.612e+001 +3.677e+001 +3.684e+001 +3.674e+001 +3.655e+001 +3.639e+001 +3.623e+001 +3.608e+001 +3.594e+001 +3.588e+001 +3.586e+001 +3.593e+001 +3.604e+001 +3.618e+001 +3.639e+001 +3.660e+001 +3.658e+001
+3.633e+001 +3.562e+001 +3.428e+001 +3.291e+001 +3.169e+001 +3.028e+001
+2.892e+001 +2.803e+001 +2.739e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +7.980e-001 +2.550e-001 +5.000e-002 +1.000e-015 -1.900e-002 -2.400e-002 -2.700e-002 -2.100e-002 -1.300e-002 -7.000e-003 +5.000e-003 +5.000e-003 +1.300e-002 +2.200e-002 +2.900e-002 +3.000e-002 +1.100e-002 -2.700e-002 -7.600e-002 -1.430e-001 -2.380e-001 -2.430e-001 -2.290e-001
-1.960e-001 -1.660e-001 -1.430e-001
   36.1625
                    28.75
                    79.26
   33.8426
    6.1294
                    12.09
    6.1294
                     1.27
   27.4107 10000000000.00
<Date: Tue Jul 08 12:35:39 2008</pre>
<Time Range=5 Currrent= 2.60 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark: IN VILLAGE, POWERLINES, FENCES</pre>
<Place: ALEXANDROU HANI
*****
#GEOSEC: 0172-A / 50.0/ 50.0/ 1 94.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                         1.0/ 561519.000/ 3914280.000/
                                                                     0.000 DH=
                                                                                            0.000/\text{rms}=163.00
    [V/A]: +6.999e+001 +4.803e+001 +3.778e+001 +3.229e+001 +2.829e+001
+2.595e+001 +2.510e+001 +2.493e+001 +2.517e+001 +2.589e+001 +2.673e+001
+2.758e+001 +2.871e+001 +3.006e+001 +3.119e+001 +3.211e+001 +3.320e+001
+3.438e+001 +3.529e+001 +3.598e+001 +3.672e+001 +3.733e+001 +3.758e+001 +3.758e+001 +3.529e+001 +3.663e+001 +3.593e+001 +3.529e+001 +3.453e+001
+3.364e+001 +3.275e+001 +3.169e+001
Err[V/A]: +5.000e-001 +5.000e-001 +4.960e-001 +4.780e-001 -4.050e-001 -2.480e-001 -1.030e-001 -1.000e-003 +8.700e-002 +1.570e-001 +1.940e-001 +2.100e-001 +2.160e-001 +2.120e-001 +2.020e-001 +1.910e-001 +1.770e-001 +1.580e-001 +1.410e-001 +1.240e-001 +9.800e-002 +5.800e-002 +1.800e-002
-2.000e-002 -6.400e-002 -1.010e-001 -1.170e-001 -1.210e-001 -1.240e-001
-1.420e-001 -1.890e-001 -2.420e-001
 100.0000
                     1.23
   24.6281
                    18.05
   58.9224
                    45.82
   24.6543 10000000000.00
<Date: Tue Jul 08 13:01:35 2008
<Time Range=5 Currrent= 2.20 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark: IN VILLAGE, POWERLINES, FENCES</pre>
<Place: ALEXANDROU HANI
<***********************************
******
#GEOSEC: 0173-B / 50.0 / 50.0 / 186.0 / 36/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                          1.0/ 561729.000/ 3914500.000/
                                                                     0.000 DH=
                                                                                            0.000/rms=136.00
               +0.000e+000 +9.008e+000 +1.408e+001 +1.643e+001 +1.798e+001
+1.885e+001 +1.919e+001 +1.927e+001 +1.927e+001 +1.925e+001 +1.930e+001
+1.948e+001 +1.982e+001 +2.039e+001 +2.094e+001 +2.144e+001 +2.201e+001
+2.264e+001 +2.313e+001 +2.353e+001 +2.398e+001 +2.436e+001 +2.447e+001
+2.437e+001 +2.398e+001 +2.325e+001 +2.252e+001 +2.186e+001 +2.105e+001
+2.014e+001 +1.938e+001 +1.871e+001 +1.786e+001 +1.685e+001 +1.602e+001
+1.536e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.650e-001 -5.940e-001 +3.180e-001 +1.440e-001 +5.700e-002 +1.400e-002 -2.000e-003 +6.000e-003 +4.000e-002
+7.600e-002 +1.140e-001 +1.450e-001 +1.550e-001 +1.520e-001 +1.410e-001 +1.290e-001 +1.210e-001 +1.130e-001 +9.200e-002 +4.900e-002 -3.000e-003 -5.600e-002 -1.160e-001 -1.670e-001 -1.910e-001 -2.010e-001 -2.060e-001 -2.120e-001 -2.230e-001 -2.360e-001 -2.550e-001 -2.710e-001
-2.660e-001
   19.8087
29.3506
11.7119
                    18.91
45.56
                    32.65
    9.1915
                   194.16
    1.0000 10000000000.00
<Date: Mon Jul 14 08:00:45 2008</pre>
```

```
1D_Inversion_Results_TEM.txt
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NE OF THE VILLAGE</pre>
<Place: ALEXANDROU HANI</pre>
#GEOSEC: 0174-B / 50.0 / 50.0 / 1.0 / 91.0 / 36 / 4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 562007.000/ 3914478.000/
                                                                0.000 DH =
                                                                                       0.000/\text{rms}=153.00
S [V/A]:
              +5.649e+000 +3.335e+000 +3.527e+000 +4.354e+000 +5.635e+000
+6.994e+000 +7.840e+000 +8.349e+000 +8.774e+000 +9.128e+000 +9.398e+000
+9.642e+000 +9.960e+000 +1.036e+001 +1.072e+001 +1.103e+001 +1.143e+001 +1.191e+001 +1.235e+001 +1.275e+001 +1.330e+001 +1.401e+001 +1.466e+001 +1.524e+001 +1.594e+001 +1.667e+001 +1.712e+001 +1.740e+001 +1.762e+001
+1.783e+001 +1.806e+001 +1.834e+001 +1.878e+001 +1.933e+001 +1.962e+001
+1.956e+001
Err[V/A]: +5.000e-001 +4.660e-001 -6.550e-001 -8.270e-001 +7.940e-001 +6.400e-001 +4.590e-001 +3.250e-001 +2.210e-001 +1.710e-001 +1.660e-001
+1.720e-001 +1.810e-001 +1.890e-001 +1.920e-001 +1.950e-001 +1.960e-001
+2.030e-001 +2.120e-001 +2.230e-001 +2.400e-001 +2.560e-001 +2.620e-001 +2.570e-001 +2.320e-001 +1.830e-001 +1.330e-001 +9.400e-002 +6.600e-002 +6.700e-002 +9.100e-002 +1.180e-001 +1.370e-001 +1.120e-001 +2.900e-002
-7.200e-002
   10.2320
                   15.13
   23.9993
                   50.09
   23.9993
                   11.86
   21.3294 10000000000.00
<Date: Mon Jul 14 08:41:01 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NE OF THE VILLAGE
<Place: ALEXANDROU HANI</pre>
<**************************
*****
#GEOSEC: 0175-B / 50.0/ 50.0/ 1.
85.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 562207.000/ 3914480.000/
                                                               0.000 DH =
                                                                                       0.000/\text{rms}=169.00
    [V/A]: +0.000e+000 +0.000e+000 +6.014e+000 +1.652e+001 +2.315e+001
+2.631e+001 +2.749e+001 +2.801e+001 +2.827e+001 +2.817e+001 +2.784e+001
+2.748e+001 +2.699e+001 +2.650e+001 +2.620e+001 +2.608e+001 +2.610e+001
+2.639e+001 +2.684e+001 +2.739e+001 +2.822e+001 +2.933e+001 +3.031e+001 +3.113e+001 +3.206e+001 +3.297e+001 +3.356e+001 +3.395e+001 +3.428e+001
+3.443e+001 +3.435e+001 +3.415e+001 +3.379e+001 +3.334e+001 +3.305e+001
+3.295e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.010e-001 +3.610e-001 +1.700e-001 +8.700e-002 +1.700e-002 -7.600e-002 -9.200e-002 -9.200e-002 -7.500e-002 -4.800e-002 -1.600e-002 +2.700e-002
+7.900e-002 +1.200e-001 +1.500e-001 +1.760e-001 +1.870e-001 +1.740e-001 +1.510e-001 +1.190e-001 +9.200e-002 +6.900e-002 +3.900e-002 +2.000e-003 -2.800e-002 -4.900e-002 -6.300e-002 -5.900e-002 -3.500e-002
-5.000e-003
   27.2187
                   41.08
   27.2187
                   13.00
   98.1146
                   44.94
   26.3273 10000000000.00
<Date: Mon Jul 14 09:07:00 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: EAST OF THE VILLAGE</pre>
<Place: ALEXANDROU HANI</pre>
*****
#GEOSEC: 0176-B / 50.0/ 50.0/ 1.0/ 562474.000/ 3914521.000/ 81.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/6 S [V/A]: +0.000e+000 +0.000e+000 +5.793e+000 +1.825e+001 +2.508e+001
                                                                                       0.000/rms = 76.00
+2.690e+001 +2.676e+001 +2.630e+001 +2.565e+001 +2.483e+001 +2.409e+001
+2.345e+001 +2.269e+001 +2.192e+001 +2.143e+001 +2.117e+001 +2.106e+001
+2.121e+001 +2.152e+001 +2.187e+001 +2.226e+001 +2.240e+001 +2.205e+001 +2.135e+001 +2.003e+001 +1.811e+001 +1.643e+001 +1.503e+001 +1.341e+001 +1.177e+001 +1.061e+001 +9.784e+000 +8.976e+000 +8.318e+000 +7.990e+000
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.420e-001
Err[V/A]:
+1.210e-001 -7.200e-002 -1.190e-001 -1.380e-001 -1.570e-001 -1.700e-001
                                                Σελίδα 62
```

```
1D_Inversion_Results_TEM.txt
-1.740e-001 -1.680e-001 -1.420e-001 -1.020e-001 -5.900e-002 +1.000e-015 +6.300e-002 +9.800e-002 +1.040e-001 +6.700e-002 -3.600e-002 -1.590e-001 -2.630e-001 -3.560e-001 -4.140e-001 -4.370e-001 -4.460e-001 -4.490e-001
-4.450e-001 -4.320e-001 -4.110e-001 -3.640e-001 -2.740e-001 -1.640e-001
-5.000e-002
  24.3363
                 17.20
                 24.14
  14.6635
 148.4346
                 18.11
    2.7590
                 42.94
 100.0000 10000000000.00
<Date: Mon Jul 14 09:35:24 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: SOUTH OF G-59
50.0/
                                                 1.0/ 562888.000/ 3914506.000/
#GEOSEC: 0177-C
                                       50.0/
64.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                               0.000/rms=111.00
                                                           0.000 DH =
S [V/A]: +1.381e+001 +9.602e+000 +8.966e+000 +9.363e+000 +1.032e+001 +1.145e+001 +1.219e+001 +1.265e+001 +1.307e+001 +1.347e+001 +1.382e+001
+1.419e+001 +1.473e+001 +1.547e+001 +1.618e+001 +1.684e+001 +1.769e+001
+1.874e+001 +1.966e+001 +2.050e+001 +2.157e+001 +2.284e+001 +2.388e+001
+2.470e+001 +2.560e+001 +2.644e+001 +2.699e+001 +2.738e+001 +2.783e+001
+2.835e+001 +2.883e+001 +2.929e+001 +2.992e+001 +3.068e+001 +3.131e+001
+3.180e+001
Err[V/A]:
             +5.000e-001 +4.770e-001 +1.200e-002 -3.380e-001 +4.340e-001
+3.680e-001 +2.730e-001 +2.030e-001 +1.550e-001 +1.430e-001 +1.590e-001
+1.850e-001 +2.150e-001 +2.430e-001 +2.590e-001 +2.660e-001 +2.700e-001 +2.740e-001 +2.760e-001 +2.780e-001 +2.760e-001 +2.630e-001 +2.420e-001
+2.160e-001 +1.790e-001 +1.370e-001 +1.100e-001 +9.600e-002 +9.100e-002
+9.500e-002 +1.050e-001 +1.140e-001 +1.210e-001 +1.210e-001 +1.130e-001
+1.040e-001
  14.6213
14.6213
                 15.19
                  1.00
  39.1775
                 19.13
  45.6013
                 17.32
  34.7968 10000000000.00
<Date: Mon Jul 14 10:07:38 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: WEST OF PERAMA</pre>
*****
#GEOSEC: 0178-B / 50.0/ 50.0/ 1.
65.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         563284.000/ 3914741.000/
                                                 1.0/
                                                           0.000 DH =
                                                                               0.000/rms=130.00
S [V/A]: +0.000e+000 +0.000e+000 +2.770e-001 +8.229e+000 +1.406e+001 +1.691e+001 +1.782e+001 +1.816e+001 +1.829e+001 +1.836e+001 +1.847e+001
+1.862e+001 +1.892e+001 +1.940e+001 +1.990e+001 +2.034e+001 +2.093e+001
+2.159e+001 +2.214e+001 +2.259e+001 +2.315e+001 +2.384e+001 +2.446e+001 +2.504e+001 +2.580e+001 +2.672e+001 +2.745e+001 +2.806e+001 +2.877e+001 +2.961e+001 +3.038e+001 +3.110e+001 +3.199e+001 +3.276e+001 +3.271e+001
+3.181e+001
Err[V/A]:
             +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.900e-001
+4.740e-001 +1.910e-001 +8.300e-002 +2.800e-002 +2.600e-002 +4.400e-002 +6.900e-002 +1.020e-001 +1.330e-001 +1.480e-001 +1.530e-001 +1.530e-001 +1.470e-001 +1.410e-001 +1.380e-001 +1.390e-001 +1.470e-001 +1.560e-001
+1.630e-001 +1.680e-001 +1.640e-001 +1.540e-001 +1.460e-001 +1.410e-001
+1.460e-001 +1.560e-001 +1.600e-001 +1.390e-001 +4.800e-002 -1.070e-001
-2.580e-001
  18.7173
                 17.49
  30.7835
                 62.32
  48.1645
                 41.84
                 90.09
  14.7350
    1.0000 10000000000.00
<Date: Mon Jul 14 10:37:39 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: NW OF PERAMA</pre>
<Place: PERAMA
```

```
1D_Inversion_Results_TEM.txt
_************
                                                                     .
**********
*****
#GEOSEC: 0179-C / 50.0/ 50.0/ 1
48.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          1.0/ 563669.000/ 3914610.000/
                                                                      0.000 DH=
                                                                                              0.000/rms=183.00
    [V/A]: +1.288e+001 +2.199e+001 +2.715e+001 +2.960e+001 +3.050e+001
+2.958e+001 +2.802e+001 +2.661e+001 +2.510e+001 +2.387e+001 +2.327e+001 +2.304e+001 +2.308e+001 +2.348e+001 +2.402e+001 +2.460e+001 +2.536e+001
+2.623e+001 +2.687e+001 +2.735e+001 +2.783e+001 +2.829e+001 +2.862e+001
+2.890e+001 +2.925e+001 +2.969e+001 +3.007e+001 +3.039e+001 +3.073e+001
+3.098e+001 +3.098e+001 +3.073e+001
Err[V/A]: -9.000e-001 -8.640e-001 -6.220e-001 -3.240e-001 +1.400e-002 -2.090e-001 -2.820e-001 -2.880e-001 -2.530e-001 -1.770e-001 -1.010e-001
-3.200e-002 +4.300e-002 +1.080e-001 +1.470e-001 +1.640e-001 +1.660e-001
+1.500e-001 +1.290e-001 +1.100e-001 +8.900e-002 +7.400e-002 +6.800e-002 +6.700e-002 +7.000e-002 +7.400e-002 +7.300e-002 +5.200e-002 +1.900e-002 -3.000e-002 -8.200e-002
   30.5814
                      7.33
   19.9994
                     13.05
   19.9994
35.9659
                      1.00
                   190.84
   50.0000 10000000000.00
<Date: Mon Jul 14 11:17:45 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: NORTH OF PERAMA
<Place: PERAMA</pre>
#GEOSEC: 0180-A / 50.0/ 50.0/ 1.0/ 563970.000/ 3914510.000/ 50.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +4.549e+001 +4.575e+001 +4.569e+001 +4.497e+001 +4.308e+001
                                                                                              0.000/\text{rms} = 88.00
+4.017e+001 +3.767e+001 +3.575e+001 +3.386e+001 +3.221e+001 +3.117e+001 +3.039e+001 +2.944e+001 +2.827e+001 +2.720e+001 +2.623e+001 +2.499e+001 +2.353e+001 +2.230e+001 +2.124e+001 +1.993e+001 +1.842e+001 +1.718e+001 +1.617e+001 +1.500e+001 +1.378e+001 +1.292e+001 +1.228e+001 +1.162e+001
+1.102e+001 +1.064e+001 +1.038e+001
Err[V/A]:
                -3.700e-002 -6.000e-003 +5.200e-002 +1.420e-001 -2.370e-001
-2.930e-001 -3.020e-001 -2.830e-001 -2.440e-001 -1.970e-001 -1.700e-001 -1.650e-001 -1.770e-001 -2.010e-001 -2.230e-001 -2.410e-001 -2.590e-001
-2.780e-001 -2.930e-001 -3.070e-001 -3.250e-001 -3.420e-001 -3.530e-001
-3.570e-001 -3.550e-001 -3.420e-001 -3.230e-001 -3.000e-001 -2.650e-001 -2.200e-001 -1.820e-001 -1.500e-001
   36.6340
                     12.90
                    12.24
   16.6683
   16.0701
                      6.23
   16.0701
                      6.23
    5.8824 10000000000.00
<Date: Mon Jul 14 11:55:40 2008
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: FENCES,BETWEEN RIVER-MAIN ROAD</pre>
<Place: PERAMA
*****
                                   50.0/ 50.0/
                                                          1.0/ 563855.000/ 3915893.000/
69.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +0.000e+000 +3.014e+001 +6.374e+001 +8.726e+001 +1.078e+002 +1.211e+002 +1.277e+002 +1.327e+002 +1.391e+002 +1.463e+002 +1.509e+002 +1.528e+002 +1.517e+002 +1.458e+002 +1.379e+002 +1.298e+002 +1.190e+002
                                                                                              0.000/rms=123.00
+1.062e+002 +9.603e+001 +8.782e+001 +7.856e+001 +6.903e+001 +6.208e+001 +5.681e+001 +5.114e+001 +4.552e+001 +4.158e+001 +3.854e+001 +3.512e+001 +3.140e+001 +2.835e+001 +2.569e+001
Err[V/A]:
               -9.000e-001 -9.000e-001 -9.000e-001 -8.650e-001 +6.550e-001
+3.650e-001 +2.550e-001 +2.400e-001 +2.380e-001 +1.990e-001 +1.220e-001
+2.600e-002 -1.070e-001 -2.430e-001 -3.250e-001 -3.700e-001 -4.040e-001 -4.270e-001 -4.380e-001 -4.430e-001 -4.450e-001 -4.450e-001 -4.420e-001 -4.380e-001 -4.300e-001 -4.200e-001 -4.120e-001 -4.090e-001 -4.130e-001
```

-4.300e-001 -4.510e-001 -4.670e-001

3.76

59.13

53.0341

167.4669

```
1D_Inversion_Results_TEM.txt
   16.0578
                   25.63
   16.0578
                     1.27
    9.0174 10000000000.00
<Date: Mon Jul 14 12:59:42 2008</pre>
<Time Range=5 Currrent= 1.90 Stack= 5 Filter=50 Deff=
                                                                              6 Ampl=OFF
<Remark: IN OLIVE TREES</pre>
<Place: SOLOCHIANA
*****
#GEOSEC: 0182-A / 50.0 / 50.0 / 1.68.0 / 32/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                       1.0/ 563702.000/ 3915971.000/
                                                                 0.000 DH =
                                                                                        0.000/\text{rms}=252.00
S [V/A]: +0.000e+000 +2.204e+001 +5.626e+001 +8.273e+001 +1.117e+002 +1.375e+002 +1.515e+002 +1.588e+002 +1.634e+002 +1.643e+002 +1.616e+002
+1.565e+002 +1.474e+002 +1.344e+002 +1.230e+002 +1.140e+002 +1.041e+002 +9.433e+001 +8.726e+001 +8.169e+001 +7.522e+001 +6.816e+001 +6.265e+001 +5.825e+001 +5.332e+001 +4.821e+001 +4.449e+001 +4.152e+001 +3.810e+001
+3.427e+001 +3.107e+001 +2.826e+001
               -9.000e-001 -9.000e-001 -9.000e-001 -8.940e-001 +8.190e-001
Err[V/A]:
+5.990e-001 +3.780e-001 +2.280e-001 +9.300e-002 -4.200e-002 -1.540e-001 -2.460e-001 -3.320e-001 -3.870e-001 -4.040e-001 -4.030e-001 -3.940e-001 -3.800e-001 -3.750e-001 -3.760e-001 -3.840e-001 -3.930e-001 -3.970e-001
-3.980e-001 -3.950e-001 -3.900e-001 -3.870e-001 -3.890e-001 -3.980e-001
-4.200e-001 -4.440e-001 -4.620e-001
   48.8670
                     3.51
                   52.05
 200.0000
   18.7544
                   23.36
   26.8429
                   21.12
    9.1065 10000000000.00
<Date: Mon Jul 14 13:29:42 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
*****
#GEOSEC: 0183-A / 50.0/ 50.0/ 1.79.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 563517.000/ 3915845.000/
                                                                0.000 DH =
                                                                                        0.000/\text{rms}=492.00
S [V/A]: +0.000e+000 +4.090e-001 +1.868e+001 +3.460e+001 +5.376e+001 +7.853e+001 +1.027e+002 +1.258e+002 +1.560e+002 +1.905e+002 +2.162e+002 +2.339e+002 +2.467e+002 +2.455e+002 +2.320e+002 +2.152e+002 +1.926e+002
+1.684e+002 +1.513e+002 +1.388e+002 +1.254e+002 +1.117e+002 +1.010e+002 +9.206e+001 +8.160e+001 +7.059e+001 +6.292e+001 +5.740e+001 +5.205e+001
+4.774e+001 +4.559e+001 +4.475e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -8.950e-001
Err[V/A]:
-8.740e-001 -8.520e-001 -8.250e-001 +7.700e-001 +6.690e-001 +5.460e-001
+3.970e-001 +1.430e-001 -1.820e-001 -3.590e-001 -4.220e-001 -4.470e-001 -4.480e-001 -4.440e-001 -4.310e-001 -4.250e-001 -4.300e-001 -4.420e-001 -4.530e-001 -4.620e-001 -4.540e-001 -4.360e-001 -3.940e-001
-3.050e-001 -1.880e-001 -6.300e-002
   67.8693
                    6.56
                   77.27
 300.0000
   51.7197
                    6.11
   51.7197
                     1.00
   16.3390 10000000000.00
<Date: Mon Jul 14 13:58:05 2008
<Time Range=5 Currrent= 3.50 Stack= 5 Filter=50 Deff=
<Remark: ON THE CROSSROAD TO ACHLADES</pre>
                                                                              6 Ampl=OFF
<Place: SOLOCHIANA
*****
                                 50.0/ 50.0/
#GEOSEC: 0184-A
                                                      1.0/ 563303.000/ 3915903.000/
72.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                 0.000 DH=
                                                                                        0.000/rms=154.00
              +1.813e+000 +9.454e+000 +1.503e+001 +1.858e+001 +2.148e+001
+2.352e+001 +2.475e+001 +2.583e+001 +2.740e+001 +2.985e+001 +3.251e+001 +3.525e+001 +3.919e+001 +4.440e+001 +4.909e+001 +5.309e+001 +5.779e+001 +6.258e+001 +6.577e+001 +6.780e+001 +6.934e+001 +6.982e+001 +6.921e+001
+6.798e+001 +6.562e+001 +6.176e+001 +5.788e+001 +5.425e+001 +4.981e+001
+4.523e+001 +4.218e+001 +4.026e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.850e-001 -7.510e-001 +5.080e-001
                                                Σελίδα 65
```

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1D_Inversion_Results_TEM.txt
+3.150e-001 +2.660e-001 +2.820e-001 +3.370e-001 +4.160e-001 +4.730e-001 +5.080e-001 +5.300e-001 +5.290e-001 +5.050e-001 +4.680e-001 +4.080e-001 +3.220e-001 +2.420e-001 +1.700e-001 +8.300e-002 -1.300e-002 -9.000e-002
-1.540e-001 -2.300e-001 -3.080e-001 -3.550e-001 -3.800e-001 -3.870e-001
-3.670e-001 -3.210e-001 -2.610e-001
                  15.69
67.14
 27.2866
300.0000
  19.1618
                   15.45
   39.3421
                   33.39
   16.9411 1000000000.00
<Date: Mon Jul 14 14:32:09 2008</pre>
<Time Range=5 Currrent= 3.20 Stack= 5 Filter=50 Deff=</pre>
                                                                            6 Ampl=OFF
<Remark: ON THE CROSSROAD TO ACHLADES</pre>
<Place: SOLOCHIANA
</pre>
*****
                                50.0/ 50.0/
                                                   1.0/ 563096.000/ 3915864.000/
#GEOSEC: 0185-C
47.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                     0.000/\text{rms}=417.00
                                                               0.000 \, DH =
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +4.649e+000 +1.435e+001 +2.266e+001 +2.850e+001 +3.336e+001 +3.951e+001 +4.721e+001 +5.411e+001 +6.026e+001 +6.773e+001 +7.539e+001 +8.029e+001 +8.303e+001 +8.469e+001
+8.472e+001 +8.367e+001 +8.224e+001 +7.996e+001 +7.668e+001 +7.353e+001
+7.064e+001 +6.708e+001 +6.316e+001 +6.024e+001 +5.789e+001 +5.501e+001
+5.136e+001 +4.787e+001 +4.456e+001 +4.031e+001 +3.551e+001 +3.194e+001
+2.929e+001
Err[V/A]:
              -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001
+8.770e-001 +7.930e-001 +7.380e-001 +6.960e-001 +6.610e-001 +6.300e-001
+5.940e-001 +5.240e-001 +4.070e-001 +2.820e-001 +1.740e-001 +5.900e-002 -3.900e-002 -9.600e-002 -1.340e-001 -1.740e-001 -2.160e-001 -2.460e-001 -2.620e-001 -2.620e-001 -2.630e-001 -2.630e-001 -2.630e-001 -2.630e-001
-3.310e-001 -3.770e-001 -4.100e-001 -4.350e-001 -4.450e-001 -4.410e-001
-4.320e-001
   24.9026
 300.0000
                   59.92
   24.8929
                   41.75
   26.4917
                   52.89
    5.3639 10000000000.00
<Date: Mon Jul 14 15:03:46 2008
<Time Range=6 Currrent= 2.80 Stack= 5 Filter=50 Deff=</pre>
                                                                            6 Ampl=OFF
<Remark: ON THE CROSSROAD TO ACHLADES</pre>
*****
                                                   1.0/ 562931.000/ 3915895.000/
#GEOSEC: 0186-B / 50.0/ 50.0/ 1.
39.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                              0.000 DH =
                                                                                     0.000/\text{rms}=224.00
S [V/A]: +0.000e+000 +0.000e+000 +1.034e+001 +1.685e+001 +2.180e+001 +2.580e+001 +2.872e+001 +3.127e+001 +3.461e+001 +3.891e+001 +4.289e+001
+4.660e+001 +5.143e+001 +5.705e+001 +6.149e+001 +6.482e+001 +6.819e+001
+7.113e+001 +7.289e+001 +7.392e+001 +7.443e+001 +7.347e+001 +7.104e+001 +6.787e+001 +6.308e+001 +5.719e+001 +5.264e+001 +4.901e+001 +4.483e+001 +4.013e+001 +3.618e+001 +3.276e+001 +2.865e+001 +2.425e+001 +2.106e+001
+1.872e+001
              +5.000e-001 -9.000e-001 -9.000e-001 -8.980e-001 +7.600e-001
Err[V/A]:
+5.680e-001 +5.050e-001 +4.930e-001 +4.930e-001 +4.990e-001 +5.020e-001 +4.990e-001 +4.780e-001 +4.310e-001 +3.730e-001 +3.140e-001 +2.420e-001 +1.690e-001 +1.170e-001 +7.000e-002 -9.000e-003 -1.340e-001 -2.440e-001
-3.170e-001 -3.680e-001 -3.910e-001 -3.950e-001 -3.970e-001 -4.070e-001
-4.310e-001 -4.520e-001 -4.680e-001 -4.790e-001 -4.840e-001 -4.830e-001
-4.810e-001
   29.8322
                   13.76
 242.3667
                   58.34
   13.0362
                    3.05
                   49.63
   17.4707
    2.9441 10000000000.00
<Date: Mon Jul 14 15:36:59 2008</pre>
<Time Range=6 Currrent= 2.60 Stack= 5 Filter=50 Deff=</pre>
                                                                            6 Ampl=OFF
<Remark: NEAR THE GREEN-HOUSE</pre>
<Place: AGGELIANA
```

```
1D_Inversion_Results_TEM.txt
_************
                                                                                                         .
**********
*****
#GEOSEC: 0187-B / 50.0/ 50.0/ 1 41.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                         1.0/ 562672.000/ 3915904.000/
                                                                                                           0.000 DH=
                                                                                                                                               0.000/rms=387.00
S [V/A]: +0.000e+000 +0.000e+000 +2.546e+001 +4.969e+001 +7.125e+001 +8.695e+001 +9.524e+001 +1.005e+002 +1.053e+002 +1.087e+002 +1.097e+002 +1.091e+002 +1.078e+002 +1.061e+002 +1.041e+002 +1.004e+002
+9.456e+001 +8.846e+001 +8.254e+001 +7.464e+001 +6.511e+001 +5.725e+001
+5.083e+001 +4.355e+001 +3.607e+001 +3.075e+001 +2.670e+001 +2.236e+001
+1.814e+001 +1.520e+001 +1.306e+001 +1.085e+001 +8.765e+000 +7.349e+000
+6.323e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.480e-001 +5.770e-001 +3.860e-001 +2.890e-001 +1.980e-001 +9.500e-002 +2.500e-002
-1.500e-002 -4.400e-002 -7.400e-002 -1.110e-001 -1.580e-001 -2.280e-001 -3.080e-001 -3.650e-001 -4.050e-001 -4.410e-001 -4.670e-001 -4.790e-001 -4.850e-001 -4.900e-001 -4.920e-001 -4.940e-001 -4.950e-001 -4.960e-001
-4.970e-001 +4.970e-001 -4.970e-001 +4.970e-001 +4.970e-001 +4.970e-001
+4.970e-001
  23.5550
139.1313
                               2.03
47.79
     21.3224
                               28.39
       3.0000
                               43.89
  100.0000 10000000000.00
<Date: Mon Jul 14 16:03:32 2008
<Time Range=6 Currrent= 2.40 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                               6 Ampl=OFF
<Remark: IN OLIVE TREES, NOT SQUARE</pre>
<Place: AGGELIANA
 <
#GEOSEC: 0188-B / 50.0 / 50.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0 / 160.0
                                                                                         1.0/ 562534.000/ 3915853.000/
                                                                                                           0.000 DH =
                                                                                                                                               0.000/\text{rms}=498.00
                       +0.000e+000 +0.000e+000 +0.000e+000 +1.182e+001 +2.442e+001
+3.594e+001 +4.526e+001 +5.398e+001 +6.607e+001 +8.178e+001 +9.523e+001 +1.059e+002 +1.166e+002 +1.250e+002 +1.293e+002 +1.313e+002 +1.324e+002
+1.323e+002 +1.314e+002 +1.301e+002 +1.277e+002 +1.240e+002 +1.201e+002 +1.162e+002 +1.110e+002 +1.046e+002 +9.946e+001 +9.520e+001 +9.039e+001
+8.557e+001 +8.220e+001 +7.974e+001 +7.713e+001 +7.429e+001 +7.163e+001
+6.877e+001
Err[V/A]:
                       -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001
-8.630e-001 -8.120e-001 +7.900e-001 +7.680e-001 +7.220e-001 +6.500e-001
+5.550e-001 +4.130e-001 +2.510e-001 +1.430e-001 +7.800e-002 +2.300e-002 -2.300e-002 -5.500e-002 -8.300e-002 -1.200e-001 -1.640e-001 -2.000e-001 -2.270e-001 -2.510e-001 -2.770e-001 -2.740e-001 -2.610e-001
 -2.370e-001 -2.120e-001 -1.930e-001 -1.800e-001 -1.930e-001 -2.360e-001
-2.850e-001
     16.6742
                                 3.38
   300.0000
                                71.68
     69.7179
                                50.84
     69.7179
                                19.16
     46.0063 10000000000.00
 <Date: Mon Jul 14 16:29:59 2008</pre>
<Time Range=6 Currrent= 2.50 Stack= 5 Filter=50 Deff=
```

```
*****
#GEOSEC: 0189-B / 50.0 / 50.0 / 1.0 / 36/5 / 0.22222 SPM=0 K= 0.000e+000 H=
                                     1.0/ 562278.000/ 3915801.000/
                                             0.000 DH =
                                                             0.000/\text{rms}=167.00
   [V/A]:
          +0.000e+000 +0.000e+000 +1.219e+000 +1.333e+001 +2.223e+001
+2.733e+001 +2.983e+001 +3.139e+001 +3.291e+001 +3.430e+001 +3.525e+001
+3.604e+001 +3.707e+001 +3.847e+001 +3.987e+001 +4.124e+001 +4.312e+001
+4.547e+001 +4.739e+001 +4.883e+001 +5.006e+001 +5.031e+001 +4.925e+001
+4.736e+001 +4.390e+001 +3.876e+001 +3.417e+001 +3.023e+001 +2.568e+001
+2.102e+001 +1.766e+001 +1.516e+001 +1.254e+001 +1.003e+001 +8.348e+000
+7.146e+000
Err[V/A]:
         +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.890e-001
+5.790e-001 +3.710e-001 +2.820e-001 +2.190e-001 +1.690e-001 +1.490e-001
+1.490e-001 +1.630e-001 +1.900e-001 +2.160e-001 +2.340e-001 +2.480e-001
```

<Remark: IN OLIVE TREES, STEEP TERAIN</pre>

6 Ampl=OFF

```
1D_Inversion_Results_TEM.txt
+2.430e-001 +2.180e-001 +1.740e-001 +8.600e-002 -5.700e-002 -1.950e-001 -3.050e-001 -4.020e-001 -4.600e-001 -4.810e-001 -4.890e-001 -4.930e-001
-4.960e-001 -4.970e-001 +4.970e-001 +4.980e-001 +4.980e-001 +4.980e-001
+4.970e-001
  21.2377
73.1848
73.1848
                   6.05
                   7.55
                   4.22
  39.5244
                 64.27
    1.3179 10000000000.00
<Date: Tue Jul 15 07:32:50 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                       6 Ampl=OFF
<Remark: IN OLIVE TREES
<Place: AGGELIANA
******
                                                 1.0/ 562217.000/ 3915987.000/
                              50.0/ 50.0/
#GEOSEC: 0190-B
71.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                           0.000 DH=
                                                                                0.000/rms=326.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +9.875e+000 +1.786e+001
+2.215e+001 +2.401e+001 +2.501e+001 +2.589e+001 +2.664e+001 +2.720e+001 +2.775e+001 +2.855e+001 +2.976e+001 +3.102e+001 +3.228e+001 +3.409e+001
+3.658e+001 +3.903e+001 +4.144e+001 +4.487e+001 +4.947e+001 +5.372e+001 +5.750e+001 +6.203e+001 +6.658e+001 +6.935e+001 +7.088e+001 +7.164e+001
+7.109e+001 +6.961e+001 +6.767e+001 +6.444e+001 +5.949e+001 +5.444e+001
+4.955e+001
Err[V/A]: -
             -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.960e-001
+5.770e-001 +3.250e-001 +2.200e-001 +1.570e-001 +1.240e-001 +1.250e-001
+1.420e-001 +1.730e-001 +2.160e-001 +2.510e-001 +2.780e-001 +3.110e-001
+3.480e-001 +3.780e-001 +4.040e-001 +4.310e-001 +4.480e-001 +4.450e-001 +4.240e-001 +3.710e-001 +2.810e-001 +1.910e-001 +1.100e-001 +1.500e-002 -8.400e-002 -1.590e-001 -2.210e-001 -2.970e-001 -3.800e-001 -4.350e-001
-4.650e-001
  26.9369
                 13.53
5.76
  20.0161
                 97.83
 114.4385
 100,0000
                  83.19
  12.2774 10000000000.00
<Date: Tue Jul 15 07:53:28 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                       6 Ampl=OFF
<Remark: IN OLIVE TREES</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0191-B
                              50.0/ 50.0/
                                                  1.0/ 562022.000/ 3916054.000/
65.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          0.000 DH =
                                                                                0.000/rms = 96.00
S [V/A]: +0.000e+000 +2.140e-001 +2.224e+001 +3.498e+001 +4.377e+001 +4.950e+001 +5.313e+001 +5.614e+001 +6.002e+001 +6.472e+001 +6.882e+001 +7.246e+001 +7.712e+001 +8.282e+001 +8.785e+001 +9.222e+001 +9.753e+001 +1.031e+002 +1.067e+002 +1.088e+002 +1.088e+002 +1.085e+002 +1.085e+002 +1.057e+002
+1.023e+002 +9.715e+001 +9.019e+001 +8.400e+001 +7.847e+001 +7.161e+001
+6.380e+001 +5.759e+001 +5.259e+001 +4.694e+001 +4.114e+001 +3.696e+001
+3.382e+001
Err[V/A]:
             -9.000e-001 -9.000e-001 -9.000e-001 -8.950e-001 +6.790e-001
+4.210e-001 +3.480e-001 +3.380e-001 +3.380e-001 +3.350e-001 +3.310e-001
+3.290e-001 +3.290e-001 +3.280e-001 +3.230e-001 +3.120e-001 +2.840e-001 +2.290e-001 +1.640e-001 +9.400e-002 +1.000e-015 -1.080e-001 -1.850e-001 -2.400e-001 -2.930e-001 -3.410e-001 -3.720e-001 -3.940e-001 -4.150e-001
-4.330e-001 -4.430e-001 -4.480e-001 -4.500e-001 -4.490e-001 -4.440e-001
-4.390e-001
  53.9941
                   5.92
  10.0162
                   1.15
 145.1583
                100.00
  25.5151
                 55.17
    7.4525 10000000000.00
<Date: Tue Jul 15 08:21:16 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                       6 Ampl=OFF
<Remark: IN OLIVE TREES, FENCES</pre>
<Place: AGGELIANA
<
```

## 1D\_Inversion\_Results\_TEM.txt

```
******
#GEOSEC: 0192-B
                                     50.0/ 50.0/
                                                            1.0/ 562082.000/ 3915860.000/
70.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                        0.000 \text{ DH} =
                                                                                                0.000/rms=259.00
               +0.000e+000 +0.000e+000 +1.764e+001 +2.993e+001 +3.882e+001
+4.503e+001 +4.892e+001 +5.193e+001 +5.528e+001 +5.863e+001 +6.093e+001 +6.259e+001 +6.438e+001 +6.638e+001 +6.819e+001 +6.990e+001 +7.226e+001 +7.527e+001 +7.791e+001 +8.017e+001 +8.287e+001 +8.585e+001 +8.816e+001
+8.992e+001 +9.153e+001 +9.204e+001 +9.093e+001 +8.886e+001 +8.527e+001
+8.046e+001 +7.647e+001 +7.315e+001 +6.902e+001 +6.350e+001 +5.775e+001
+5.187e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +7.460e-001 +4.880e-001 +3.870e-001 +3.420e-001 +2.940e-001 +2.370e-001 +1.930e-001
+1.660e-001 +1.490e-001 +1.500e-001 +1.610e-001 +1.740e-001 +1.890e-001
+1.970e-001 +1.960e-001 +1.890e-001 +1.780e-001 +1.620e-001 +1.450e-001 +1.200e-001 +6.600e-002 -2.800e-002 -1.170e-001 -1.860e-001 -2.410e-001 -2.700e-001 -2.780e-001 -2.880e-001 -3.220e-001 -3.940e-001 -4.540e-001
-4.840e-001
   42.4808
                     10.13
 42.4808
100.2964
                      1.00
                    100.00
   91.6662
                     76.03
   18.4126 10000000000.00
<Date: Tue Jul 15 08:46:47 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: NE OF AGGELIANA
                                                                                     6 Ampl=OFF
<Place: AGGELIANA
*****
                                 / 50.0/ 50.0/ 1.0/ 561758.000/ 3915772.000/
#GEOSEC: 0193
115.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                         0.000 DH =
0.000/\text{rms}=188.00
S [V/A]: +0.000e+000 +0.000e+000 +2.616e+000 +1.921e+001 +2.948e+001 +3.250e+001 +3.243e+001 +3.219e+001 +3.218e+001 +3.279e+001 +3.379e+001 +3.498e+001 +3.684e+001 +3.958e+001 +4.244e+001 +4.531e+001 +4.950e+001
+5.535e+001 +6.108e+001 +6.655e+001 +7.378e+001 +8.229e+001 +8.883e+001 +9.368e+001 +9.844e+001 +1.024e+002 +1.046e+002 +1.058e+002 +1.061e+002
+1.040e+002 +9.935e+001 +9.279e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.420e-001 +1.810e-001 -3.100e-002 -2.600e-002 +4.000e-002 +1.310e-001 +1.990e-001
+2.490e-001 +3.020e-001 +3.580e-001 +4.020e-001 +4.370e-001 +4.750e-001 +5.100e-001 +5.270e-001 +5.280e-001 +5.080e-001 +4.540e-001 +3.860e-001 +3.170e-001 +2.350e-001 +1.540e-001 +9.900e-002 +4.900e-002 -3.600e-002 -1.850e-001 -3.310e-001 -4.250e-001
   34.4524
                     25.45
 400.0000
                   100.00
                     44.61
69.75
   69.4914
   21.6796
     3.0000 10000000000.00
<Date: Tue Jul 15 09:10:02 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                     6 Ampl=OFF
<Remark: NORTH OF AGGELIANA, FENCES</pre>
#GEOSEC: 0194-B / 50.0/ 50.0/ 1.0/ 561679.000/ 3915991.000/ 107.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=430.00
S [V/A]: +0.000e+000 +0.000e+000 +1.568e+001 +3.917e+001 +6.076e+001 +7.899e+001 +9.081e+001 +9.971e+001 +1.095e+002 +1.189e+002 +1.249e+002 +1.288e+002 +1.328e+002 +1.372e+002 +1.409e+002 +1.440e+002 +1.473e+002
+1.498e+002 +1.503e+002 +1.498e+002 +1.477e+002 +1.437e+002 +1.389e+002 +1.336e+002 +1.258e+002 +1.153e+002 +1.064e+002 +9.898e+001 +9.090e+001
+8.328e+001 +7.825e+001 +7.456e+001 +7.017e+001 +6.409e+001 +5.744e+001
+5.056e+001
                +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.850e-001
Err[V/A]:
+7.240e-001 +5.810e-001 +5.010e-001 +4.160e-001 +3.130e-001 +2.330e-001
+1.860e-001 +1.600e-001 +1.540e-001 +1.500e-001 +1.370e-001 +1.040e-001 +4.900e-002 -4.000e-003 -4.900e-002 -1.030e-001 -1.670e-001 -2.230e-001
```

```
1D_Inversion_Results_TEM.txt
-2.740e-001 -3.300e-001 -3.750e-001 -3.930e-001 -3.930e-001 -3.760e-001 -3.410e-001 -3.110e-001 -3.030e-001 -3.380e-001 -4.210e-001 -4.770e-001
-4.950e-001
   56.9571
                    1.00
    9.6654
                    1.02
 231.1973
                   67.49
                   84.87
   95.4364
   24.4474 10000000000.00
<Date: Tue Jul 15 10:44:59 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NORTH OF AGGELIANA</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0195-B / 50.0/ 50.0/ 1.65.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 561670.000/ 3916274.000/
                                                                0.000 DH=
                                                                                      0.000/rms=189.00
S [V/A]: +0.000e+000 +0.000e+000 +5.866e+000 +1.701e+001 +2.393e+001
+2.708e+001 +2.816e+001 +2.864e+001 +2.889e+001 +2.900e+001 +2.907e+001
+2.917e+001 +2.947e+001 +3.009e+001 +3.089e+001 +3.178e+001 +3.314e+001 +3.508e+001 +3.694e+001 +3.866e+001 +4.083e+001 +4.317e+001 +4.484e+001
+4.600e+001 +4.713e+001 +4.822e+001 +4.912e+001 +4.998e+001 +5.113e+001
+5.233e+001 +5.298e+001 +5.316e+001 +5.296e+001 +5.253e+001 +5.244e+001
+5.288e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.020e-001 +3.410e-001 +1.510e-001 +8.000e-002 +3.300e-002 +1.500e-002 +1.900e-002
+3.800e-002 +7.600e-002 +1.270e-001 +1.720e-001 +2.080e-001 +2.480e-001
+2.830e-001 +2.990e-001 +3.000e-001 +2.830e-001 +2.410e-001 +1.960e-001
+1.570e-001 +1.240e-001 +1.100e-001 +1.150e-001 +1.230e-001 +1.210e-001 +9.100e-002 +4.600e-002 +3.000e-003 -3.000e-002 -2.400e-002 +2.600e-002
+8.800e-002
 17.5266
33.5799
200.3506
31.3916
                    1.73
                   37.79
                   53.47
                   23.58
   55.6375 10000000000.00
<Date: Tue Jul 15 11:16:42 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NORTH OF AGGELIANA</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0196-B / 50.0 / 50.0 / 1.61.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 561456.000/ 3916302.000/
H= 0.000 DH= 0.000/
                                                                                      0.000/rms=101.00
              +0.000e+000 +0.000e+000 +2.194e+001 +3.386e+001 +4.063e+001
S [V/A]:
+4.305e+001 +4.361e+001 +4.382e+001 +4.402e+001 +4.423e+001 +4.440e+001 +4.456e+001 +4.482e+001 +4.521e+001 +4.560e+001 +4.596e+001 +4.639e+001 +4.681e+001 +4.700e+001 +4.702e+001 +4.683e+001 +4.633e+001 +4.575e+001
+4.523e+001 +4.467e+001 +4.425e+001 +4.415e+001 +4.419e+001 +4.425e+001
+4.396e+001 +4.315e+001 +4.193e+001 +3.986e+001 +3.695e+001 +3.436e+001
+3.215e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.900e-001 +5.290e-001 +1.500e-001 +4.800e-002 +2.700e-002 +2.300e-002 +2.200e-002 +2.300e-002 +2.300e-002 +2.300e-002 +3.600e-002 +4.600e-002 +5.200e-002 +5.300e-002 +4.800e-002 +3.200e-002 +1.300e-002 -9.000e-003 -3.700e-002 -6.400e-002 -7.600e-002 -7.500e-002 -5.900e-002 -2.800e-002 -3.000e-003 +7.000e-003 -1.100e-002 -7.500e-002 -1.540e-001 -2.250e-001 -2.950e-001 -3.460e-001 -3.700e-001
-3.850e-001
   36.3886
41.7987
                    1.01
                    5.35
   46.7150
                   80.36
  26.9872
                  100.00
    4.9100 10000000000.00
<Date: Tue Jul 15 11:45:53 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                             6 Ampl=OFF
<Remark: NORTH OF AGGELIANA</pre>
<Place: AGGELIANA
*****
```

```
1D_Inversion_Results_TEM.txt
#GEOSEC: 0197-B / 50.0/ 50.0/ 1.0/ 561478.000/ 3915963.000/ 102.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=114.00
                +0.000e+000 +0.000e+000 +1.624e+000 +1.883e+001 +3.256e+001
S [V/A]:
+4.148e+001 +4.665e+001 +5.074e+001 +5.592e+001 +6.237e+001 +6.792e+001 +7.262e+001 +7.805e+001 +8.349e+001 +8.709e+001 +8.934e+001 +9.112e+001 +9.196e+001 +9.189e+001 +9.140e+001 +9.030e+001 +8.817e+001 +8.546e+001
+8.229e+001 +7.733e+001 +7.049e+001 +6.458e+001 +5.962e+001 +5.402e+001
+4.839e+001 +4.438e+001 +4.132e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.950e-001 +6.730e-001 +5.210e-001 +4.820e-001 +4.710e-001 +4.570e-001 +4.320e-001
+3.990e-001 +3.460e-001 +2.720e-001 +2.020e-001 +1.440e-001 +7.900e-002 +1.800e-002 -2.200e-002 -5.100e-002 -9.000e-002 -1.500e-001 -2.140e-001 -2.760e-001 -3.420e-001 -3.930e-001 -4.140e-001 -4.210e-001 -4.180e-001
-4.080e-001 -3.990e-001 -3.920e-001
   48.5387
                       4.52
    7.5925
                       1.11
 176.2003
                      56.74
   44.2293 64.17
10.3884 100000000000.00
<Date: Tue Jul 15 12:18:39 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                         6 Ampl=OFF
<Remark: NORTH OF AGGELIANA, POWER LINES</pre>
<Place: AGGELIANA
*****
                                  / 50.0/ 50.0/
#GEOSEC: 0198-C
                                                              1.0/ 561558.000/ 3915873.000/
119.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                             0.000 DH =
0.000/\text{rms}=301.00
     [V/A]:
                 +0.000e+000 +0.000e+000 +1.289e+000 +5.625e+000 +1.172e+001
+1.872e+001 +2.431e+001 +2.909e+001 +3.517e+001 +4.290e+001 +4.998e+001 +5.654e+001 +6.507e+001 +7.499e+001 +8.264e+001 +8.801e+001 +9.269e+001 +9.540e+001 +9.601e+001 +9.591e+001 +9.559e+001 +9.544e+001 +9.553e+001 +9.554e+001 +9.511e+001 +9.354e+001 +9.136e+001 +8.907e+001 +8.633e+001
+8.419e+001 +8.403e+001 +8.558e+001
                +5.000e-001 -9.000e-001 -9.000e-001 +9.000e-001
Err[V/A]:
+8.860e-001 +8.330e-001 +7.850e-001 +7.430e-001 +7.090e-001 +6.850e-001 +6.630e-001 +6.220e-001 +5.480e-001 +4.540e-001 +3.510e-001 +2.160e-001
+8.300e-002 +1.300e-002 -1.200e-002 -1.400e-002 -1.000e-003 +3.000e-003 -1.100e-002 -5.100e-002 -1.130e-001 -1.550e-001 -1.700e-001 -1.480e-001
-6.200e-002 +6.300e-002 +1.890e-001
   22.8933
                        1.22
                       1.4\bar{5}
     5.4693
 400.0000
                      61.74
                      45.15
   63.2321
   80.4036 10000000000.00
<Date: Tue Jul 15 13:08:25 2008
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                         6 Ampl=OFF
<Remark: NORTH OF AGGELIANA, POWER LINES</pre>
*****
#GEOSEC: 0199 / 50.0/ 50.0/ 1.0/ 561166.000/ 3915884.000/ 95.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +0.000e+000 +1.743e+001 +3.306e+001 +4.421e+001 +5.000e+001 +5.184e+001 +5.253e+001 +5.299e+001 +5.340e+001 +5.372e+001 +5.401e+001 +5.433e+001 +5.467e+001 +5.490e+001 +5.507e+001 +5.523e+001
                                                                                                    0.000/rms=158.00
+5.531e+001 +5.521e+001 +5.493e+001 +5.432e+001 +5.327e+001 +5.223e+001 +5.134e+001 +5.037e+001 +4.958e+001 +4.925e+001 +4.915e+001 +4.915e+001
+4.889e+001 +4.796e+001 +4.623e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.570e-001
+3.330e-001 +1.320e-001 +6.700e-002 +4.100e-002 +3.500e-002 +3.500e-002
+3.400e-002 +3.100e-002 +2.700e-002 +2.200e-002 +1.900e-002 +1.200e-002 -3.000e-003 -2.300e-002 -4.700e-002 -7.700e-002 -1.050e-001 -1.120e-001 -9.200e-002 -5.700e-002 -2.600e-002 -8.000e-003 -1.200e-002 -7.300e-002 -1.830e-001 -2.890e-001
 100.0000
                        3.67
   12.6017
                        1.00
```

```
1D_Inversion_Results_TEM.txt
   58.4641
                    62.67
                     19.92
   33.1213
   44.0087 10000000000.00
<Date: Tue Jul 15 14:17:37 2008</pre>
<Time Range=5 Currrent= 1.90 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: 400M EAST OF G-12</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0200-A / 50.0/ 50.0/ 1.0 106.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          1.0/ 561364.000/ 3915805.000/
                                                                        0.000 DH =
0.000/\text{rms}=593.00
                +9.769e+000 +1.654e+001 +2.164e+001 +2.517e+001 +2.819e+001
    [V/A]:
+3.027e+001 +3.115e+001 +3.149e+001 +3.160e+001 +3.154e+001 +3.146e+001
+3.144e+001 +3.151e+001 +3.181e+001 +3.232e+001 +3.297e+001 +3.409e+001 +3.587e+001 +3.775e+001 +3.962e+001 +4.215e+001 +4.527e+001 +4.786e+001
+5.005e+001 +5.267e+001 +5.572e+001 +5.822e+001 +6.038e+001 +6.297e+001
+6.564e+001 +6.731e+001 +6.808e+001
Err[V/A]: -9.000e-001 -8.790e-001 -7.770e-001 -6.200e-001 +4.120e-001 +2.190e-001 +1.070e-001 +4.600e-002 +5.000e-003 -1.200e-002 -9.000e-003 +3.000e-003 +2.800e-002 +7.100e-002 +1.140e-001 +1.570e-001 +2.110e-001 +2.690e-001 +3.070e-001 +3.270e-001 +3.350e-001 +3.260e-001 +3.080e-001
+2.910e-001 +2.740e-001 +2.610e-001 +2.520e-001 +2.410e-001 +2.180e-001
+1.720e-001 +1.110e-001 +4.600e-002
   29.8626
                    15.71
   29.8626
                      1.46
   46.9963
                    21.85
   46.9963
                      1.00
 100.0000 10000000000.00
<Date: Tue Jul 15 14:43:54 2008</pre>
<Time Range=5 Currrent= 3.40 Stack= 5 Filter=50 Deff=
<Remark: FENCES, POWERLINES, NOT SQUARE</pre>
                                                                                    6 Ampl=OFF
******
#GEOSEC: 0201-D / 50.0/ 50.0/ 1.0/ 560979.000/ 3915906.000/ 97.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/r S [V/A]: +0.000e+000 +0.000e+000 +1.396e+001 +2.631e+001 +3.399e+001 +3.785e+001 +3.957e+001 +4.076e+001 +4.204e+001 +4.347e+001 +4.465e+001
                                                                                              0.000/rms=144.00
+4.568e+001 +4.703e+001 +4.870e+001 +5.019e+001 +5.145e+001 +5.292e+001 +5.436e+001 +5.523e+001 +5.567e+001 +5.584e+001 +5.550e+001 +5.484e+001 +5.401e+001 +5.271e+001 +5.088e+001 +4.924e+001 +4.787e+001 +4.641e+001 +4.529e+001 +4.495e+001 +4.513e+001 +4.585e+001 +4.694e+001 +4.724e+001
+4.624e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +7.050e-001 +3.280e-001 +2.070e-001 +1.750e-001 +1.580e-001 +1.510e-001 +1.500e-001 +1.540e-001 +1.620e-001 +1.690e-001 +1.620e-001 +1.620e-001 +1.620e-001 +1.620e-001 +1.090e-001 +7.200e-002 +3.800e-002 -5.000e-003 -5.200e-002 -8.800e-002 -1.180e-001 -1.500e-001 -1.780e-001 -1.800e-001 -1.800e-001 -1.640e-001
-7.800e-002 -5.000e-003 +5.600e-002 +1.010e-001 +7.200e-002 -6.300e-002
-2.220e-001
   98.4885
                      4.27
    6.3771
                      1.00
   62.8512
27.5035
                    88.57
66.91
   84.8314 10000000000.00
<Date: Tue Jul 15 15:21:23 2008</pre>
<Time Range=6 Currrent= 3.20 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: POWERLINES, 260M NE OF G-12</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0202-B / 50.0/ 50.0/ 1. 98.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 561033.000/ 3916183.000/
                                                                      0.000 DH =
                                                                                              0.000/\text{rms}=260.00
    [V/A]: +0.000e+000 +0.000e+000 +3.441e+000 +2.064e+001 +3.343e+001
+4.096e+001 +4.436e+001 +4.627e+001 +4.769e+001 +4.834e+001 +4.832e+001 +4.816e+001 +4.797e+001 +4.796e+001 +4.810e+001 +4.828e+001 +4.845e+001
+4.852e+001 +4.842e+001 +4.820e+001 +4.778e+001 +4.705e+001 +4.624e+001
                                                    Σελίδα 72
```

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1D_Inversion_Results_TEM.txt
+4.541e+001 +4.424e+001 +4.281e+001 +4.169e+001 +4.087e+001 +4.011e+001 +3.960e+001 +3.936e+001 +3.909e+001 +3.833e+001 +3.644e+001 +3.397e+001
+3.141e+001
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.850e-001
Err[V/A]:
+5.590e-001 +3.270e-001 +2.160e-001 +1.140e-001 +2.700e-002 -1.300e-002 -2.200e-002 -1.200e-002 +9.000e-003 +2.100e-002 +2.300e-002 +1.400e-002 -4.000e-003 -2.200e-002 -3.900e-002 -6.100e-002 -8.900e-002 -1.130e-001 -1.320e-001 -1.490e-001 -1.550e-001 -1.440e-001 -1.220e-001 -8.500e-002 -4.800e-002 -4.200e-002 -7.500e-002 -1.690e-001 -3.040e-001 -3.900e-001
-4.360e-001
    9.9652
                    1.16
 400.0000
                    3.84
                  56.66
   50.4235
   31.6262
                 100.00
   24.6791 10000000000.00
<Date: Tue Jul 15 15:47:56 2008</pre>
<Time Range=6 Currrent= 3.20 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: 500M NE OF G-12</pre>
*****
#GEOSEC: 0203-C / 50.0/ 50.0/ 1. 97.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 560782.000/ 3916084.000/
                                                              0.000 DH=
                                                                                    0.000/rms=232.00
S [V/A]: +0.000e+000 +0.000e+000 +3.161e+000 +1.494e+001 +2.353e+001 +2.893e+001 +3.193e+001 +3.413e+001 +3.656e+001 +3.908e+001 +4.091e+001
+4.226e+001 +4.362e+001 +4.472e+001 +4.525e+001 +4.541e+001 +4.533e+001
+4.501e+001 +4.468e+001 +4.442e+001 +4.413e+001 +4.376e+001 +4.332e+001
+4.280e+001 +4.197e+001 +4.086e+001 +3.998e+001 +3.937e+001 +3.893e+001
+3.895e+001 +3.938e+001 +3.993e+001 +4.044e+001 +3.990e+001 +3.771e+001
+3.444e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.800e-001 +6.000e-001 +4.390e-001 +3.770e-001 +3.250e-001 +2.740e-001 +2.310e-001
+1.940e-001 +1.470e-001 +9.100e-002 +4.400e-002 +9.000e-003 -2.100e-002 -3.900e-002 -4.100e-002 -3.900e-002 -5.100e-002 -7.200e-002
-9.500e-002 -1.180e-001 -1.280e-001 -1.150e-001 -8.600e-002 -3.300e-002
+3.700e-002 +8.100e-002 +8.400e-002 +8.000e-003 -2.030e-001 -3.940e-001
-4.760e-001
    8.0527
                    1.49
 122.4452
                    5.21
   55.4540
                  36.98
   32.2629
                   9.63
   34.9391 10000000000.00
<Date: Tue Jul 15 16:18:40 2008</pre>
<Time Range=6 Currrent= 2.90 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: 320M NORTH OF G-12</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0204-C / 50.0 / 50.0 / 1.86.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 561068.000/ 3916073.000/
                                                              0.000 DH=
                                                                                    0.000/rms=313.00
    [V/A]: +0.000e+000 +0.000e+000 +4.348e+000 +1.248e+001 +1.744e+001
+1.986e+001 +2.103e+001 +2.189e+001 +2.300e+001 +2.443e+001 +2.572e+001
+2.687e+001 +2.830e+001 +2.983e+001 +3.085e+001 +3.147e+001 +3.189e+001
+3.199e+001 +3.192e+001 +3.188e+001 +3.192e+001 +3.216e+001 +3.247e+001 +3.281e+001 +3.327e+001 +3.387e+001 +3.442e+001 +3.494e+001 +3.567e+001 +3.655e+001 +3.724e+001 +3.771e+001 +3.802e+001 +3.789e+001 +3.739e+001
+3.673e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.000e-001 +3.980e-001 +2.710e-001 +2.530e-001 +2.630e-001 +2.770e-001 +2.830e-001
+2.800e-001 +2.620e-001 +2.170e-001 +1.600e-001 +1.070e-001 +4.600e-002
+1.000e-015 -1.100e-002 -2.000e-003 +2.100e-002 +4.800e-002 +6.500e-002
+7.400e-002 +8.200e-002 +9.100e-002 +1.010e-001 +1.100e-001 +1.170e-001
+1.140e-001 +9.700e-002 +6.800e-002 +1.700e-002 -5.100e-002 -1.010e-001
-1.390e-001
 100.0000
                    2.37
    4.6146
                   1.00
                 100.00
   37.2720
  48.0428
                 100.00
```

```
1D_Inversion_Results_TEM.txt
  23.3394 10000000000.00
<Date: Tue Jul 15 16:51:08 2008</pre>
<Time Range=6 Currrent= 2.70 Stack= 5 Filter=50 Deff=</pre>
                                                                         6 Ampl=OFF
<Remark: POWER LINES</pre>
<Place: AGGELIANA
#GEOSEC: 0205 / 50.0/ 50.0/ 1.0 16.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 560701.000/ 3919367.000/
                                                            0.000 DH =
                                                                                  0.000/\text{rms}=703.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.701e+000 +6.691e+000 +1.257e+001 +1.693e+001 +2.019e+001 +2.378e+001 +2.758e+001 +3.063e+001
+3.331e+001 +3.685e+001 +4.132e+001 +4.520e+001 +4.810e+001 +5.020e+001
+4.946e+001 +4.642e+001 +4.284e+001 +3.820e+001 +3.325e+001 +2.961e+001
+2.677e+001 +2.350e+001 +1.991e+001 +1.715e+001 +1.496e+001 +1.259e+001 +1.035e+001 +8.894e+000 +7.908e+000
             -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001
Err[V/A]:
+8.980e-001 +8.480e-001 +7.590e-001 +6.540e-001 +5.620e-001 +5.200e-001
+5.060e-001 +5.020e-001 +4.870e-001 +4.350e-001 +3.280e-001 +9.400e-002 -2.230e-001 -3.820e-001 -4.340e-001 -4.540e-001 -4.590e-001 -4.610e-001 -4.660e-001 -4.760e-001 -4.860e-001 -4.910e-001 -4.940e-001 -4.940e-001
-4.920e-001 -4.860e-001 -4.770e-001
   21.8208
                  12.89
 200.0000
                  29.63
    5.4873
                  13.07
    1.0000 10000000000.00
<Date: Thu Jul 17 07:14:47 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: FENCES, NATIONAL ROAD
<Place: PANORMOS
<***************************
*****
#GEOSEC: 0207-B / 50.0/ 50.0/ 1.
14.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 561108.000/ 3919373.000/
                                                            0.000 DH =
                                                                                  0.000/\text{rms}=217.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.281e+001 +2.613e+001 +3.753e+001 +4.558e+001 +5.186e+001 +5.840e+001 +6.326e+001 +6.418e+001
+6.265e+001 +5.864e+001 +5.252e+001 +4.713e+001 +4.281e+001 +3.797e+001
+3.318e+001 +2.984e+001 +2.741e+001 +2.490e+001 +2.255e+001 +2.096e+001 +1.981e+001 +1.857e+001 +1.724e+001 +1.615e+001 +1.516e+001 +1.385e+001
+1.223e+001 +1.090e+001 +9.826e+000 +8.637e+000 +7.466e+000 +6.658e+000
+6.070e+000
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.370e-001 +7.230e-001 +6.250e-001 +4.680e-001 +2.080e-001 -4.900e-002 -2.360e-001 -3.660e-001 -4.290e-001 -4.490e-001 -4.540e-001 -4.540e-001
-4.470e-001 -4.370e-001 -4.240e-001 -4.030e-001 -3.750e-001 -3.490e-001 -3.310e-001 -3.200e-001 -3.280e-001 -3.530e-001 -3.840e-001 -4.210e-001 -4.510e-001 -4.640e-001 -4.690e-001 -4.680e-001 -4.620e-001 -4.540e-001
-4.440e-001
   26.7592
                   7.79
 200.0000
                  24.35
    5.1817
                  38.94
    1.0000 10000000000.00
<Date: Thu Jul 17 07:58:57 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
<Remark: NATIONAL ROAD, BY THE SEA
<Place: PANORMOS
*****
0.000/\text{rms}=245.00
+3.123e+001 +3.700e+001 +4.130e+001 +4.577e+001 +4.955e+001 +5.128e+001
+5.174e+001 +5.126e+001 +4.958e+001 +4.749e+001 +4.530e+001 +4.220e+001
+3.821e+001 +3.477e+001 +3.185e+001 +2.844e+001 +2.484e+001 +2.218e+001 +2.013e+001 +1.787e+001 +1.555e+001 +1.387e+001 +1.256e+001 +1.112e+001 +9.644e+000 +8.569e+000 +7.743e+000 +6.838e+000 +5.913e+000 +5.228e+000
```

+8.080e-001 +6.600e-001 +5.580e-001 +4.310e-001 +2.650e-001 +1.200e-001

-1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001

+4.689e+000

Err[V/A]:

```
1D_Inversion_Results_TEM.txt
+1.000e-002 -1.000e-001 -1.990e-001 -2.650e-001 -3.140e-001 -3.640e-001 -4.060e-001 -4.300e-001 -4.420e-001 -4.500e-001 -4.550e-001 -4.550e-001 -4.570e-001 -4.570e-001 -4.580e-001 -4.600e-001 -4.610e-001 -4.620e-001
-4.630e-001 -4.640e-001 -4.640e-001 -4.650e-001 -4.680e-001 -4.720e-001
-4.750e-001
   16.7813
74.7534
                   30.78
    4.9186
                   19.47
    1.3077 10000000000.00
<Date: Thu Jul 17 08:30:45 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: NEXT TO HOTEL, BY THE SEA</pre>
                                                                               6 Ampl=OFF
<Place: PANORMOS
******
#GEOSEC: 0209-B / 50.0/ 50.0/ 1
7.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 561615.000/ 3919326.000/
                                                                 0.000 DH =
                                                                                        0.000/\text{rms}=277.00
S [V/A]: +0.000e+000 +0.000e+000 +1.962e+001 +5.031e+001 +7.921e+001
+9.541e+001 +9.584e+001 +9.100e+001 +8.216e+001 +7.060e+001 +6.117e+001 +5.377e+001 +4.578e+001 +3.805e+001 +3.263e+001 +2.867e+001 +2.445e+001
+2.031e+001 +1.737e+001 +1.519e+001 +1.289e+001 +1.072e+001 +9.272e+000 +8.260e+000 +7.267e+000 +6.407e+000 +5.902e+000 +5.592e+000 +5.350e+000
+5.243e+000 +5.281e+000 +5.396e+000 +5.630e+000 +6.003e+000 +6.369e+000
+6.711e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.760e-001
+3.590e-001 -1.630e-001 -3.580e-001 -4.410e-001 -4.740e-001 -4.840e-001
-4.870e-001 -4.890e-001 -4.890e-001 -4.890e-001 -4.890e-001 -4.890e-001
-4.910e-001 -4.910e-001 -4.920e-001 -4.910e-001 -4.880e-001 -4.830e-001 -4.750e-001 -4.570e-001 -4.170e-001 -3.600e-001 -2.880e-001 -1.740e-001
-2.200e-002 +1.000e-001 +1.890e-001 +2.680e-001 +3.230e-001 +3.440e-001
+3.540e-001
 27.2298
200.0000
                   4.32
17.99
    2.5504
                   12.07
                     5.22
    1.0000
   24.0000 10000000000.00
<Date: Thu Jul 17 08:58:22 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                               6 Ampl=OFF
<Remark: BY THE SEA, POWERLINES</pre>
<Place: PANORMOS
*****
#GEOSEC: 0210-C / 50.0/ 50.0/ 1
4.0/40/5/0/22222 SPM=0 K= 0.000e+000 H=
5. [V/A] + 0.000e+000 H=
                                                     1.0/ 561885.000/ 3919523.000/
                                                                0.000 DH =
                                                                                        0.000/rms=126.00
S [V/A]: +0.000e+000 +0.000e+000 +2.520e-001 +1.709e+001 +3.153e+001 +4.191e+001 +4.794e+001 +5.165e+001 +5.412e+001 +5.370e+001 +5.092e+001 +4.735e+001 +4.226e+001 +3.620e+001 +3.140e+001 +2.769e+001 +2.366e+001
+1.974e+001 +1.705e+001 +1.510e+001 +1.309e+001 +1.122e+001 +9.974e+000
+9.089e+000 +8.192e+000 +7.359e+000 +6.806e+000 +6.399e+000 +5.969e+000 +5.541e+000 +5.232e+000 +4.997e+000 +4.749e+000 +4.521e+000 +4.380e+000 +4.289e+000 +4.200e+000 +4.087e+000 +3.942e+000 +3.755e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.990e-001
+7.370e-001 +5.270e-001 +3.550e-001 +1.130e-001 -1.750e-001 -3.430e-001 -4.170e-001 -4.580e-001 -4.780e-001 -4.850e-001 -4.870e-001 -4.850e-001 -4.850e-001 -4.670e-001 -4.550e-001 -4.550e-001 -4.210e-001 -3.930e-001 -3.690e-001 -3.510e-001 -3.310e-001 -3.120e-001 -2.960e-001 -2.400e-001 -2.030e-001 -1.600e-001
-1.310e-001 -1.240e-001 -1.720e-001 -2.600e-001 -3.400e-001
                   9.75
13.94
   28.2993
 120.0000
    2.2744
                   10.14
    1.7855
                     4.00
    3.0029 10000000000.00
<Date: Thu Jul 17 09:29:47 2008
<Time Range=7 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                               6 Ampl=OFF
<Remark: BY THE SEA, FENCES, NEAR HOUSE</pre>
<Place: PANORMOS
<
```

```
******
#GEOSEC: 0211-C
                                    50.0/ 50.0/
                                                          1.0/ 562050.000/ 3919482.000/
10.0/40/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                      0.000 \text{ DH} =
                                                                                              0.000/rms=227.00
               +0.000e+000 +0.000e+000 +0.000e+000 +1.792e+001 +3.505e+001
+4.696e+001 +5.307e+001 +5.642e+001 +5.859e+001 +5.870e+001 +5.724e+001
+5.524e+001 +5.228e+001 +4.864e+001 +4.562e+001 +4.316e+001 +4.029e+001 +3.719e+001 +3.479e+001 +3.282e+001 +3.052e+001 +2.802e+001 +2.608e+001
+2.452e+001 +2.277e+001 +2.094e+001 +1.961e+001 +1.856e+001 +1.738e+001
+1.614e+001 +1.519e+001 +1.442e+001 +1.354e+001 +1.260e+001 +1.186e+001 +1.125e+001 +1.048e+001 +9.497e+000 +8.559e+000 +7.665e+000 Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.990e-001 +7.280e-001 +4.700e-001 +2.940e-001 +1.090e-001 -7.300e-001 -1.860e-001
-2.480e-001 -2.910e-001 -3.160e-001 -3.270e-001 -3.310e-001 -3.340e-001 -3.370e-001 -3.410e-001 -3.460e-001 -3.510e-001 -3.560e-001 -3.560e-001 -3.510e-001 -3.510e-001 -3.580e-001 -3.290e-001 -3.230e-001 -3.190e-001 -3.180e-001 -3.160e-001 -3.150e-001 -3.140e-001 -3.200e-001 -3.330e-001 -3.670e-001 -4.210e-001 -4.630e-001 -4.840e-001
   38.1572
                    10.97
 120.0000
                     18.80
   11.7849
                     33.14
    5.4889
                    61.20
    1.7986 10000000000.00
<Date: Thu Jul 17 09:56:15 2008
<Time Range=7 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                    6 Ampl=OFF
<Remark: BY THE SEA, FENCES
<Place: PANORMOS
*******
#GEOSEC: 0212-B / 50.0/ 50.0/ 1.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 562245.000/ 3919353.000/
                                                                      0.000 DH=
                                                                                              0.000/rms=128.00
               +0.000e+000 +0.000e+000 +3.979e+000 +1.774e+001 +2.825e+001
+3.514e+001 +3.895e+001 +4.156e+001 +4.428e+001 +4.698e+001 +4.895e+001 +5.052e+001 +5.235e+001 +5.431e+001 +5.568e+001 +5.640e+001 +5.640e+001 +5.473e+001 +5.191e+001 +4.869e+001 +4.417e+001 +3.887e+001 +3.475e+001
+3.155e+001 +2.801e+001 +2.436e+001 +2.167e+001 +1.952e+001 +1.709e+001
+1.457e+001 +1.274e+001 +1.139e+001 +9.978e+000 +8.683e+000 +7.856e+000
+7.310e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.840e-001 +6.220e-001 +4.430e-001 +3.600e-001 +2.970e-001 +2.460e-001 +2.160e-001
+2.000e-001 +1.840e-001 +1.570e-001 +1.120e-001 +4.800e-002 -6.700e-002 -2.230e-001 -3.310e-001 -3.920e-001 -4.310e-001 -4.500e-001 -4.550e-001 -4.560e-001 -4.570e-001 -4.610e-001 -4.660e-001 -4.710e-001 -4.750e-001 -4.790e-001 -4.780e-001 -4.760e-001 -4.670e-001 -4.470e-001 -4.160e-001
-3.770e-001
   29.9995
                      9.58
                     20.18
 120.0000
   25.7504
                    28.59
    2.5451
                    19.48
    1.3374 10000000000.00
<Date: Thu Jul 17 10:25:21 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: BY THE SEA, CLUB MARINE HOTEL</pre>
<Place: PANORMOS
*****
#GEOSEC: 0213-B / 50.0/ 50.0/ 58.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                          1.0/ 562468.000/ 3919393.000/
                                                                     0.000 DH = 
                                                                                            0.000/\text{rms}=227.00
               +0.000e+000 +0.000e+000 +0.000e+000 +4.802e+000 +1.271e+001
    [V/A]:
+1.978e+001 +2.428e+001 +2.748e+001 +3.098e+001 +3.475e+001 +3.776e+001 +4.022e+001 +4.290e+001 +4.506e+001 +4.565e+001 +4.507e+001 +4.307e+001
+3.949e+001 +3.602e+001 +3.301e+001 +2.945e+001 +2.568e+001 +2.288e+001
+2.072e+001 +1.838e+001 +1.606e+001 +1.447e+001 +1.329e+001 +1.206e+001
+1.087e+001 +1.002e+001 +9.332e+000 +8.513e+000 +7.546e+000 +6.713e+000
+5.989e+000
               -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001
Err[V/A]:
+8.670e-001 +7.270e-001 +6.160e-001 +5.280e-001 +4.600e-001 +4.160e-001 +3.720e-001 +2.900e-001 +1.460e-001 -1.300e-002 -1.570e-001 -2.970e-001
-3.900e-001 -4.270e-001 -4.420e-001 -4.520e-001 -4.580e-001 -4.600e-001
```

```
1D_Inversion_Results_TEM.txt
-4.590e-001 -4.560e-001 -4.480e-001 -4.380e-001 -4.260e-001 -4.110e-001 -3.960e-001 -3.920e-001 -3.990e-001 -4.200e-001 -4.510e-001 -4.720e-001
-4.850e-001
  18.5815
                   6.87
 100.0000
                  20.81
  20.3607
                  17.26
    2.6158
                  36.76
    1.0000 10000000000.00
<Date: Thu Jul 17 11:41:07 2008</pre>
<Time Range=6 Currrent= 3.50 Stack= 5 Filter=50 Deff=
                                                                        6 Ampl=OFF
<Remark: BY SEA, IN VILLAGE, POWERLINES
<Place: PANORMOS</pre>
*****
#GEOSEC: 0214 / 50.0/ 50.0/ 1. 12.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                  1.0/ 562621.000/ 3919365.000/
                                                            0.000 DH=
                                                                                 0.000/rms=902.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000
+1.908e+001 +4.541e+001 +5.470e+001 +5.413e+001 +5.006e+001 +4.716e+001
+4.505e+001 +4.257e+001 +3.933e+001 +3.603e+001 +3.285e+001 +2.870e+001 +2.409e+001 +2.071e+001 +1.825e+001 +1.573e+001 +1.340e+001 +1.183e+001 +1.067e+001 +9.398e+000 +8.071e+000 +7.078e+000 +6.290e+000 +5.420e+000
+4.554e+000 +3.940e+000 +3.481e+000
Err[V/A]: -1.000e-015 -1.000e-015 -1.000e-015 -9.000e-001 +9.000e-001 +5.530e-001 -1.910e-001 -3.100e-001 -2.890e-001 -2.800e-001 -3.060e-001 -3.700e-001 -4.270e-001 -4.600e-001 -4.800e-001
-4.870e-001 -4.880e-001 -4.860e-001 -4.810e-001 -4.740e-001 -4.680e-001 -4.660e-001 -4.690e-001 -4.750e-001 -4.800e-001 -4.840e-001 -4.860e-001
-4.860e-001 -4.870e-001 -4.870e-001 23.2257 6.37
 100.0000
                  14.94
                   8.80
    5.1628
    1.2930
                   5.76
    1.0000 10000000000.00
<Date: Thu Jul 17 12:05:49 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                        6 Ampl=OFF
<Remark: AROUND THE CHURCH, IN VILLAGE</pre>
<Place: PANORMOS
*****
0.000/rms=383.00
+7.814e+001 +7.298e+001 +6.619e+001 +6.089e+001 +5.698e+001 +5.295e+001
+4.928e+001 +4.690e+001 +4.526e+001 +4.362e+001 +4.204e+001 +4.082e+001 +3.971e+001 +3.817e+001 +3.599e+001 +3.384e+001 +3.174e+001 +2.886e+001 +2.520e+001 +2.199e+001 +1.922e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.290e-001 +6.570e-001 +5.430e-001 +3.910e-001 +1.390e-001 -1.040e-001
-2.610e-001 -3.540e-001 -3.850e-001 -3.800e-001 -3.630e-001 -3.310e-001 -2.870e-001 -2.470e-001 -2.160e-001 -1.870e-001 -1.710e-001 -1.760e-001 -1.960e-001 -2.370e-001 -2.970e-001 -3.490e-001 -3.910e-001 -4.360e-001
-4.720e-001 -4.880e-001 -4.950e-001
  29.7541
                   5.89
 160.0000
14.7406
                  31.13
                  34.30
   26,4046
                  24.80
    1.6839 10000000000.00
<Date: Thu Jul 17 12:30:20 2008</pre>
<Time Range=5 Currrent= 3.50 Stack= 5 Filter=50 Deff=
                                                                        6 Ampl=OFF
<Remark: BY THE SEA, IN VILLAGE,ON HILL</pre>
<Place: PANORMOS
<****************
#GEOSEC: 0216-B / 50.0/ 50.0/ 1.
57.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 563085.000/ 3919517.000/
                                                             0.000 DH =
                                                                                 0.000/rms=407.00
S [V/A]: +0.000e+000 +0.000e+000 +2.020e+001 +4.917e+001 +8.036e+001
+1.098e+002 +1.267e+002 +1.356e+002 +1.406e+002 +1.403e+002 +1.373e+002
```

```
1D_Inversion_Results_TEM.txt
+1.342e+002 +1.309e+002 +1.283e+002 +1.269e+002 +1.259e+002 +1.241e+002 +1.208e+002 +1.166e+002 +1.122e+002 +1.060e+002 +9.843e+001 +9.224e+001 +8.728e+001 +8.184e+001 +7.657e+001 +7.313e+001 +7.073e+001 +6.835e+001
+6.592e+001 +6.359e+001 +6.093e+001 +5.644e+001 +4.960e+001 +4.320e+001
+3.778e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.950e-001 +7.680e-001 +5.270e-001 +3.120e-001 +9.600e-002 -7.200e-002 -1.350e-001
-1.410e-001 -1.160e-001 -7.700e-002 -5.900e-002 -6.600e-002 -1.020e-001 -1.670e-001 -2.240e-001 -2.660e-001 -3.040e-001 -3.270e-001 -3.320e-001 -3.270e-001 -3.070e-001 -2.720e-001 -2.360e-001 -2.040e-001 -1.800e-001 -1.890e-001 -2.410e-001 -3.170e-001 -4.090e-001 -4.700e-001 -4.880e-001
-4.950e-001
   38.1481
                        3.33
 200.0000
                      45.12
   61.9273
                      61.20
   16.4583
                      86.20
    1.1622 10000000000.00
<Date: Thu Jul 17 13:03:40 2008</pre>
<Time Range=6 Currrent= 3.10 Stack= 5 Filter=50 Deff=</pre>
                                                                                          6 Ampl=OFF
<Remark: ON HILLS, EAST OF PANORMOS</pre>
<place: PANORMOS</pre>
*****
#GEOSEC: 0217-C / 50.0 / 50.0 / 1.67.0 / 36/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                               1.0/ 563236.000/ 3919392.000/
                                                                           0.000 DH=
                                                                                                     0.000/rms=161.00
                +0.000e+000 +5.018e+000 +4.231e+001 +6.807e+001 +9.064e+001
S [V/A]:
+1.042e+002 +1.090e+002 +1.110e+002 +1.120e+002 +1.114e+002 +1.096e+002 +1.074e+002 +1.045e+002 +1.015e+002 +9.939e+001 +9.801e+001 +9.673e+001 +9.563e+001 +9.477e+001 +9.391e+001 +9.252e+001 +9.020e+001 +8.755e+001
+8.468e+001 +8.041e+001 +7.459e+001 +6.947e+001 +6.500e+001 +5.966e+001
+5.374e+001 +4.894e+001 +4.483e+001 +3.977e+001 +3.409e+001 +2.977e+001
+2.652e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.980e-001 +7.650e-001 +3.830e-001 +1.710e-001 +8.500e-002 +1.400e-002 -6.100e-002 -1.120e-001
-1.370e-001 -1.430e-001 -1.280e-001 -1.050e-001 -8.500e-002 -6.500e-002
-5.400e-001 -1.430e-001 -7.200e-002 -1.010e-001 -1.490e-001 -1.970e-001 -2.420e-001 -2.940e-001 -3.420e-001 -3.690e-001 -3.830e-001 -3.960e-001 -4.130e-001 -4.310e-001 -4.490e-001 -4.660e-001 -4.780e-001 -4.800e-001
-4.800e-001
 32.1982
200.0000
                        3.17
                      30.97
   58.3363
                      83.62
                      45.81
     8.0361
     1.9792 10000000000.00
<Date: Thu Jul 17 13:50:09 2008</pre>
<Time Range=6 Currrent= 2.90 Stack= 5 Filter=50 Deff= <Remark: EAST OF PANORMOS, AT SHEPERT'S
                                                                                          6 Ampl=OFF
<Place: PANORMOS
<
*****
#GEOSEC: 0218-B / 50.0/ 50.0/ 1. 78.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               1.0/ 563551.000/ 3919455.000/
                                                                          0.000 DH =
                                                                                                     0.000/\text{rms}=563.00
S [V/A]: +0.000e+000 +0.000e+000 +3.963e+001 +7.374e+001 +1.138e+002
+1.527e+002 +1.767e+002 +1.927e+002 +2.081e+002 +2.185e+002 +2.191e+002 +2.141e+002 +2.035e+002 +1.893e+002 +1.783e+002 +1.702e+002 +1.618e+002 +1.533e+002 +1.463e+002 +1.397e+002 +1.305e+002 +1.184e+002 +1.073e+002 +9.744e+001 +8.516e+001 +7.129e+001 +6.075e+001 +5.249e+001 +4.356e+001
+3.494e+001 +2.905e+001 +2.482e+001 +2.051e+001 +1.650e+001 +1.381e+001
+1.187e+001
                 +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.880e-001
Err[V/A]:
+7.570e-001 +5.760e-001 +4.520e-001 +3.110e-001 +1.090e-001 -7.600e-002
-2.000e-001 -2.810e-001 -3.070e-001 -2.960e-001 -2.750e-001 -2.530e-001 -2.500e-001 -2.720e-001 -3.080e-001 -3.590e-001 -4.110e-001 -4.450e-001 -4.650e-001 -4.810e-001 -4.910e-001 -4.950e-001 -4.960e-001 -4.970e-001 -4.980e-001 -4.980e-001 -4.980e-001 -4.970e-001
-4.970e-001
   44.0755
                       2.80
 250,0000
                      63.32
```

```
1D_Inversion_Results_TEM.txt
                       31.39
   18.8613
     6.0360
                        6.15
     1.0000 10000000000.00
<Date: Thu Jul 17 14:35:08 2008</pre>
<Time Range=6 Currrent= 2.80 Stack= 5 Filter=50 Deff=
                                                                                             6 Ampl=OFF
<Remark: EAST OF PANORMOS</pre>
<Place: PANORMOS
<***************************
*****
#GEOSEC: 0219-A / 50.0/ 50.0/ 1.0 93.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                 1.0/ 563791.000/ 3919413.000/
                                                                            0.000 DH =
                                                                                                        0.000/\text{rms}=920.00
S [V/A]: +0.000e+000 +0.000e+000 +2.901e+001 +5.563e+001 +8.332e+001 +1.084e+002 +1.243e+002 +1.362e+002 +1.503e+002 +1.667e+002 +1.798e+002
+1.897e+002 +1.997e+002 +2.082e+002 +2.132e+002 +2.166e+002 +2.204e+002 +2.249e+002 +2.292e+002 +2.332e+002 +2.384e+002 +2.439e+002 +2.470e+002 +2.479e+002 +2.456e+002 +2.371e+002 +2.253e+002 +2.122e+002 +1.940e+002
+1.726e+002 +1.561e+002 +1.433e+002
                 +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.790e-001
Err[V/A]:
+7.220e-001 +5.720e-001 +5.040e-001 +4.640e-001 +4.220e-001 +3.700e-001 +3.130e-001 +2.380e-001 +1.640e-001 +1.210e-001 +1.020e-001 +9.700e-002
+1.040e-001 +1.150e-001 +1.210e-001 +1.160e-001 +9.100e-002 +4.800e-002
-1.000e-002 -1.060e-001 -2.310e-001 -3.210e-001 -3.750e-001 -4.140e-001 -4.320e-001 -4.340e-001 -4.320e-001
   69.9391
                        6.73
  250.0000
                     100.00
  200.0000
                       90.88
    27.3907
                       62.61
     3.1627 10000000000.00
 <Date: Thu Jul 17 15:05:23 2008
<Time Range=5 Currrent= 2.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                            6 Ampl=OFF
<Remark: EAST OF PANORMOS, ON HILLS</pre>
*****
                                                              1.0/ 563992.000/ 3919444.000/
#GEOSEC: 0220-C / 50.0/ 50.0/ 1. 76.0/40/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                            0.000 DH =
                                                                                                        0.000/\text{rms}=428.00
76.0/40/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/Fr S [V/A]: +0.000e+000 +0.000e+000 +1.598e+001 +4.191e+001 +6.771e+001 +9.211e+001 +1.093e+002 +1.223e+002 +1.360e+002 +1.473e+002 +1.522e+002 +1.533e+002 +1.518e+002 +1.477e+002 +1.430e+002 +1.383e+002 +1.317e+002 +1.231e+002 +1.152e+002 +1.078e+002 +9.836e+001 +8.710e+001 +7.782e+001 +7.013e+001 +6.123e+001 +5.187e+001 +4.515e+001 +4.009e+001 +3.484e+001 +3.001e+001 +2.694e+001 +2.491e+001 +2.311e+001 +2.186e+001 +2.142e+001 +2.142e+001 +2.142e+001 +2.234e+001 +2.242e+001 +2.175e+001 Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.940e-001 +7.920e-001 +6.670e-001 +5.700e-001 +4.400e-001 +2.610e-001 +1.090e-001
+7.920e-001 +6.670e-001 +5.700e-001 +4.400e-001 +2.610e-001 +1.090e-001 +3.000e-003 -8.900e-002 -1.580e-001 -2.000e-001 -2.320e-001 -2.720e-001 -3.190e-001 -3.580e-001 -3.880e-001 -4.200e-001 -4.460e-001 -4.620e-001 -4.710e-001 -4.780e-001 -4.820e-001 -4.830e-001 -4.810e-001 -4.750e-001
-4.590e-001 -4.320e-001 -3.920e-001 -3.150e-001 -1.830e-001 -5.600e-002
+4.200e-002 +1.090e-001 +6.800e-002 -1.030e-001 -2.870e-001
    52.7544
                        7.18
  250.0000
                       56.24
    22.6852
                       44.87
      3.5293
                       20.87
    50.0000 10000000000.00
<Date: Fri Jul 18 07:27:35 2008</pre>
<Time Range=7 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                             6 Ampl=OFF
<Remark: EAST OF PANORMOS, ON HILLS</pre>
<Place: PANORMOS
*****
#GEOSEC: 0221-B / 50.0/ 50.0/ 1.
75.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                 1.0/ 564214.000/ 3919455.000/
                                                                                                        0.000/rms=549.00
                                                                             0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +2.035e+001 +4.471e+001 +7.017e+001 +9.579e+001 +1.138e+002 +1.264e+002 +1.380e+002 +1.460e+002 +1.493e+002 +1.509e+002 +1.528e+002 +1.560e+002 +1.598e+002 +1.635e+002 +1.680e+002 +1.714e+002 +1.716e+002 +1.631e+002 +1.527e+002 +1.427e+002
+1.342e+002 +1.245e+002 +1.150e+002 +1.086e+002 +1.038e+002 +9.852e+001
                                                          Σελίδα 79
```

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1D_Inversion_Results_TEM.txt
+9.280e+001 +8.815e+001 +8.424e+001 +7.949e+001 +7.363e+001 +6.781e+001
+6.167e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.910e-001
+7.960e-001 +6.550e-001 +5.200e-001 +3.520e-001 +1.850e-001 +9.700e-002
+7.000e-002 +8.100e-002 +1.200e-001 +1.480e-001 +1.530e-001 +1.250e-001 +4.700e-002 -5.000e-002 -1.430e-001 -2.430e-001 -3.200e-001 -3.510e-001 -3.580e-001 -3.470e-001 -3.190e-001 -2.940e-001 -2.780e-001 -2.700e-001 -2.740e-001 -2.820e-001 -2.910e-001 -3.120e-001 -3.650e-001 -4.300e-001
-4.710e-001
 53.5079
250.0000
                     6.85
                    78.10
   77.8790
                    61.37
   77.8790
                     4.00
   35.2402 10000000000.00
<Date: Fri Jul 18 08:09:49 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: WEST OF SKEPASTI, ON HILLS
                                                                                6 Ampl=OFF
<Place: SKEPASTI
<********************************
#GEOSEC: 0222-C
#GEOSEC: 0222-C / 50.0/ 50.0/ 1
67.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 564371.000/ 3919535.000/
                                                                    0.000 DH =
                                                                                          0.000/\text{rms}=342.00
S [V/A]: +0.000e+000 +0.000e+000 +3.172e+001 +5.669e+001 +8.289e+001 +1.074e+002 +1.229e+002 +1.331e+002 +1.426e+002 +1.507e+002 +1.559e+002 +1.595e+002 +1.629e+002 +1.653e+002 +1.656e+002 +1.646e+002 +1.618e+002
+1.574e+002 +1.533e+002 +1.499e+002 +1.459e+002 +1.412e+002 +1.369e+002 +1.326e+002 +1.268e+002 +1.197e+002 +1.142e+002 +1.100e+002 +1.057e+002
+1.018e+002 +9.923e+001 +9.712e+001 +9.405e+001 +8.884e+001 +8.261e+001
+7.590e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.720e-001
+7.150e-001 +5.400e-001 +4.150e-001 +3.040e-001 +2.170e-001 +1.680e-001
+1.340e-001 +9.300e-002 +3.700e-002 -1.800e-002 -6.500e-002 -1.120e-001 -1.420e-001 -1.500e-001 -1.490e-001 -1.510e-001 -1.680e-001 -1.950e-001 -2.220e-001 -2.470e-001 -2.580e-001 -2.510e-001 -2.310e-001 -1.980e-001
-1.620e-001 -1.470e-001 -1.600e-001 -2.160e-001 -3.190e-001 -4.040e-001
-4.540e-001
   41.0808
                     4.38
 250.0000
                    71.35
   80.6436
                  100.00
   50.0000
                  100.00
   39.7391 1000000000.00
<Date: Fri Jul 18 08:35:54 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                6 Ampl=OFF
<Remark: WEST OF SKEPASTI, ON HILLS</pre>
#GEOSEC: 0223-B
                                  50.0/ 50.0/
                                                        1.0/ 564606.000/ 3919664.000/
93.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                    0.000 DH =
                                                                                          0.000/\text{rms}=760.00
    [V/A]:
               +0.000e+000 +0.000e+000 +4.423e+000 +2.118e+001 +3.426e+001
+4.349e+001 +4.950e+001 +5.456e+001 +6.131e+001 +7.019e+001 +7.857e+001
+8.641e+001 +9.668e+001 +1.089e+002 +1.189e+002 +1.267e+002 +1.348e+002
+1.414e+002 +1.444e+002 +1.449e+002 +1.432e+002 +1.389e+002 +1.343e+002
+1.304e+002 +1.263e+002 +1.232e+002 +1.222e+002 +1.223e+002 +1.230e+002 +1.229e+002 +1.212e+002 +1.182e+002 +1.135e+002 +1.081e+002 +1.050e+002
+1.040e+002
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.880e-001
Err[V/A]:
+6.880e-001 +5.740e-001 +5.500e-001 +5.530e-001 +5.600e-001 +5.620e-001 +5.560e-001 +5.340e-001 +4.900e-001 +4.350e-001 +3.740e-001 +2.860e-001 +1.700e-001 +6.900e-002 -1.500e-002 -1.030e-001 -1.710e-001 -1.940e-001 -1.880e-001 -1.490e-001 -1.890e-001 -1.800e-002 +1.500e-002 -1.800e-002 +1.500e-002 +1.500e-002
-4.700e-002 -1.290e-001 -1.900e-001 -2.220e-001 -1.940e-001 -1.140e-001
-1.900e-002
   32.5550
 250.0000
                  100.00
   91.2782
                  100.00
   50.0000
                  100.00
   43.3882 10000000000.00
```

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1D_Inversion_Results_TEM.txt
<Date: Fri Jul 18 09:13:18 2008</pre>
<Time Range=6 Currrent= 3.40 Stack= 5 Filter=50 Deff=
<Remark: NW OF SKEPASTI, ON HILLS</pre>
                                                                                 6 Ampl=OFF
<Place: SKEPASTI
*****
                                                       1.0/ 564795.000/ 3919601.000/
#GEOSEC: 0224-B / 50.0/ 50.0/ 1.88.0/36/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                          0.000/rms=431.00
                                                                   0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +1.620e+001 +3.022e+001 +4.288e+001
+5.286e+001 +5.808e+001 +6.092e+001 +6.327e+001 +6.560e+001 +6.792e+001 +7.047e+001 +7.442e+001 +7.999e+001 +8.511e+001 +8.925e+001 +9.332e+001
+9.578e+001 +9.587e+001 +9.489e+001 +9.294e+001 +9.046e+001 +8.869e+001
+8.761e+001 +8.701e+001 +8.751e+001 +8.892e+001 +9.079e+001 +9.361e+001
+9.688e+001 +9.879e+001 +9.938e+001 +9.864e+001 +9.628e+001 +9.386e+001
+9.202e+001
Err[V/A]:
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.470e-001
+5.960e-001 +3.760e-001 +2.510e-001 +1.820e-001 +1.810e-001 +2.190e-001
+2.630e-001 +3.100e-001 +3.380e-001 +3.260e-001 +2.820e-001 +1.890e-001 +6.000e-002 -3.600e-002 -9.100e-002 -1.220e-001 -1.210e-001 -9.800e-002 -6.400e-002 -8.000e-003 +6.500e-002 +1.210e-001 +1.560e-001 +1.690e-001 +1.390e-001 +7.500e-002 +4.000e-003 -7.700e-002 -1.340e-001 -1.400e-001
-1.290e-001
   45.6021
                    12.08
155.3427 34.87
93.9233 10000000000.00
<Date: Fri Jul 18 10:06:30 2008
<Time Range=6 Currrent= 3.10 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: NW OF SKEPASTI, ON HILLS</pre>
<Place: SKEPASTI
<***************************
*****
#GEOSEC: 0225-B / 50.0/ 50.0/ 1.0/ 565023.000/ 3919572.000/ 82.0/36/3/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/6 S [V/A]: +0.000e+000 +7.723e+000 +3.578e+001 +5.334e+001 +6.810e+001
                                                                                          0.000/\text{rms}=554.00
+7.868e+001 +8.450e+001 +8.839e+001 +9.251e+001 +9.664e+001 +9.957e+001
+1.017e+002 +1.037e+002 +1.049e+002 +1.049e+002 +1.040e+002 +1.020e+002 +9.897e+001 +9.632e+001 +9.422e+001 +9.205e+001 +9.012e+001 +8.890e+001 +8.807e+001 +8.730e+001 +8.684e+001 +8.697e+001 +8.758e+001 +8.910e+001
+9.199e+001 +9.512e+001 +9.792e+001 +1.005e+002 +1.006e+002 +9.712e+001
+9.181e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.910e-001 +7.260e-001 +4.560e-001 +3.180e-001 +2.590e-001 +2.190e-001 +1.820e-001 +1.510e-001 +1.240e-001 +8.300e-002 +2.400e-002 -3.200e-002 -7.900e-002 -1.240e-001
-1.500e-001 -1.510e-001 -1.390e-001 -1.160e-001 -9.000e-002 -7.100e-002 -5.800e-002 -3.800e-002 -7.000e-003 +3.000e-002 +7.000e-002 +1.240e-001 +1.770e-001 +1.970e-001 +1.760e-001 +8.100e-002 -1.110e-001 -2.790e-001
-3.850e-001
   50.9069
                     8.87
                    21.10
 250.0000
   87.0703 100000000000000000
<Date: Fri Jul 18 10:43:52 2008</pre>
<Time Range=6 Currrent= 3.00 Stack= 5 Filter=50 Deff=
                                                                                6 Ampl=OFF
<Remark: NW OF SKEPASTI, HILLS, FENCES</pre>
*****
#GEOSEC: 0226-B / 50.0/ 50.0/ 1.69.0/36/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                       1.0/ 565229.000/ 3919588.000/
                                                                                          0.000/\text{rms}=231.00
                                                                   0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +7.000e+000 +2.134e+001 +3.043e+001 +3.485e+001 +3.690e+001 +3.847e+001 +4.056e+001 +4.330e+001 +4.581e+001
+4.805e+001 +5.085e+001 +5.394e+001 +5.631e+001 +5.805e+001 +5.981e+001
+6.131e+001 +6.214e+001 +6.259e+001 +6.288e+001 +6.292e+001 +6.266e+001 +6.213e+001 +6.097e+001 +5.869e+001 +5.610e+001 +5.351e+001 +5.016e+001 +4.648e+001 +4.379e+001 +4.179e+001 +3.962e+001 +3.716e+001 +3.476e+001
+3.220e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.170e-001
+4.080e-001 +2.760e-001 +2.640e-001 +2.820e-001 +3.010e-001 +3.070e-001
+3.040e-001 +2.890e-001 +2.570e-001 +2.210e-001 +1.870e-001 +1.440e-001
                                                  Σελίδα 81
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1D_Inversion_Results_TEM.txt
+9.700e-002 +6.300e-002 +3.900e-002 +1.500e-002 -1.200e-002 -4.200e-002 -7.900e-002 -1.400e-001 -2.190e-001 -2.750e-001 -3.070e-001 -3.240e-001
-3.190e-001 -3.020e-001 -2.850e-001 -2.810e-001 -3.170e-001 -3.820e-001
-4.350e-001
  26.2802
                 5.90
99.94
  73.5849
18.0192 10000000000.00
<Date: Fri Jul 18 11:52:07 2008
<Time Range=6 Currrent= 2.90 Stack= 5 Filter=50 Deff=
                                                                      6 Ampl=OFF
<Remark: NW OF SKEPASTI, FENCES</pre>
<Place: SKEPASTI
<
*****
#GEOSEC: 0227-B / 50.0/ 50.0/ 1.80.0/36/3/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 565429.000/ 3919631.000/
                                                          0.000 \text{ DH} =
                                                                              0.000/\text{rms}=571.00
   [V/A]: +0.000e+000 +0.000e+000 +7.030e-001 +1.760e+001 +3.213e+001
+4.310e+001 +5.051e+001 +5.663e+001 +6.422e+001 +7.304e+001 +8.005e+001
+8.552e+001 +9.135e+001 +9.651e+001 +9.924e+001 +1.002e+002 +9.986e+001
+9.782e+001 +9.551e+001 +9.350e+001 +9.125e+001 +8.899e+001 +8.718e+001 +8.545e+001 +8.288e+001 +7.906e+001 +7.528e+001 +7.169e+001 +6.714e+001
+6.207e+001 +5.830e+001 +5.547e+001 +5.244e+001 +4.905e+001 +4.572e+001
+4.205e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.980e-001 +7.710e-001 +6.540e-001 +6.040e-001 +5.610e-001 +5.030e-001 +4.430e-001 +3.840e-001 +3.060e-001 +2.040e-001 +1.090e-001 +2.800e-002 -5.700e-002
-1.200e-001 -1.400e-001 -1.390e-001 -1.280e-001 -1.200e-001 -1.280e-001 -1.500e-001 -1.910e-001 -2.460e-001 -2.870e-001 -3.130e-001 -3.300e-001
-3.290e-001 -3.150e-001 -2.990e-001 -2.920e-001 -3.290e-001 -4.000e-001
-4.530e-001
    7.0089
                 85.61
 148.0112
  32.2245\ 1000000000000000000000
<Date: Fri Jul 18 12:22:39 2008
<Time Range=6 Currrent= 2.60 Stack= 5 Filter=50 Deff=</pre>
                                                                      6 Ampl=OFF
<Remark: NORTH OF SKEPASTI, FENCES</pre>
<Place: SKEPASTI
<****************************
#GEOSEC: 0228-B
                           / 50.0/ 50.0/
                                               1.0/ 565614.000/ 3919551.000/
74.0/36/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                           0.000 DH =
                                                                              0.000/\text{rms}=139.00
             +0.000e+000 +0.000e+000 +0.000e+000 +6.443e+000 +1.449e+001
+2.098e+001 +2.539e+001 +2.897e+001 +3.334e+001 +3.864e+001 +4.325e+001 +4.727e+001 +5.200e+001 +5.660e+001 +5.931e+001 +6.062e+001 +6.101e+001
+6.015e+001 +5.875e+001 +5.725e+001 +5.520e+001 +5.268e+001 +5.051e+001
+4.861e+001 +4.628e+001 +4.363e+001 +4.158e+001 +3.992e+001 +3.805e+001
+3.610e+001 +3.463e+001 +3.346e+001 +3.211e+001 +3.066e+001 +2.956e+001
+2.872e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.380e-001 +7.240e-001 +6.610e-001 +6.150e-001 +5.780e-001 +5.460e-001
+5.090e-001 +4.370e-001 +3.200e-001 +2.010e-001 +9.800e-002 -1.300e-002 -1.050e-001 -1.560e-001 -1.830e-001 -2.060e-001 -2.260e-001 -2.410e-001 -2.510e-001 -2.60e-001 -2.60e-001 -2.570e-001 -2.480e-001
-2.360e-001 -2.280e-001 -2.230e-001 -2.190e-001 -2.110e-001 -1.980e-001
-1.840e-001
                 1.37
57.63
    5.6921
 102.3357
  21.0980 10000000000.00
<Date: Fri Jul 18 13:01:46 2008</pre>
<Time Range=6 Currrent= 2.60 Stack= 5 Filter=50 Deff=
                                                                      6 Ampl=OFF
<Remark: NORTH OF SKEPASTI, FENCES</pre>
#GEOSEC: 0229-B
                           / 50.0/ 50.0/ 1.0/ 565911.000/ 3919527.000/
106.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                            0.000 DH =
0.000/\text{rms}=238.00
             +0.000e+000 +0.000e+000 +9.625e+000 +2.905e+001 +4.732e+001
S [V/A]:
+6.437e+001 +7.671e+001 +8.609e+001 +9.553e+001 +1.022e+002 +1.040e+002
                                            Σελίδα 82
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```
1D_Inversion_Results_TEM.txt
+1.034e+002 +1.011e+002 +9.766e+001 +9.450e+001 +9.171e+001 +8.813e+001 +8.387e+001 +8.029e+001 +7.719e+001 +7.330e+001 +6.861e+001 +6.461e+001 +6.124e+001 +5.742e+001 +5.374e+001 +5.151e+001 +5.018e+001 +4.926e+001
+4.895e+001 +4.907e+001 +4.922e+001 +4.919e+001 +4.867e+001 +4.787e+001
+4.709e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.940e-001 +7.960e-001 +6.780e-001 +5.730e-001 +4.130e-001 +1.920e-001 +2.400e-002
-7.500e-002 -1.400e-001 -1.740e-001 -1.900e-001 -2.030e-001 -2.180e-001
-2.340e-001 -2.460e-001 -2.590e-001 -2.790e-001 -3.040e-001 -3.200e-001 -3.220e-001 -3.070e-001 -2.620e-001 -2.040e-001 -1.440e-001 -7.000e-002 -6.000e-003 +1.800e-002 +1.000e-002 -2.600e-002 -7.700e-002 -1.050e-001
-1.190e-001
                    1.00
    6.9412
 250.0000
                  41.16
   40.1374
                   69.16
  11.7919
                   11.59
  66.4156 10000000000.00
<Date: Fri Jul 18 13:38:25 2008
<Time Range=6 Currrent= 2.40 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: NE OF SKEPASTI, FENCES</pre>
<Place: SKEPASTI
*****
#GEOSEC: 0230-C / 50.0/ 50.0/ 1.
97.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/
                                                           565966.000/ 3918980.000/
                                                               0.000 DH=
                                                                                     0.000/rms=348.00
              +0.000e+000 +0.000e+000 +2.113e+001 +3.545e+001 +4.523e+001
S [V/A]:
+5.126e+001 +5.496e+001 +5.822e+001 +6.268e+001 +6.861e+001 +7.393e+001
+7.859e+001 +8.405e+001 +8.954e+001 +9.314e+001 +9.537e+001 +9.704e+001 +9.758e+001 +9.700e+001 +9.594e+001 +9.423e+001 +9.215e+001 +9.058e+001
+8.928e+001 +8.733e+001 +8.363e+001 +7.876e+001 +7.314e+001 +6.499e+001
+5.511e+001 +4.739e+001 +4.143e+001 +3.500e+001 +2.862e+001 +2.405e+001
+2.056e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +7.070e-001 +4.210e-001 +3.530e-001 +3.600e-001 +3.830e-001 +3.970e-001 +3.920e-001
+3.710e-001 +3.250e-001 +2.550e-001 +1.890e-001 +1.310e-001 +6.400e-002
-7.000e-003 -5.600e-002 -8.600e-002 -1.040e-001 -1.040e-001 -1.000e-001 -1.090e-001 -1.600e-001 -2.680e-001 -3.680e-001 -4.310e-001 -4.700e-001 -4.860e-001 -4.910e-001 -4.930e-001 -4.940e-001 -4.960e-001 -4.970e-001
-4.980e-001
 7.8574
126.1336
                    1.05
                  55.15
41.99
   64.1192
   12.0879
                   39.68
    1.0000 10000000000.00
<Date: Fri Jul 18 14:30:15 2008</pre>
<Time Range=6 Currrent= 2.40 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: NE OF SKEPASTI, FENCES</pre>
<Place: SKEPASTI
*****
#GEOSEC: 0231
                                50.0/
                                          50.0/
                                                     1.0/ 565039.000/ 3918947.000/
60.0/32/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                     0.000/\text{rms}=354.00
S [V/A]: +9.827e+000 +2.479e+001 +3.566e+001 +4.347e+001 +5.113e+001
+5.749e+001 +6.095e+001 +6.295e+001 +6.474e+001 +6.643e+001 +6.752e+001 +6.792e+001 +6.715e+001 +6.406e+001 +5.980e+001 +5.550e+001 +4.992e+001 +4.371e+001 +3.902e+001 +3.540e+001 +3.145e+001 +2.754e+001 +2.479e+001
+2.276e+001 +2.061e+001 +1.848e+001 +1.692e+001 +1.564e+001 +1.405e+001
+1.210e+001 +1.042e+001 +9.001e+000
Err[V/A]: -9.000e-001 -9.000e-001 -8.600e-001 -7.490e-001 +5.780e-001 +3.800e-001 +2.480e-001 +1.770e-001 +1.340e-001 +1.040e-001 +6.300e-002
-7.000e-003 -1.360e-001 -2.880e-001 -3.760e-001 -4.170e-001 -4.410e-001
-4.530e-001 -4.560e-001 -4.560e-001 -4.530e-001 -4.460e-001 -4.380e-001
-4.290e-001 -4.170e-001 -4.090e-001 -4.130e-001 -4.280e-001 -4.550e-001
-4.820e-001 -4.930e-001 -4.980e-001
   54.7952
                  41.08
                   27.58
    3.6851
    1.0000 10000000000.00
<Date: Fri Jul 18 15:12:13 2008</pre>
```

```
1D_Inversion_Results_TEM.txt
<Time Range=5 Currrent= 1.90 Stack= 5 Filter=50 Deff= <Remark: NEXT TO NATIONAL ROAD
                                                                                                                                   6 Ampl=OFF
<Place: SKEPASTI
 ******
#GEOSEC: 0243 / 50.0/ 50.0/ 1. 88.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                           1.0/ 567736.000/ 3917789.000/
                                                                                                            0.000 DH =
                                                                                                                                                   0.000/\text{rms}=734.00
S [V/A]: +2.001e+001 +8.054e+001 +1.376e+002 +1.991e+002 +2.870e+002 +3.809e+002 +4.340e+002 +4.654e+002 +4.971e+002 +5.278e+002 +5.416e+002
+5.397e+002 +5.198e+002 +4.814e+002 +4.456e+002 +4.171e+002 +3.861e+002 +3.556e+002 +3.325e+002 +3.125e+002 +2.862e+002 +2.530e+002 +2.245e+002 +2.008e+002 +1.741e+002 +1.475e+002 +1.293e+002 +1.159e+002 +1.016e+002
+8.722e+001 +7.617e+001 +6.705e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.990e-001 -8.960e-001 +8.730e-001 +7.300e-001 +5.080e-001 +3.810e-001 +3.050e-001 +2.020e-001 +5.400e-002 -1.040e-001 -2.600e-001 -3.490e-001 -3.710e-001 -3.680e-001 -3.520e-001
-3.410e-001 -3.500e-001 -3.760e-001 -4.160e-001 -4.540e-001 -4.710e-001
-4.780e-001 -4.810e-001 -4.790e-001 -4.760e-001 -4.730e-001 -4.720e-001
 -4.770e-001 -4.850e-001 -4.910e-001
  185.7845
                                12.04
                                95.81
  800.0001
     48.3508
                                60.30
       8.3750 10000000000.00
<Date: Wed Aug 27 08:55:35 2008
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                                   6 Ampl=OFF
<Remark: PHYLLITES</pre>
<Place: EXADIS
 1.0/ 567678.000/ 3917554.000/
#GEOSEC: 0244-C
                                                     50.0/ 50.0/
99.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/r S [V/A]: +3.557e+002 +3.578e+002 +3.815e+002 +4.177e+002 +4.832e+002 +5.868e+002 +6.858e+002 +7.632e+002 +8.266e+002 +8.458e+002 +8.305e+002 +8.073e+002 +7.749e+002 +7.341e+002 +6.36e+002 +6.525e+002 +5.936e+002 +5.936e+002 +6.858e+002 +7.341e+002 +6.334e+002 +6.352e+002 +7.341e+002 +6.334e+002 +6.34e+002 +6.34e+
                                                                                                                                                   0.000/\text{rms}=822.00
+5.180e+002 +4.531e+002 +3.981e+002 +3.334e+002 +2.650e+002 +2.155e+002
+1.794e+002 +1.427e+002 +1.096e+002 +8.871e+001 +7.422e+001 +5.991e+001
+4.700e+001 +3.847e+001 +3.239e+001 +2.615e+001 +2.028e+001 +1.633e+001
+1.352e+001
Err[V/A]:
                        +1.350e-001 -1.790e-001 -4.010e-001 -5.440e-001 +6.490e-001
+6.840e-001 +6.350e-001 +5.110e-001 +2.670e-001 -9.000e-003 -1.460e-001 -1.960e-001 -2.270e-001 -2.710e-001 -3.280e-001 -3.810e-001 -4.330e-001 -4.690e-001 -4.850e-001 -4.920e-001 -4.970e-001 -4.990e-001 -4.990e-001 -5.000e-001 -5.000e-001 -5.000e-001 -4.990e-001 -4.990e-001 -4.990e-001
 -4.990e-001 -4.990e-001 -4.990e-001 -4.990e-001 -5.000e-001 -5.000e-001
-5.000e-001
  144.8709
800.0001
                                  2.39
                              125.41
     35.0405
                                36.26
       2.9131 10000000000.00
<Date: Wed Aug 27 09:36:59 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                                   6 Ampl=OFF
<Remark: POWER-LINES, PHYLLITES</pre>
<Place: EXADIS</pre>
 #GEOSEC: 0245-B / 50.0/ 50.0/ 1.0/ 566897.000/ 3916920.000/ 78.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=1083.00
S [V/A]: +1.648e+002 +2.503e+002 +3.545e+002 +4.804e+002 +6.896e+002 +9.923e+002 +1.242e+003 +1.405e+003 +1.503e+003 +1.477e+003 +1.377e+003
+1.266e+003 +1.124e+003 +9.710e+002 +8.585e+002 +7.752e+002 +6.867e+002 +6.002e+002 +5.372e+002 +4.868e+002 +4.270e+002 +3.596e+002 +3.067e+002
+2.654e+002 +2.212e+002 +1.793e+002 +1.518e+002 +1.321e+002 +1.119e+002 +9.269e+001 +7.919e+001 +6.905e+001 +5.819e+001 +4.756e+001 +4.019e+001
+3.481e+001
Err[V/A]: -8.720e-001 -8.820e-001 -8.870e-001 -8.900e-001 +8.860e-001 +8.540e-001 +7.460e-001 +5.310e-001 +1.500e-001 -2.390e-001 -3.900e-001 -4.370e-001 -4.570e-001 -4.640e-001 -4.630e-001 -4.600e-001 -4.550e-001
```

```
1D_Inversion_Results_TEM.txt
-4.520e-001 -4.550e-001 -4.640e-001 -4.780e-001 -4.900e-001 -4.940e-001 -4.960e-001 -4.960e-001 -4.960e-001 -4.950e-001 -4.950e-001 -4.950e-001 -4.950e-001 -4.950e-001
-4.950e-001
981.1902
1000.0001
                    85.86
                    51.61
   16.7784
                    33.33
    2.6332 10000000000.00
<Date: Wed Aug 27 10:05:33 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                 6 Ampl=OFF
<Remark: POWER-LINES, NEXT TO G-05</pre>
<Place: EXADIS
*****
#GEOSEC: 0246-B / 50.0/ 50.0/ 1.0 68.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 566799.000/ 3917110.000/
                                                                   0.000 DH=
                                                                                           0.000/rms=467.00
S [V/A]: +8.037e+001 +1.534e+002 +2.351e+002 +3.267e+002 +4.538e+002 +5.719e+002 +6.220e+002 +6.394e+002 +6.413e+002 +6.207e+002 +5.861e+002
+5.479e+002 +4.968e+002 +4.398e+002 +3.967e+002 +3.642e+002 +3.290e+002 +2.934e+002 +2.663e+002 +2.443e+002 +2.177e+002 +1.877e+002 +1.638e+002 +1.445e+002 +1.229e+002 +1.010e+002 +8.564e+001 +7.408e+001 +6.180e+001 +4.990e+001 +4.168e+001 +3.571e+001 +2.961e+001 +2.401e+001 +2.036e+001
+1.785e+001
Err[V/A]: -9.000e-001 -8.990e-001 -8.960e-001 -8.900e-001 +8.450e-001 +6.040e-001 +2.910e-001 +1.020e-001 -6.200e-002 -2.310e-001 -3.380e-001
-3.910e-001 -4.220e-001 -4.330e-001 -4.320e-001 -4.280e-001 -4.230e-001
-4.230e-001 -4.300e-001 -4.420e-001 -4.590e-001 -4.760e-001 -4.850e-001
-4.890e-001 -4.920e-001 -4.940e-001 -4.950e-001 -4.960e-001 -4.970e-001 -4.970e-001 -4.970e-001 -4.970e-001 -4.930e-001
-4.890e-001
                    21.12
 600.0001
 400.0000
                    72.69
                    29.26
   11.6683
    1.0065 10000000000.00
<Date: Wed Aug 27 10:31:20_2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                 6 Ampl=OFF
<Remark: NEAR TO G-05
<Place: EXADIS
<***************
*****
#GEOSEC: 0247-C / 50.0 / 50.0 1. 67.0 / 36 / 4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 566886.000/ 3917313.000/
                                                                  0.000 DH =
                                                                                           0.000/\text{rms}=406.00
    [V/A]: +0.000e+000 +0.000e+000 +1.177e+001 +3.345e+001 +5.161e+001
+6.553e+001 +7.480e+001 +8.254e+001 +9.236e+001 +1.039e+002 +1.130e+002
+1.204e+002 +1.293e+002 +1.406e+002 +1.519e+002 +1.631e+002 +1.789e+002 +1.982e+002 +2.123e+002 +2.204e+002 +2.234e+002 +2.181e+002 +2.090e+002 +1.995e+002 +1.864e+002 +1.687e+002 +1.523e+002 +1.373e+002 +1.189e+002 +9.942e+001 +8.525e+001 +7.463e+001 +6.327e+001 +5.187e+001 +4.350e+001
+3.700e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.810e-001 +6.920e-001 +5.810e-001 +5.460e-001 +5.160e-001 +4.680e-001 +4.190e-001
+3.870e-001 +3.780e-001 +4.010e-001 +4.360e-001 +4.620e-001 +4.680e-001
+4.180e-001 +3.130e-001 +1.740e-001 -1.400e-002 -1.830e-001 -2.650e-001 -3.110e-001 -3.620e-001 -4.200e-001 -4.560e-001 -4.740e-001 -4.850e-001 -4.900e-001 -4.910e-001 -4.920e-001 -4.930e-001 -4.960e-001 -4.980e-001
-4.990e-001
18.7771
                     2.91
 262.5205
7.2530
                  143.98
                    35.78
    1.0658 10000000000.00
<Date: Wed Aug 27 11:06:08 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                 6 Ampl=OFF
<Remark: NEAR TO G-80
<Place: EXADIS</pre>
*****
                               / 50.0/ 50.0/ 1.0/ 566949.000/ 3917435.000/
#GEOSEC: 0248-B
68.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                    0.000 \text{ DH} =
                                                                                          0.000/\text{rms}=695.00
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +0.000e+000 +1.756e+000 +6.161e+000 +1.158e+001 +1.720e+001 +2.143e+001 +2.486e+001 +2.920e+001 +3.479e+001 +4.019e+001 +4.551e+001 +5.308e+001 +6.338e+001 +7.340e+001 +8.289e+001 +9.579e+001
+1.117e+002 +1.243e+002 +1.329e+002 +1.389e+002 +1.395e+002 +1.362e+002
+1.322e+002 +1.265e+002 +1.192e+002 +1.122e+002 +1.052e+002 +9.547e+001 +8.353e+001 +7.380e+001 +6.596e+001 +5.714e+001 +4.791e+001 +4.089e+001
+3.528e+001
Err[V/A]:
                +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +9.000e-001
+8.610e-001 +7.750e-001 +7.150e-001 +6.810e-001 +6.710e-001 +6.750e-001
+6.820e-001 +6.880e-001 +6.890e-001 +6.840e-001 +6.750e-001 +6.520e-001 +5.920e-001 +4.910e-001 +3.510e-001 +1.420e-001 -6.700e-002 -1.710e-001 -2.140e-001 -2.480e-001 -2.970e-001 -3.480e-001 -3.940e-001 -4.360e-001 -4.630e-001 -4.740e-001 -4.800e-001 -4.850e-001 -4.900e-001 -4.950e-001
-4.970e-001
   26.4239
                     11.03
 400.0000
                   119.78
    8.4665
                     51.10
     1.0330 10000000000.00
<Date: Wed Aug 27 11:28:43 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                      6 Ampl=OFF
<Remark: NORTH TO G-80</pre>
<Place: EXADIS</pre>
*****
                                    50.0/ 50.0/
#GEOSEC: 0249-A
                                                          1.0/ 567137.000/ 3917552.000/
71.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                       0.000 DH=
                                                                                                0.000/rms=194.00
S [V/A]: +0.000e+000 +1.639e+001 +4.747e+001 +6.777e+001 +8.570e+001
+9.882e+001 +1.061e+002 +1.110e+002 +1.161e+002 +1.215e+002 +1.261e+002 +1.305e+002 +1.373e+002 +1.470e+002 +1.560e+002 +1.630e+002 +1.690e+002 +1.709e+002 +1.689e+002 +1.660e+002 +1.625e+002 +1.596e+002 +1.579e+002 +1.571e+002 +1.542e+002 +1.487e+002 +1.411e+002 +1.283e+002 +1.105e+002 +9.510e+001 +8.261e+001 +6.892e+001 +5.569e+001 +4.682e+001
+4.057e+001
Err[V/A]:
                -9.000e-001 -9.000e-001 -9.000e-001 -8.830e-001 +7.130e-001
+4.510e-001 +3.170e-001 +2.590e-001 +2.220e-001 +2.060e-001 +2.170e-001
+2.460e-001 +2.920e-001 +3.240e-001 +3.080e-001 +2.500e-001 +1.320e-001
-1.300e-002 -9.400e-002 -1.180e-001 -1.040e-001 -6.300e-002 -3.200e-002 -2.400e-002 -5.700e-002 -1.560e-001 -2.720e-001 -3.680e-001 -4.450e-001 -4.820e-001 -4.920e-001 -4.950e-001 -4.970e-001 -4.970e-001 -4.960e-001
-4.940e-001
   79.7008
                   12.87
107.41
66.52
 203.0022
   24.0545
     1.0000 10000000000.00
<Date: Wed Aug 27 11:51:12 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                      6 Ampl=OFF
<Remark: NORTH TO G-44
<Place: EXADIS
*****
#GEOSEC: 0250-A / 50.0/ 50.0/ 1.84.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 567121.000/ 3917807.000/
                                                                       0.000 DH =
                                                                                                0.000/\text{rms}=460.00
S [V/A]: +0.000e+000 +0.000e+000 +1.313e+001 +2.218e+001 +2.808e+001
+3.141e+001 +3.295e+001 +3.381e+001 +3.451e+001 +3.495e+001 +3.514e+001 +3.527e+001 +3.548e+001 +3.594e+001 +3.659e+001 +3.737e+001 +3.864e+001 +4.053e+001 +4.236e+001 +4.406e+001 +4.620e+001 +4.868e+001 +5.076e+001
+5.265e+001 +5.534e+001 +5.939e+001 +6.384e+001 +6.870e+001 +7.595e+001
+8.515e+001 +9.151e+001 +9.430e+001 +9.328e+001 +8.718e+001 +8.011e+001
+7.357e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +6.840e-001 +3.440e-001 +2.020e-001 +1.380e-001 +8.500e-002 +4.300e-002 +2.700e-002
+2.800e-002 +4.600e-002 +8.400e-002 +1.250e-001 +1.620e-001 +2.040e-001
+2.410e-001 +2.590e-001 +2.620e-001 +2.560e-001 +2.450e-001 +2.450e-001 +2.600e-001 +3.010e-001 +3.730e-001 +4.410e-001 +4.910e-001 +5.130e-001 +4.540e-001 +3.000e-001 +8.600e-002 -1.810e-001 -3.580e-001 -4.180e-001
-4.460e-001
   35.1746
                     34.93
                   198.25
 114.8141
```

```
1D_Inversion_Results_TEM.txt
 114.8141
                      32.88
     2.7831 100000000000.00
<Date: Wed Aug 27 12:15:04 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                         6 Ampl=OFF
<Remark: NORTH TO G-44</pre>
<Place: EXADIS</pre>
*****
#GEOSEC: 0251-B / 50.0/ 50.0/ 1.0/ 567384.000/ 3917818.000/ 94.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri S [V/A]: +1.082e+001 +7.574e+000 +7.692e+000 +8.785e+000 +1.067e+001 +1.301e+001 +1.476e+001 +1.608e+001 +1.749e+001 +1.900e+001 +2.026e+001
                                                                                                    0.000/\text{rms}=250.00
+2.142e+001 +2.306e+001 +2.529e+001 +2.756e+001 +2.977e+001 +3.285e+001
+3.685e+001 +4.038e+001 +4.342e+001 +4.704e+001 +5.104e+001 +5.432e+001 +5.730e+001 +6.144e+001 +6.723e+001 +7.289e+001 +7.842e+001 +8.590e+001 +9.502e+001 +1.021e+002 +1.068e+002 +1.089e+002 +1.036e+002 +9.314e+001
+8.158e+001
                +5.000e-001 +4.160e-001 -4.230e-001 -6.890e-001 +7.170e-001
Err[V/A]:
+6.400e-001 +5.410e-001 +4.620e-001 +3.930e-001 +3.570e-001 +3.520e-001 +3.670e-001 +3.990e-001 +4.400e-001 +4.720e-001 +4.910e-001 +5.040e-001
+4.980e-001 +4.760e-001 +4.450e-001 +4.030e-001 +3.640e-001 +3.530e-001
+3.630e-001 +3.930e-001 +4.330e-001 +4.600e-001 +4.720e-001 +4.680e-001 +4.300e-001 +3.500e-001 +2.160e-001 -5.600e-002 -3.750e-001 -4.780e-001
-4.970e-001
   18.2783
                      13.43
 129.2388
                    168.29
   61.7004
                      96.79
     1.3138 10000000000.00
<Date: Wed Aug 27 12:39:07 2008</pre>
<Time Range=6 Currrent= 3.60 Stack= 5 Filter=50 Deff=
                                                                                         6 Ampl=OFF
<Remark: NORTH TO G-40</pre>
******
                                                            1.0/ 567648.000/ 3917801.000/
                                     49.0/ 49.0/
87.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                    0.000/rms=771.00
                                                                         0.000 DH =
S [V/A]: +0.000e+000 +6.943e+000 +4.767e+001 +8.052e+001 +1.178e+002 +1.518e+002 +1.725e+002 +1.866e+002 +2.002e+002 +2.082e+002 +2.075e+002 +2.028e+002 +1.944e+002 +1.827e+002 +1.715e+002 +1.605e+002 +1.450e+002
+1.257e+002 +1.099e+002 +9.730e+001 +8.356e+001 +7.004e+001 +6.047e+001 +5.325e+001 +4.541e+001 +3.749e+001 +3.190e+001 +2.771e+001 +2.335e+001 +1.929e+001 +1.662e+001 +1.477e+001 +1.294e+001 +1.129e+001 +1.021e+001
+9.404e+000
                -9.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.710e-001
Err[V/A]:
+7.000e-001 +5.260e-001 +4.160e-001 +2.750e-001 +7.200e-002 -9.000e-002 -1.820e-001 -2.450e-001 -2.990e-001 -3.510e-001 -3.990e-001 -4.440e-001 -4.720e-001 -4.820e-001 -4.850e-001 -4.870e-001 -4.870e-001 -4.880e-001 -4.890e-001 -4.910e-001 -4.930e-001 -4.940e-001 -4.930e-001
-4.910e-001 -4.860e-001 -4.790e-001 -4.660e-001 -4.460e-001 -4.310e-001
-4.200e-001
   78.1320
                      10.21
 800.0001
                      34.30
   39.8814
                      30.53
     2.2333 10000000000.00
<Date: Wed Aug 27 14:11:17 2008
<Time Range=6 Currrent= 3.50 Stack= 5 Filter=50 Deff=</pre>
                                                                                         6 Ampl=OFF
<Remark: POWER-LINE, FENCES, NOT SQUARE</pre>
<Place: EXADIS
******
#GEOSEC: 0253-B
#GEOSEC: 0253-B / 50.0/ 50.0/ 1.0
84.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 567498.000/ 3917386.000/
                                                                         0.000 DH=
                                                                                                    0.000/rms=720.00
S [V/A]: +0.000e+000 +4.104e+001 +9.497e+001 +1.515e+002 +2.356e+002 +3.326e+002 +3.931e+002 +4.309e+002 +4.681e+002 +5.021e+002 +5.230e+002 +5.373e+002 +5.535e+002 +5.697e+002 +5.731e+002 +5.597e+002 +5.175e+002 +4.442e+002 +3.794e+002 +3.285e+002 +2.750e+002 +2.245e+002 +1.902e+002 +1.652e+002 +1.391e+002 +1.141e+002 +9.730e+001 +8.508e+001 +7.249e+001
```

Σελίδα 87

+6.057e+001 +5.226e+001 +4.597e+001 +3.903e+001 +3.179e+001 +2.637e+001

```
1D_Inversion_Results_TEM.txt
```

```
+2.220e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.930e-001 +8.100e-001 +6.200e-001 +4.770e-001 +3.660e-001 +2.660e-001 +2.000e-001
+1.700e-001 +1.500e-001 +8.100e-002 -7.200e-002 -2.630e-001 -4.290e-001 -4.850e-001 -4.940e-001 -4.950e-001 -4.950e-001 -4.950e-001 -4.910e-001 -4.900e-001 -4.900e-001 -4.990e-001 -4.880e-001 -4.890e-001 -4.910e-001 -4.940e-001 -4.990e-001
-4.990e-001
   70.6028
                      4.17
 800.0001
                     90.90
   72.9355
                     36.39
     3.3216 10000000000.00
<Date: Thu Aug 28 08:34:02 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                     6 Ampl=OFF
<Remark: POWER-LINES</pre>
<Place: EXADIS
******
#GEOSEC: 0254-B / 50.0/ 50.0/ 1.078.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                           1.0/ 567274.000/ 3917331.000/
                                                                                               0.000/rms=439.00
                                                                      0.000 \, DH =
S [V/A]: +0.000e+000 +3.496e+001 +8.232e+001 +1.251e+002 +1.754e+002 +2.166e+002 +2.355e+002 +2.457e+002 +2.544e+002 +2.584e+002 +2.551e+002
+2.100e+002 +2.335e+002 +2.437e+002 +2.544e+002 +2.554e+002 +2.351e+002 +2.475e+002 +2.346e+002 +2.187e+002 +2.071e+002 +1.993e+002 +1.919e+002 +1.854e+002 +1.800e+002 +1.744e+002 +1.655e+002 +1.524e+002 +1.398e+002 +1.285e+002 +1.144e+002 +9.825e+001 +8.562e+001 +7.530e+001 +6.361e+001
+5.171e+001 +4.324e+001 +3.700e+001 +3.050e+001 +2.432e+001 +2.009e+001
+1.700e+001
-2.280e-001 -2.840e-001 -2.920e-001 -2.640e-001 -2.260e-001 -1.830e-001
-1.650e-001 -1.890e-001 -2.370e-001 -3.080e-001 -3.780e-001 -4.180e-001 -4.420e-001 -4.620e-001 -4.780e-001 -4.870e-001 -4.910e-001 -4.950e-001 -4.970e-001 -4.970e-001 -4.980e-001 -4.980e-001 -4.980e-001 -4.990e-001
-4.990e-001
   37.8121
  340.4859
                     68.63
   28.3362
                     51.78
     1.0000 10000000000.00
<Date: Thu Aug 28 09:00:01 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: POWER-LINES, FENCES, NEXT G-44</pre>
******
                                 / 50.0/ 50.0/
                                                           1.0/ 567457.000/ 3917212.000/
#GEOSEC: 0255-B
100.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                         0.000 DH =
0.000/rms=552.00
     [V/A]:
               +5.882e+002 +5.503e+002 +5.479e+002 +5.627e+002 +5.988e+002
+6.616e+002 +7.255e+002 +7.815e+002 +8.406e+002 +8.807e+002 +8.865e+002
+8.748e+002 +8.455e+002 +7.959e+002 +7.418e+002 +6.884e+002 +6.173e+002 +5.356e+002 +4.734e+002 +4.258e+002 +3.744e+002 +3.235e+002 +2.870e+002 +2.593e+002 +2.294e+002 +1.992e+002 +1.775e+002 +1.603e+002 +1.407e+002 +1.192e+002 +1.023e+002 +8.871e+001 +7.347e+001 +5.829e+001 +4.786e+001
+4.042e+001
Err[V/A]: +3.290e-001 +1.190e-001 -7.400e-002 -2.180e-001 +3.490e-001 +4.350e-001 +4.480e-001 +4.080e-001 +2.960e-001 +1.170e-001 -3.100e-002
-1.300e-001 -2.220e-001 -3.120e-001 -3.780e-001 -4.200e-001 -4.500e-001
-4.650e-001 -4.680e-001 -4.680e-001 -4.670e-001 -4.650e-001 -4.640e-001 -4.620e-001 -4.610e-001 -4.610e-001 -4.630e-001 -4.670e-001 -4.670e-001 -4.760e-001 -4.870e-001 -4.930e-001 -4.960e-001 -4.980e-001 -4.990e-001 -4.990e-001
-4.990e-001
 436.3016
818.9946
                    14.50
                   127.20
55.00
   18.9373
     2.3563 10000000000.00
<Date: Thu Aug 28 09:28:49 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: POWER-LINES, NEAR ROAD</pre>
```

```
*****
                                                            / 50.0/ 50.0/ 1.0/ 567306.000/ 3917026.000/
#GEOSEC: 0256
104.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                                      0.000 DH =
0.000/\text{rms}=1071.00
                             +1.278e+002 +2.103e+002 +3.147e+002 +4.506e+002 +6.973e+002
+1.069e+003 +1.334e+003 +1.475e+003 +1.572e+003 +1.625e+003 +1.620e+003
+1.575e+003 +1.479e+003 +1.338e+003 +1.216e+003 +1.118e+003 +1.011e+003
+9.045e+002 +8.285e+002 +7.696e+002 +7.014e+002 +6.237e+002 +5.583e+002 +5.022e+002 +4.356e+002 +3.650e+002 +3.143e+002 +2.757e+002 +2.343e+002
+1.927e+002 +1.623e+002 +1.387e+002
Err[V/A]: -8.920e-001 -8.950e-001 -8.970e-001 -8.980e-001 +8.970e-001 +8.690e-001 +7.090e-001 +4.640e-001 +2.440e-001 +5.900e-002 -1.060e-001 -2.400e-001 -3.480e-001 -4.060e-001 -4.230e-001 -4.250e-001 -4.190e-001 -4.080e-001 -4.020e-001 -4.030e-001 -4.170e-001 -4.420e-001 -4.620e-001
-4.750e-001 -4.840e-001 -4.880e-001 -4.900e-001 -4.910e-001 -4.930e-001
-4.950e-001 -4.970e-001 -4.980e-001
431.4059
2000.0002
                                    13.46
161.80
      39.3190
                                      68.96
         2.4042 100000000000.00
<Date: Thu Aug 28 09:50:46 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff= <Remark: NORTH TO G-56, NEAR ROAD
                                                                                                                                                            6 Ampl=OFF
<Place: EXADIS
 *****
#GEOSEC: 0257 / 50.0/ 50.0/ 1.0/ 567157.000/ 3916729.000/ 90.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH=
0.000/\text{rms}=1481.00
S [V/A]: +2.025e+002 +2.730e+002 +3.554e+002 +4.513e+002 +6.088e+002 +8.538e+002 +1.087e+003 +1.251e+003 +1.323e+003 +1.221e+003 +1.073e+003 +9.483e+002 +8.201e+002 +7.085e+002 +6.403e+002 +5.968e+002 +5.562e+002
+5.198e+002 +4.917e+002 +4.649e+002 +4.257e+002 +3.726e+002 +3.263e+002 +2.884e+002 +2.468e+002 +2.065e+002 +1.797e+002 +1.602e+002 +1.400e+002
+1.198e+002 +1.046e+002 +9.204e+001

Err[V/A]: -7.700e-001 -8.190e-001 -8.460e-001 -8.600e-001 +8.670e-001

+8.540e-001 +7.830e-001 +5.540e-001 -1.600e-002 -4.260e-001 -4.770e-001
-4.810e-001 -4.730e-001 -4.470e-001 -4.090e-001 -3.670e-001 -3.190e-001 -2.950e-001 -3.170e-001 -3.640e-001 -4.250e-001 -4.680e-001 -4.830e-001 -4.870e-001 -4.880e-001 -4.850e-001 -4.810e-001 -4.780e-001 -4.750e-001 -4.750e-001 -4.750e-001 -4.750e-001 -4.750e-001
   956.2624
                                       97.47
   956.2624
60.5455
                                      31.30
74.77
         8.6447 10000000000.00
 <Date: Thu Aug 28 10:47:30 2008</pre>
 <Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                                                                                            6 Ampl=OFF
<Remark: SOUTH TO G-56, NEAR ROAD</pre>
 <Place: EXADIS
 <****************
*****
#GEOSEC: 0258-B / 50.0/ 50.0/ 1.0/ 566916.000/ 3916818.000/ 78.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/r S [V/A]: +3.508e+002 +3.197e+002 +3.100e+002 +3.100e+002 +3.180e+002 +3.354e+002 +3.508e+002 +3.707e+002 +3.883e+002 +4.000e+002 +4.000e+002 +3.838e+002 +4.000e+002 +3.838e+002 +4.000e+002 +3.838e+002 +3.838e+00
                                                                                                                                                                               0.000/rms=431.00
+3.948e+002 +3.813e+002 +3.596e+002 +3.377e+002 +3.177e+002 +2.928e+002 +2.654e+002 +2.450e+002 +2.295e+002 +2.125e+002 +1.949e+002 +1.811e+002 +1.692e+002 +1.543e+002 +1.364e+002 +1.216e+002 +1.091e+002 +9.442e+001 +7.912e+001 +6.807e+001 +5.987e+001 +5.138e+001 +4.347e+001 +3.827e+001
+3.465e+001
Frr[V/A]: +3.770e-001 +2.220e-001 +6.700e-002 -5.600e-002 +1.720e-001 +2.570e-001 +2.830e-001 +2.640e-001 +1.920e-001 +6.600e-002 -4.900e-002 -1.360e-001 -2.200e-001 -2.930e-001 -3.370e-001 -3.630e-001 -3.840e-001 -3.770e-001 -3.680e-001 -3.590e-001 -3.610e-001 -3.730e-001 -3.930e-001 -4.210e-001 -4.500e-001 -4.680e-001 -4.780e-001 -4.850e-001 -4.890e-001 -4.890e-001 -4.850e-001 -4.780e-001 -4.670e-001
```

```
1D_Inversion_Results_TEM.txt
-4.530e-001
 343.0099
                   85.88
 343.0099
                   17.03
   28.9360
                   62.77
    3.2609 10000000000.00
<Date: Thu Aug 28 11:17:52 2008
<Time Range=6 Current= 3.40 Stack= 5 Filter=50 Deff=
<Remark: SOUTH TO G-05, NEAR ROAD</pre>
                                                                             6 Ampl=OFF
<Place: EXADIS
#GEOSEC: 0259--B / 50.0/ 50.0/ 1
67.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 566713.000/ 3916850.000/
                                                                 0.000 DH =
                                                                                       0.000/rms=615.00
S [V/A]: +6.553e+001 +1.307e+002 +1.947e+002 +2.555e+002 +3.209e+002 +3.646e+002 +3.809e+002 +3.910e+002 +4.048e+002 +4.217e+002 +4.303e+002 +4.290e+002 +4.136e+002 +3.813e+002 +3.495e+002 +3.236e+002 +2.953e+002
+2.682e+002 +2.494e+002 +2.351e+002 +2.187e+002 +2.001e+002 +1.844e+002 +1.707e+002 +1.537e+002 +1.342e+002 +1.189e+002 +1.065e+002 +9.249e+001
+7.804e+001 +6.753e+001 +5.956e+001 +5.094e+001 +4.228e+001 +3.597e+001
+3.112e+001
Err[V/A]:
              -9.000e-001 -8.990e-001 -8.880e-001 -8.520e-001 +6.890e-001
+3.600e-001 +1.950e-001 +1.720e-001 +1.830e-001 +1.470e-001 +4.100e-002
-1.000e-001 -2.650e-001 -3.720e-001 -4.040e-001 -4.060e-001 -3.920e-001 -3.690e-001 -3.520e-001 -3.470e-001 -3.550e-001 -3.780e-001 -4.020e-001 -4.230e-001 -4.440e-001 -4.620e-001 -4.720e-001 -4.770e-001 -4.820e-001
-4.850e-001 -4.870e-001 -4.880e-001 -4.900e-001 -4.920e-001 -4.950e-001
-4.960e-001
 34.4021
400.0000
                    0.48
                  101.02
   30.2111
                   62.73
    3.4846 10000000000.00
<Date: Thu Aug 28 11:54:05 2008</pre>
<Time Range=6 Currrent= 3.30 Stack= 5 Filter=50 Deff= <Remark: NORTH TO G-09, POWER-LINES
                                                                             6 Ampl=OFF
<Place: ACHLADES
#GEOSEC: 0260-B / 50.0/ 50.0/ 1 62.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 566520.000/ 3916846.000/
                                                                                       0.000/\text{rms} = 836.00
                                                                 0.000 DH=
              +0.000e+000 +4.625e+001 +1.022e+002 +1.644e+002 +2.643e+002
+3.838e+002 +4.364e+002 +4.426e+002 +4.282e+002 +4.071e+002 +3.934e+002 +3.852e+002 +3.790e+002 +3.753e+002 +3.732e+002 +3.706e+002 +3.645e+002 +3.512e+002 +3.3642e+002 +2.906e+002 +2.596e+002 +2.342e+002
+2.131e+002 +1.885e+002 +1.617e+002 +1.416e+002 +1.256e+002 +1.081e+002
+9.052e+001 +7.807e+001 +6.873e+001 +5.865e+001 +4.846e+001 +4.094e+001
+3.507e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.960e-001 +7.930e-001 +3.470e-001 -3.000e-002 -1.940e-001 -2.020e-001 -1.600e-001
-1.150e-001 -6.900e-002 -3.900e-002 -4.000e-002 -6.700e-002 -1.310e-001
-2.270e-001 -3.050e-001 -3.580e-001 -4.010e-001 -4.310e-001 -4.460e-001 -4.560e-001 -4.670e-001 -4.760e-001 -4.820e-001 -4.850e-001 -4.870e-001 -4.880e-001 -4.890e-001 -4.890e-001 -4.910e-001 -4.940e-001 -4.970e-001
-4.980e-001
 43.1417 400.0000
                  0.35
101.94
   66.8537
                   66.14
    5.0600 10000000000.00
<Date: Thu Aug 28 13:00:48 2008
<Time Range=6 Currrent= 3.20 Stack= 5 Filter=50 Deff=
<Remark: WEST TO G-09, NEAR ROAD</pre>
                                                                             6 Ampl=OFF
*****
#GEOSEC: 0261-B / 50.0/ 50.0/ 1.
53.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/
                                                              566286.000/ 3916923.000/
                                                                 0.000 DH =
                                                                                       0.000/rms=566.00
              +0.000e+000 +0.000e+000 +2.151e+001 +3.924e+001 +5.689e+001
+7.380e+001 +8.551e+001 +9.383e+001 +1.022e+002 +1.103e+002 +1.166e+002
+1.222e+002 +1.301e+002 +1.411e+002 +1.519e+002 +1.619e+002 +1.742e+002
```

```
1D_Inversion_Results_TEM.txt
+1.866e+002 +1.940e+002 +1.978e+002 +1.996e+002 +1.983e+002 +1.949e+002 +1.902e+002 +1.816e+002 +1.671e+002 +1.519e+002 +1.375e+002 +1.198e+002 +1.009e+002 +8.732e+001 +7.718e+001 +6.638e+001 +5.550e+001 +4.740e+001
+4.099e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.700e-001 +7.320e-001 +5.920e-001 +4.850e-001 +3.860e-001 +3.190e-001 +3.030e-001 +3.160e-001 +3.480e-001 +3.880e-001 +4.060e-001 +3.990e-001 +3.570e-001
+2.690e-001 +1.750e-001 +9.500e-002 +1.100e-002 -6.900e-002 -1.350e-001 -2.010e-001 -2.950e-001 -3.950e-001 -4.460e-001 -4.690e-001 -4.810e-001 -4.860e-001 -4.860e-001 -4.870e-001 -4.910e-001 -4.940e-001
-4.970e-001
   27.4812
  200.0000
                     146.01
   15.2753
                      41.12
     2.2350 10000000000.00
<Date: Thu Aug 28 13:38:24 2008</pre>
<Time Range=6 Currrent= 3.00 Stack= 5 Filter=50 Deff= <Remark: WEST TO G-09, NEAR ROAD
                                                                                           6 Ampl=OFF
<Place: ACHLADES
<pre>
*****
#GEOSEC: 0262-B / 50.0/ 50.0/ 1.
53.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                1.0/ 566072.000/ 3916885.000/
                                                                             0.000 DH=
                                                                                                      0.000/rms=329.00
S [V/A]: +0.000e+000 +0.000e+000 +1.366e+001 +2.408e+001 +3.298e+001 +4.128e+001 +4.831e+001 +5.504e+001 +6.474e+001 +7.840e+001 +9.185e+001
+1.045e+002 +1.206e+002 +1.373e+002 +1.480e+002 +1.542e+002 +1.589e+002 +1.613e+002 +1.614e+002 +1.599e+002 +1.561e+002 +1.488e+002 +1.405e+002 +1.323e+002 +1.212e+002 +1.075e+002 +9.629e+001 +8.684e+001 +7.580e+001 +6.412e+001 +5.545e+001 +4.885e+001 +4.183e+001 +3.508e+001 +3.053e+001
+2.730e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.350e-001 +7.140e-001 +6.820e-001 +6.860e-001 +7.010e-001 +7.100e-001 +7.030e-001
+6.780e-001 +6.100e-001 +4.770e-001 +3.360e-001 +2.250e-001 +1.220e-001 +3.400e-002 -3.100e-002 -9.300e-002 -1.760e-001 -2.680e-001 -3.310e-001
-3.740e-001 -4.130e-001 -4.440e-001 -4.610e-001 -4.710e-001 -4.790e-001
-4.850e-001 -4.880e-001 -4.880e-001 -4.880e-001 -4.850e-001 -4.800e-001
-4.740e-001
   23.2315
                      5.56
86.57
  500.0001
   28.7814
                       58.49
     3.3778 10000000000.00
<Date: Thu Aug 28 14:00:10 2008
<Time Range=6 Currrent= 2.90 Stack= 5 Filter=50 Deff=
<Remark: EAST TO ACHLADES, NEAR ROAD</pre>
                                                                                           6 Ampl=OFF
#GEOSEC: 0263-C
                                      50.0/ 50.0/
                                                                1.0/ 565900.000/ 3916966.000/
54.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                             0.000 DH =
                                                                                                      0.000/\text{rms}=660.00
S [V/A]: +7.039e+001 +5.213e+001 +4.390e+001 +3.987e+001 +3.721e+001 +3.618e+001 +3.634e+001 +3.706e+001 +3.849e+001 +4.080e+001 +4.322e+001
+4.560e+001 +4.885e+001 +5.290e+001 +5.644e+001 +5.951e+001 +6.333e+001
+6.769e+001 +7.106e+001 +7.349e+001 +7.553e+001 +7.619e+001 +7.540e+001
+7.406e+001 +7.211e+001 +7.014e+001 +6.916e+001 +6.881e+001 +6.872e+001 +6.791e+001 +6.509e+001 +6.026e+001
Err[V/A]: +5.000e-001 +4.930e-001 +4.570e-001 +3.740e-001 -2.220e-001 -4.100e-002 +7.900e-002 +1.570e-001 +2.280e-001 +2.910e-001 +3.300e-001
+3.500e-001 +3.620e-001 +3.600e-001 +3.510e-001 +3.410e-001 +3.240e-001 +2.930e-001 +2.500e-001 +1.940e-001 +1.010e-001 -1.400e-002 -9.400e-002 -1.330e-001 -1.400e-001 -1.050e-001 -5.700e-002 -2.200e-002 -3.100e-002
-1.600e-001 -3.460e-001 -4.550e-001
  42.2984
200.0000
                      25.22
                      64.41
   26.0908
                     103.66
     1.7665 10000000000.00
<Date: Thu Aug 28 14:26:54 2008</pre>
<Time Range=5 Currrent= 2.50 Stack= 5 Filter=50 Deff=
                                                                                           6 Ampl=OFF
<Remark: EAST TO ACHLADES, CROSS-ROAD</pre>
```

```
*****
#GEOSEC: 0264-A
                                                 1.0/ 565931.000/ 3917316.000/
                              50.0/ 50.0/
68.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +4.891e+001 +2.793e+001 +1.844e+001 +1.359e+001 +1.026e+001 +8.456e+000 +7.904e+000 +7.791e+000 +7.869e+000 +8.057e+000 +8.225e+000
                                                                               0.000/rms=545.00
+8.358e+000 +8.537e+000 +8.797e+000 +9.091e+000 +9.406e+000 +9.887e+000
+1.058e+001 +1.127e+001 +1.194e+001 +1.289e+001 +1.418e+001 +1.547e+001
+1.678e+001 +1.872e+001 +2.148e+001 +2.404e+001 +2.620e+001 +2.810e+001 +2.813e+001 +2.609e+001 +2.340e+001 +1.981e+001 +1.606e+001 +1.350e+001
+1.170e+001
             +5.000e-001 +5.000e-001 +5.000e-001 +5.000e-001 -4.980e-001
Err[V/A]:
-4.280e-001 -2.040e-001 -2.600e-002 +7.900e-002 +1.130e-001 +1.100e-001 +1.100e-001 +1.280e-001 +1.660e-001 +2.090e-001 +2.480e-001 +2.920e-001 +3.370e-001 +3.680e-001 +3.910e-001 +4.180e-001 +4.570e-001 +4.950e-001
+5.300e-001 +5.670e-001 +5.870e-001 +5.600e-001 +4.680e-001 +2.110e-001 -2.270e-001 -4.400e-001 -4.850e-001 -4.950e-001 -4.960e-001 -4.960e-001
-4.940e-001
    9.7603
                 18.19
    9.7603
                 3.62
82.77
 131.6335
    1.0000 10000000000.00
<Date: Fri Aug 29 08:39:41 2008
<Time Range=6 Currrent= 2.90 Stack= 5 Filter=50 Deff=</pre>
                                                                       6 Ampl=OFF
<Remark: SOUTH TO SIRIPIDIANA</pre>
<place: SIRIPIDIANA
#GEOSEC: 0265-D / 50.0 / 50.0 / 1.80.0 / 36/4 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 566171.000/ 3917360.000/
                                                           0.000 DH =
                                                                               0.000/\text{rms}=698.00
    [V/A]:
             +0.000e+000 +0.000e+000 +1.620e-001 +6.465e+000 +1.034e+001
+1.205e+001 +1.285e+001 +1.344e+001 +1.413e+001 +1.492e+001 +1.560e+001 +1.622e+001 +1.708e+001 +1.831e+001 +1.960e+001 +2.096e+001 +2.306e+001
+2.627e+001 +2.975e+001 +3.345e+001 +3.904e+001 +4.700e+001 +5.460e+001
+6.132e+001 +6.883e+001 +7.488e+001 +7.696e+001 +7.679e+001 +7.466e+001
+7.033e+001 +6.563e+001 +6.097e+001 +5.463e+001 +4.673e+001 +4.001e+001
+3.439e+001
Err[V/A]:
             +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.740e-001
+4.520e-001 +3.020e-001 +2.690e-001 +2.530e-001 +2.460e-001 +2.490e-001
+2.650e-001 +2.970e-001 +3.500e-001 +4.040e-001 +4.560e-001 +5.230e-001 +5.960e-001 +6.480e-001 +6.830e-001 +7.080e-001 +7.120e-001 +6.860e-001 +6.270e-001 +4.940e-001 +2.670e-001 +6.700e-002 -7.900e-002 -2.100e-001
-3.160e-001 -3.800e-001 -4.230e-001 -4.610e-001 -4.860e-001 -4.950e-001
-4.980e-001
  16.4410
                 14.98
  16.4410
                  0.83
 200.0000
                155.61
    2.2065 10000000000.00
<Date: Fri Aug 29 09:07:04 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: SE TO SIRIPIDIANA
                                                                       6 Ampl=OFF
<Place: SIRIPIDIANA
<
*****
#GEOSEC: 0266-C / 50.0/ 50.0/ 1.84.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                1.0/ 566622.000/ 3917443.000/
                                                           0.000 \text{ DH} =
                                                                               0.000/rms = 747.00
             +0.000e+000 +0.000e+000 +0.000e+000 +3.816e+000 +2.098e+001
+2.752e+001 +2.855e+001 +2.894e+001 +2.969e+001 +3.118e+001 +3.285e+001 +3.454e+001 +3.684e+001 +3.982e+001 +4.265e+001 +4.536e+001 +4.922e+001
+5.452e+001 +5.964e+001 +6.442e+001 +7.049e+001 +7.710e+001 +8.169e+001
+8.474e+001 +8.744e+001 +8.956e+001 +9.075e+001 +9.133e+001 +9.089e+001
+8.742e+001 +8.124e+001 +7.379e+001 +6.317e+001 +5.081e+001 +4.162e+001
+3.481e+001
             -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001
Err[V/A]:
+5.640e-001 +1.360e-001 +1.080e-001 +1.760e-001 +2.580e-001 +3.050e-001
+3.290e-001 +3.480e-001 +3.670e-001 +3.880e-001 +4.110e-001 +4.420e-001
+4.730e-001 +4.850e-001 +4.780e-001 +4.430e-001 +3.670e-001 +2.860e-001
```

```
1D_Inversion_Results_TEM.txt
+2.160e-001 +1.480e-001 +9.500e-002 +6.000e-002 +1.200e-002 -1.020e-001 -2.920e-001 -4.220e-001 -4.750e-001 -4.940e-001 -4.980e-001 -4.990e-001
-5.000e-001
   30.6518
                  18.53
   30.6518
                   0.25
 161.7199
                 160.33
  10.4786 10000000000.00
<Date: Fri Aug 29 09:32:46_2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: POWER-LINES, NORTH TO G-06</pre>
<Place: SIRIPIDIANA</pre>
<
*****
#GEOSEC: 0267-A / 50.0/ 50.0/ 1.73.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                  1.0/ 566477.000/ 3917495.000/
                                                             0.000 \text{ DH} =
                                                                                   0.000/\text{rms}=736.00
    [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.413e+001 +2.323e+001
+2.469e+001 +2.333e+001 +2.184e+001 +2.014e+001 +1.850e+001 +1.741e+001
+1.666e+001 +1.597e+001 +1.548e+001 +1.533e+001 +1.539e+001 +1.570e+001
+1.644e+001 +1.741e+001 +1.853e+001 +2.034e+001 +2.317e+001 +2.624e+001 +2.944e+001 +3.410e+001 +4.033e+001 +4.572e+001 +5.031e+001 +5.570e+001
+6.170e+001 +6.660e+001 +7.052e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.590e-001 -4.700e-002 -3.220e-001 -3.570e-001 -3.500e-001 -3.220e-001 -2.870e-001 -2.470e-001 -1.850e-001 -9.800e-002 -1.200e-002 +6.500e-002 +1.630e-001 +2.770e-001 +3.680e-001 +4.410e-001 +5.220e-001 +5.980e-001 +6.460e-001
+6.700e-001 +6.770e-001 +6.530e-001 +6.070e-001 +5.550e-001 +4.960e-001
+4.430e-001 +4.000e-001 +3.560e-001
  17.7247
17.7247
                  25.11
                   6.41
                 157.97
 400.0000
    1.0000 10000000000.00
<Date: Fri Aug 29 09:54:58 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: POWER-LINES, NORTH TO G-06
                                                                          6 Ampl=OFF
<Place: SIRIPIDIANA
#GEOSEC: 0268-B / 50.0/ 50.0/ 1 82.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 566233.000/ 3917168.000/
                                                                                   0.000/\text{rms}=761.00
                                                              0.000 DH=
              +4.200e-001 +5.391e+000 +9.958e+000 +1.339e+001 +1.653e+001
+1.868e+001 +1.950e+001 +1.971e+001 +1.965e+001 +1.949e+001 +1.945e+001
+1.959e+001 +1.995e+001 +2.067e+001 +2.144e+001 +2.220e+001 +2.325e+001 +2.464e+001 +2.603e+001 +2.748e+001 +2.975e+001 +3.334e+001 +3.744e+001
+4.203e+001 +4.944e+001 +6.105e+001 +7.289e+001 +8.396e+001 +9.621e+001 +1.047e+002 +1.056e+002 +1.025e+002 +9.429e+001 +8.009e+001 +6.633e+001
+5.478e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.990e-001 -8.580e-001 +6.610e-001 +3.480e-001 +1.400e-001 +3.100e-002 -2.600e-002 -2.400e-002 +2.100e-002
+7.100e-002 +1.310e-001 +1.890e-001 +2.220e-001 +2.420e-001 +2.620e-001
+2.940e-001 +3.360e-001 +3.850e-001 +4.610e-001 +5.570e-001 +6.340e-001 +6.920e-001 +7.440e-001 +7.730e-001 +7.630e-001 +7.080e-001 +5.420e-001 +2.130e-001 -8.800e-002 -2.950e-001 -4.440e-001 -4.940e-001 -4.990e-001
-5.000e-001
   20.8130
                  21.56
                 2.71
197.53
   20.8130
 200.0000
    1,0000 10000000000.00
<Date: Fri Aug 29 10:48:56 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: WEST TO G-06
                                                                          6 Ampl=OFF
<Place: SIRIPIDIANA
*****
#GEOSEC: 0269-B / 50.0 / 50.0 / 1.88.0 / 36/4 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/
                                                           566382.000/ 3917117.000/
                                                                                   0.000/rms=737.00
                                                              0.000 DH =
             +0.000e+000 +0.000e+000 +0.000e+000 +2.431e+000 +7.804e+000
+1.313e+001 +1.680e+001 +1.958e+001 +2.289e+001 +2.697e+001 +3.080e+001
+3.463e+001 +4.021e+001 +4.826e+001 +5.679e+001 +6.555e+001 +7.846e+001
                                              Σελίδα 93
```

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1D_Inversion_Results_TEM.txt
+9.600e+001 +1.114e+002 +1.235e+002 +1.349e+002 +1.418e+002 +1.434e+002 +1.429e+002 +1.410e+002 +1.375e+002 +1.328e+002 +1.269e+002 +1.172e+002
+1.032e+002 +9.072e+001 +8.035e+001 +6.865e+001 +5.682e+001 +4.831e+001
+4.185e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.890e-001 +8.010e-001 +7.180e-001 +6.610e-001 +6.380e-001 +6.450e-001 +6.620e-001 +6.880e-001 +7.180e-001 +7.400e-001 +7.530e-001 +7.540e-001
+7.240e-001 +6.560e-001 +5.480e-001 +3.620e-001 +1.440e-001 +1.600e-002 -4.600e-002 -9.500e-002 -1.640e-001 -2.460e-001 -3.280e-001 -4.120e-001 -4.630e-001 -4.810e-001 -4.870e-001 -4.910e-001 -4.930e-001 -4.950e-001
-4.960e-001
   13.6653
   13.6653
                    0.25
                  170.50
 400.0000
    9.1361 10000000000.00
<Date: Fri Aug 29 11:10:27 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                               6 Ampl=OFF
<Remark: SW TO G-06
*****
#GEOSEC: 0270-B / 50.0/ 50.0/ 1. 44.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                       1.0/ 565764.000/ 3917145.000/
                                                                  0.000 \text{ DH} = 
                                                                                         0.000/rms=292.00
S [V/A]: +6.945e+000 +6.019e+000 +7.231e+000 +8.846e+000 +1.085e+001 +1.272e+001 +1.372e+001 +1.423e+001 +1.462e+001 +1.502e+001 +1.548e+001
+1.605e+001 +1.702e+001 +1.857e+001 +2.023e+001 +2.192e+001 +2.435e+001
+2.762e+001 +3.069e+001 +3.354e+001 +3.729e+001 +4.194e+001 +4.606e+001 +4.976e+001 +5.444e+001 +5.970e+001 +6.333e+001 +6.564e+001 +6.725e+001 +6.763e+001 +6.692e+001 +6.550e+001 +6.232e+001 +5.622e+001 +4.951e+001
+4.327e+001
Err[V/A]: +5.000e-001 -2.510e-001 -7.680e-001 -7.870e-001 +6.910e-001 +4.870e-001 +3.020e-001 +1.910e-001 +1.330e-001 +1.480e-001 +2.050e-001
+2.700e-001 +3.510e-001 +4.300e-001 +4.810e-001 +5.120e-001 +5.360e-001 +5.490e-001 +5.480e-001 +5.410e-001 +5.280e-001 +5.110e-001 +4.960e-001
+4.810e-001 +4.480e-001 +3.770e-001 +2.880e-001 +1.950e-001 +8.600e-002
-2.100e-002 -1.080e-001 -2.000e-001 -3.350e-001 -4.490e-001 -4.860e-001
-4.960e-001
   16.5074
                   16.54
                   53.18
 200.0000
 116.8896
                  123.27
    8.1107 10000000000000000
<Date: Fri Aug 29 12:03:18 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                               6 Ampl=OFF
<Remark: SOUTH TO SIRIPIDIANA</pre>
#GEOSEC: 0271-C
                                 50.0/ 50.0/
                                                       1.0/ 565663.000/ 3917035.000/
47.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                  0.000 DH =
                                                                                         0.000/\text{rms}=204.00
S [V/A]:
              +0.000e+000 +0.000e+000 +8.008e+000 +1.681e+001 +2.214e+001
+2.483e+001 +2.626e+001 +2.744e+001 +2.908e+001 +3.130e+001 +3.337e+001
+3.527e+001 +3.762e+001 +4.020e+001 +4.213e+001 +4.353e+001 +4.490e+001
+4.601e+001 +4.663e+001 +4.707e+001 +4.763e+001 +4.860e+001 +4.989e+001
+5.146e+001 +5.403e+001 +5.778e+001 +6.114e+001 +6.384e+001 +6.629e+001 +6.711e+001 +6.583e+001 +6.338e+001 +5.900e+001 +5.256e+001 +4.656e+001
+4.125e+001
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.340e-001
Err[V/A]:
+3.700e-001 +2.800e-001 +2.830e-001 +3.110e-001 +3.390e-001 +3.500e-001
+3.460e-001 +3.250e-001 +2.840e-001 +2.390e-001 +1.970e-001 +1.460e-001 +9.600e-002 +7.000e-002 +6.500e-002 +8.100e-002 +1.290e-001 +1.840e-001 +2.370e-001 +2.900e-001 +3.210e-001 +3.070e-001 +2.550e-001 +1.410e-001
 -3.500e-002 -1.870e-001 -2.950e-001 -3.880e-001 -4.510e-001 -4.780e-001
-4.900e-001
   24.3753
                     8.96
   65.0906
                   43.46
                  144.12
   54.4721
    1.5846 10000000000.00
<Date: Fri Aug 29 12:28:27 2008</pre>
```

```
1D_Inversion_Results_TEM.txt
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: EAST TO ACHLADES
<Place: ACHLADES
                                                                             6 Ampl=OFF
<Place: ACHLADES
******
                                                     1.0/ 565390.000/ 3917065.000/
#GEOSEC: 0272-C / 50.0/ 50.0/ 1. 41.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                      0.000/\text{rms}=257.00
              +0.000e+000 +0.000e+000 +6.909e+000 +2.378e+001 +3.514e+001
+4.020e+001 +4.136e+001 +4.157e+001 +4.150e+001 +4.138e+001 +4.145e+001
+4.167e+001 +4.225e+001 +4.333e+001 +4.459e+001 +4.585e+001 +4.760e+001 +4.972e+001 +5.146e+001 +5.284e+001 +5.434e+001 +5.570e+001 +5.634e+001
+5.632e+001 +5.515e+001 +5.180e+001 +4.761e+001 +4.342e+001 +3.821e+001
+3.277e+001 +2.892e+001 +2.606e+001 +2.291e+001 +1.946e+001 +1.661e+001
+1.417e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.380e-001 +3.330e-001 +8.700e-002 +1.300e-002 -1.100e-002 -1.000e-003 +2.400e-002 +5.400e-002 +9.600e-002 +1.440e-001 +1.760e-001 +1.960e-001 +2.070e-001
+2.030e-001 +1.880e-001 +1.690e-001 +1.390e-001 +9.100e-002 +3.000e-002 -5.500e-002 -1.960e-001 -3.520e-001 -4.280e-001 -4.580e-001 -4.710e-001 -4.720e-001 -4.690e-001 -4.690e-001 -4.750e-001 -4.880e-001 -4.960e-001
-4.990e-001
   41.4847
                   24.87
   57.2402
5.1889
                   70.34
                   22.53
    1.4637 100000000000.00
<Date: Fri Aug 29 12:53:09 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                             6 Ampl=OFF
<Remark: EAST TO ACHLADES</pre>
<Place: ACHLADES
<***************************
*****
#GEOSEC: 0273-B / 50.0/ 50.0/ 1.82.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 566902.000/ 3917692.000/
                                                                0.000 DH =
0.000/\text{rms} = 2851.00
              +0.000e+000 +0.000e+000 +4.812e+000 +1.025e+001 +1.328e+001
    [V/A]:
+1.381e+001 +1.323e+001 +1.252e+001 +1.170e+001 +1.096e+001 +1.055e+001
+1.036e+001 +1.036e+001 +1.066e+001 +1.122e+001 +1.193e+001 +1.318e+001 +1.530e+001 +1.777e+001 +2.057e+001 +2.512e+001 +3.243e+001 +4.065e+001 +4.950e+001 +6.257e+001 +7.941e+001 +9.221e+001 +1.008e+002 +1.070e+002
+1.073e+002 +1.021e+002 +9.442e+001 +8.261e+001 +6.769e+001 +5.563e+001
+4.612e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.340e-001 -5.000e-002 -2.700e-001 -3.120e-001 -2.980e-001 -2.400e-001 -1.590e-001
-6.600e-002 +6.300e-002 +2.180e-001 +3.470e-001 +4.490e-001 +5.620e-001
+6.680e-001 +7.350e-001 +7.780e-001 +8.150e-001 +8.410e-001 +8.510e-001 +8.500e-001 +8.310e-001 +7.620e-001 +6.330e-001 +4.570e-001 +1.840e-001 -1.520e-001 -3.600e-001 -4.480e-001 -4.870e-001 -4.980e-001 -4.990e-001
-5.000e-001
                 22.30
165.16
   18.3185
 400.0000
 400.0000
                   13.90
    1.0000 10000000000.00
<Date: Fri Aug 29 13:39:24 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NORTH TO G-80
*****
#GEOSEC: 0274-B / 50.0 / 50.0 / 1.77.0 / 36 / 4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 566469.000/ 3917695.000/
                                                               0.000 DH =
                                                                                      0.000/\text{rms}=332.00
S [V/A]: +1.783e+001 +1.116e+001 +9.181e+000 +8.734e+000 +8.929e+000
+9.474e+000 +9.870e+000 +1.007e+001 +1.013e+001 +1.001e+001 +9.826e+000
+9.666e+000 +9.493e+000 +9.392e+000 +9.388e+000 +9.467e+000 +9.647e+000
+9.980e+000 +1.035e+001 +1.072e+001 +1.123e+001 +1.184e+001 +1.230e+001 +1.259e+001 +1.272e+001 +1.252e+001 +1.210e+001 +1.166e+001 +1.110e+001
+1.061e+001 +1.038e+001 +1.032e+001 +1.038e+001 +1.052e+001 +1.050e+001
+1.020e+001
Err[V/A]: +5.000e-001 +5.000e-001 +4.290e-001 +1.050e-001 +1.760e-001
```

```
1D_Inversion_Results_TEM.txt
+2.310e-001 +1.690e-001 +8.300e-002 -1.100e-002 -8.100e-002 -1.050e-001 -1.030e-001 -7.600e-002 -2.500e-002 +3.000e-002 +7.800e-002 +1.320e-001 +1.880e-001 +2.250e-001 +2.470e-001 +2.540e-001 +2.350e-001 +1.860e-001
+1.140e-001 -4.000e-003 -1.420e-001 -2.210e-001 -2.490e-001 -2.350e-001
-1.680e-001 -8.200e-002 -7.000e-003 +5.000e-002 +2.300e-002 -1.110e-001
 -2.620e-001
      9.8992
                             20.37
                               5.66
       9.8992
                             15.90
  112.0514
       7.4881 10000000000.00
<Date: Fri Aug 29 14:07:42 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                      6 Ampl=OFF
<Remark: ES TO SIRIPIDIANA</pre>
*****
                                                  50.0/ 50.0/
                                                                                1.0/ 566098.000/ 3917718.000/
#GEOSEC: 0275-B
57.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                 0.000 DH =
                                                                                                                                     0.000/\text{rms}=426.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +3.471e+000 +2.716e+001 +3.831e+001 +3.976e+001 +3.911e+001 +3.781e+001 +3.613e+001 +3.470e+001
+3.346e+001 +3.203e+001 +3.070e+001 +2.999e+001 +2.976e+001 +2.996e+001
+3.088e+001 +3.216e+001 +3.358e+001 +3.564e+001 +3.830e+001 +4.061e+001 +4.259e+001 +4.503e+001 +4.793e+001 +5.038e+001 +5.242e+001 +5.429e+001
+5.440e+001 +5.206e+001 +4.852e+001 +4.328e+001 +3.740e+001 +3.331e+001
+3.049e+001
Err[V/A]:
                      -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001
+6.520e-001 +3.300e-002 -1.350e-001 -1.860e-001 -2.090e-001 -2.230e-001
-2.270e-001 -2.110e-001 -1.610e-001 -8.900e-002 -1.200e-002 +8.800e-002 +1.940e-001 +2.640e-001 +3.040e-001 +3.300e-001 +3.350e-001 +3.250e-001
+3.120e-001 +3.000e-001 +2.920e-001 +2.780e-001 +2.360e-001 +1.100e-001
 -1.360e-001 -3.330e-001 -4.220e-001 -4.590e-001 -4.630e-001 -4.500e-001
-4.290e-001
    35.7115
7.8002
                             28.15
                               4.08
  110.7950
                           127.79
       4.3501 10000000000.00
<Date: Fri Aug 29 14:31:45 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                      6 Ampl=OFF
<Remark: ÉS TO SIRIPIDIANA
<Place: SIRIPIDIANA
*****
#GEOSEC: G10-01-C / 50.0/ 50.0/ 1.36.0/40/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                   1.0/ 563084.000/ 3915426.000/
                                                                                                 0.000 DH =
                                                                                                                                     0.000/\text{rms}=141.00
S [V/A]: +0.000e+000 +6.700e-001 +1.930e+001 +2.792e+001 +3.158e+001 +3.182e+001 +3.106e+001 +3.026e+001 +2.930e+001 +2.824e+001 +2.741e+001 +2.674e+001 +2.592e+001 +2.492e+001 +2.403e+001 +2.324e+001 +2.225e+001
+2.115e+001 +2.033e+001 +1.971e+001 +1.910e+001 +1.860e+001 +1.836e+001
+1.829e+001 +1.838e+001 +1.876e+001 +1.933e+001 +2.002e+001 +2.117e+001 +2.288e+001 +2.455e+001 +2.602e+001 +2.764e+001 +2.889e+001 +2.930e+001 +2.928e+001 +2.891e+001 +2.810e+001 +2.701e+001 +2.563e+001
                      -9.000e-001 -9.000e-001 -9.000e-001 -8.620e-001 +3.210e-001
Err[V/A]:
-5.\overline{600}e^{-002} -1.450e^{-001} -1.620e^{-001} -1.650e^{-001} -1.640e^{-001} -1.620e^{-001}
-1.630e-001 -1.730e-001 -1.920e-001 -2.090e-001 -2.220e-001 -2.300e-001 -2.260e-001 -2.100e-001 -1.880e-001 -1.520e-001 -9.900e-002 -4.900e-002 -2.000e-003 +6.200e-002 +1.410e-001 +2.100e-001 +2.690e-001 +3.330e-001 +3.820e-001 +3.890e-001 +3.890
 -3.600e-002 -1.020e-001 -1.840e-001 -2.780e-001 -3.590e-001
    28.5612
                             16.00
    15.4418
                             49.47
    80.0000
                             73.27
    80.0000
                             79.47
       4.7070 10000000000.00
<Date: Tue May 20 13:35:49 2008
<Time Range=7 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                      6 Ampl=OFF
<Remark:
<Place: PERAMA

<a hree</a>
```

```
******
#GEOSEC: G59-01-B
                                   50.0/ 50.0/
                                                         1.0/ 562482.000/ 3914600.000/
74.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                     0.000 \text{ DH} =
                                                                                            0.000/rms=105.00
               +0.000e+000 +0.000e+000 +3.301e+000 +1.209e+001 +1.724e+001
+1.921e+001 +1.965e+001 +1.969e+001 +1.958e+001 +1.935e+001 +1.914e+001
+1.899e+001 +1.883e+001 +1.866e+001 +1.852e+001 +1.843e+001 +1.838e+001 +1.850e+001 +1.881e+001 +1.928e+001 +2.013e+001 +2.146e+001 +2.278e+001
+2.396e+001 +2.535e+001 +2.670e+001 +2.749e+001 +2.788e+001 +2.793e+001 +2.734e+001 +2.638e+001 +2.530e+001 +2.383e+001 +2.206e+001 +2.052e+001
+1.909e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.020e-001 +2.690e-001 +6.300e-002 -5.000e-003 -4.100e-002 -5.800e-002 -5.700e-002 -5.000e-002 -4.400e-002 -4.200e-002 -3.800e-002 -2.500e-002 +6.000e-003
+6.700e-002 +1.350e-001 +1.990e-001 +2.690e-001 +3.230e-001 +3.380e-001
+3.240e-001 +2.800e-001 +2.060e-001 +1.320e-001 +5.800e-002 -4.300e-002 -1.600e-001 -2.380e-001 -2.830e-001 -3.170e-001 -3.470e-001 -3.810e-001
-4.120e-001
  19.3000
18.1000
57.8000
                    15.30
                    22.10
                    39.40
   80,0000
                    34.90
    6.1600 10000000000.00
<Date: Tue May 20 14:20:28 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark:
<Place: PERAMA
<
*******
#GEOSEC: G59-02-B / 50.0/ 50.0/ 1.0/ 562453.000/ 3914711.000/ 71.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                            0.000/\text{rms}=259.00
               +1.284e+001 +8.737e+000 +7.988e+000 +8.234e+000 +9.011e+000
+1.001e+001 +1.071e+001 +1.113e+001 +1.148e+001 +1.169e+001 +1.179e+001 +1.184e+001 +1.190e+001 +1.201e+001 +1.215e+001 +1.233e+001 +1.266e+001 +1.326e+001 +1.329e+001 +1.481e+001 +1.611e+001 +1.800e+001 +1.981e+001
+2.142e+001 +2.331e+001 +2.518e+001 +2.645e+001 +2.743e+001 +2.855e+001
+2.974e+001 +3.053e+001 +3.096e+001 +3.112e+001 +3.082e+001 +3.029e+001
+2.972e+001
Err[V/A]: +5.000e-001 +4.880e-001 +9.700e-002 -2.880e-001 +4.210e-001 +3.840e-001 +2.890e-001 +2.030e-001 +1.240e-001 +6.400e-002 +3.700e-002
+3.000e-002 +3.500e-002 +5.500e-002 +8.500e-002 +1.230e-001 +1.820e-001
+2.660e-001 +3.420e-001 +4.040e-001 +4.660e-001 +5.050e-001 +5.040e-001 +4.730e-001 +4.060e-001 +3.200e-001 +2.640e-001 +2.350e-001 +2.110e-001 +1.730e-001 +1.230e-001 +6.600e-002 -6.000e-003 -7.700e-002 -1.170e-001
-1.430e-001
   11.9000
14.7000
                     8.46
                    17.60
   80.0000
                    50.70
                    46.70
   80.0000
   19.0000 10000000000.00
<Date: Tue May 20 14:47:03 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark:
<Place: PERAMA
<
#GEOSEC: G63-50-1A / 50.0/ 50.0/ 1.26.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                       1.0/ 563256.000/ 3918071.000/
                                                                    0.000 DH=
                                                                                            0.000/rms=192.00
               +0.000e+000 +0.000e+000 +0.000e+000 +5.778e+000 +1.264e+001
+1.673e+001 +1.784e+001 +1.792e+001 +1.757e+001 +1.716e+001 +1.696e+001 +1.697e+001 +1.717e+001 +1.764e+001 +1.818e+001 +1.871e+001 +1.940e+001
+2.024e+001 +2.096e+001 +2.161e+001 +2.249e+001 +2.360e+001 +2.455e+001
+2.530e+001 +2.603e+001 +2.647e+001 +2.650e+001 +2.636e+001 +2.608e+001
+2.572e+001 +2.541e+001 +2.508e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +6.270e-001 +1.710e-001 -3.100e-002 -1.060e-001 -8.500e-002 -2.800e-002
+3.200e-002 +9.500e-002 +1.520e-001 +1.830e-001 +1.950e-001 +2.010e-001 +2.020e-001 +2.050e-001 +2.130e-001 +2.250e-001 +2.300e-001 +2.170e-001 +1.850e-001 +1.230e-001 +4.100e-002 -1.700e-002 -4.800e-002 -6.400e-002
```

```
1D_Inversion_Results_TEM.txt
-7.000e-002 -8.100e-002 -9.600e-002
                     2.00
27.57
   14.1184
   19.3571
   56.1832
                     39.49
   22.1273
                     27.29
   16.2847 10000000000.00
<Date: Tue May 20 12:15:51 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                      6 Ampl=OFF
<Remark: NEXT TO VILLAGE</pre>
Place: ROUMELI

*****
#GEOSEC: G63-50-1B-2 / 50.0/ 50.0/
                                                            1.0/ 563241.000/ 3918110.000/
25.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                         0.000 DH=
                                                                                                 0.000/rms=108.00
S [V/A]: +0.000e+000 +6.350e+000 +2.775e+001 +3.729e+001 +4.123e+001 +4.104e+001 +3.993e+001 +3.911e+001 +3.841e+001 +3.802e+001 +3.800e+001
+3.822e+001 +3.871e+001 +3.956e+001 +4.046e+001 +4.130e+001 +4.238e+001
+4.365e+001 +4.470e+001 +4.560e+001 +4.669e+001 +4.794e+001 +4.893e+001
+4.971e+001 +5.050e+001 +5.106e+001 +5.108e+001 +5.069e+001 +4.957e+001 +4.726e+001 +4.450e+001 +4.163e+001 +3.773e+001 +3.313e+001 +2.960e+001
+2.695e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.050e-001 +2.440e-001 -8.900e-002 -1.360e-001 -1.140e-001 -7.200e-002 -2.300e-002 +1.900e-002 +5.200e-002 +8.600e-002 +1.170e-001 +1.340e-001 +1.410e-001 +1.430e-001 +1.400e-001 +1.370e-001 +1.340e-001 +1.300e-001 +1.240e-001 +1.140e-001
+1.000e-001 +7.300e-002 +2.600e-002 -2.700e-002 -8.600e-002 -1.710e-001 -2.750e-001 -3.510e-001 -4.000e-001 -4.350e-001 -4.520e-001 -4.540e-001
-4.500e-001
   64.0000
                       3.59
                     21.10
   34.5000
   58.0000
                     79.40
                     59.00
   18.4000
     3.1700 10000000000.00
<Date: Tue May 20 12:30:03 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                      6 Ampl=OFF
<Remark: NO FENSES
<Place: ROUMELI
*****
#GEOSEC: PAN-001 / 25.0/ 25.0/ 1.0/ 561994.000/ 3917768.000/ 24.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +8.246e+000 +8.345e+000 +8.621e+000 +8.898e+000 +9.254e+000 +9.673e+000 +1.003e+001 +1.037e+001 +1.084e+001 +1.147e+001 +1.208e+001
                                                                                                 0.000/rms=236.00
+1.264e+001 +1.338e+001 +1.422e+001 +1.487e+001 +1.534e+001 +1.575e+001
+1.592e+001 +1.575e+001 +1.538e+001 +1.467e+001 +1.334e+001 +1.375e+001 +1.592e+001 +1.575e+001 +1.538e+001 +1.467e+001 +1.360e+001 +1.265e+001 +1.185e+001 +1.098e+001 +1.017e+001 +9.667e+000 +9.345e+000 +9.049e+000 +8.743e+000 +8.396e+000 +7.944e+000 Err[V/A]: -1.700e-002 +1.150e-001 +1.800e-001 +1.950e-001 +1.990e-001 +1.990e-001 +2.200e-001 +2.200e-001 +2.750e-001 +2.940e-001
+3.010e-001 +2.960e-001 +2.690e-001 +2.300e-001 +1.810e-001 +1.030e-001 -1.000e-002 -1.150e-001 -2.020e-001 -2.860e-001 -3.450e-001 -3.670e-001 -3.670e-001 -3.000e-001 -2.480e-001 -2.020e-001 -1.710e-001
-1.990e-001 -2.880e-001 -3.720e-001
   10.1729
37.5968
5.9187
                     9.74
18.58
10.00
     4.4480 10000000000.00
<Date: Thu May 22 10:50:07 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                      3 Ampl=OFF
<Remark:
1.0/
#GEOSEC: PAN-002
                                    25.0/ 25.0/
                                                                     562014.000/ 3917788.000/
24.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +5.490e+000 +6.754e+000 +7.529e+000 +7.988e+000 +8.320e+000
+8.501e+000 +8.578e+000 +8.659e+000 +8.815e+000 +9.131e+000 +9.526e+000
                                                                                                 0.000/rms=246.00
+9.968e+000 +1.065e+001 +1.163e+001 +1.262e+001 +1.357e+001 +1.486e+001
                                                      Σελίδα 98
```

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1D_Inversion_Results_TEM.txt
+1.643e+001 +1.769e+001 +1.864e+001 +1.953e+001 +2.008e+001 +2.013e+001 +1.990e+001 +1.933e+001 +1.834e+001 +1.731e+001 +1.628e+001 +1.485e+001
+1.306e+001 +1.152e+001 +1.022e+001
              +7.650e-001 +6.010e-001 +4.260e-001 +2.850e-001 +1.560e-001
Err[V/A]:
+7.100e-002 +5.600e-002 +7.700e-002 +1.280e-001 +2.050e-001 +2.700e-001 +3.220e-001 +3.760e-001 +4.240e-001 +4.530e-001 +4.660e-001 +4.630e-001 +4.300e-001 +3.760e-001 +3.070e-001 +2.020e-001 +6.900e-002 -3.600e-002 -1.150e-001 -1.980e-001 -2.790e-001 -3.370e-001 -3.820e-001 -4.260e-001
-4.620e-001 -4.790e-001 -4.880e-001
 8.9897
102.7062
17.9368
                   11.32
20.90
                    31.25
    2.3264 10000000000.00
<Date: Thu May 22 10:57:12 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                 3 Ampl=OFF
<Remark:
<Place: PONORMOS
*****
#GEOSEC: PAN-003 / 25.0/25.0/1.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 562034.000/ 3917803.000/
                                                                                          0.000/rms=170.00
                                                                    0.000 DH =
               +9.655e+000 +9.832e+000 +9.954e+000 +9.971e+000 +9.913e+000
+9.775e+000 +9.657e+000 +9.607e+000 +9.632e+000 +9.811e+000 +1.010e+001
+1.044e+001 +1.099e+001 +1.180e+001 +1.262e+001 +1.341e+001 +1.449e+001 +1.586e+001 +1.709e+001 +1.823e+001 +1.977e+001 +2.181e+001 +2.374e+001
+2.549e+001 +2.757e+001 +2.943e+001 +3.016e+001 +3.017e+001 +2.956e+001
+2.844e+001 +2.752e+001 +2.688e+001
Err[V/A]: +8.000e-002 +6.900e-002 +3.500e-002 -8.000e-003 -4.500e-002 -6.500e-002 -4.900e-002 -1.200e-002 +4.800e-002 +1.290e-001 +1.950e-001 +2.470e-001 +3.030e-001 +3.540e-001 +3.850e-001 +4.010e-001 +4.110e-001
+4.150e-001 +4.170e-001 +4.230e-001 +4.380e-001 +4.570e-001 +4.600e-001 +4.390e-001 +3.680e-001 +2.210e-001 +6.900e-002 -5.100e-002 -1.460e-001 -1.860e-001 -1.720e-001 -1.430e-001
   10.1736
                    10.53
   18.3549
                    10.00
 153.5381
                    70.45
   10.9425 10000000000.00
<Date: Thu May 22 11:02:29 2008
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=</pre>
                                                                                 3 Ampl=OFF
<Remark:
*****
#GEOSEC: PAN-004-A / 25.0/ 25.0/ 1.0/ 562051.000/ 3917849.000/ 16.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +1.693e+001 +1.791e+001 +1.834e+001 +1.847e+001 +1.839e+001 +1.812e+001 +1.789e+001 +1.774e+001 +1.768e+001 +1.782e+001 +1.808e+001
                                                                                          0.000/\text{rms}=228.00
+1.838e+001 +1.877e+001 +1.920e+001 +1.954e+001 +1.981e+001 +2.015e+001
+2.055e+001 +2.085e+001 +2.101e+001 +2.099e+001 +2.059e+001 +1.995e+001
+1.924e+001 +1.824e+001 +1.693e+001 +1.575e+001 +1.465e+001 +1.320e+001
+1.145e+001 +1.002e+001 +8.861e+000
Err[V/A]: +2.880e-001 +1.700e-001 +7.900e-002 +1.300e-002 -4.300e-002 -6.900e-002 -6.200e-002 -3.700e-002 +8.000e-003 +6.200e-002 +9.600e-002
+1.120e-001 +1.140e-001 +1.050e-001 +9.600e-002 +9.400e-002 +9.600e-002 +9.000e-002 +6.800e-002 +2.700e-002 -4.700e-002 -1.420e-001 -2.100e-001 -2.550e-001 -2.980e-001 -3.430e-001 -3.820e-001 -4.150e-001 -4.490e-001
-4.730e-001 -4.830e-001 -4.880e-001
   18.1833
                   5.20
10.00
   18.3122
   20.2754
                    42.79
    2.5161 10000000000.00
<Date: Thu May 22 11:11:10 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                 3 Ampl=OFF
<Remark:
*****
#GEOSEC: PAN-005
                               / 25.0/ 25.0/ 1.0/ 562081.000/ 3917866.000/
                                                  Σελίδα 99
```

```
1D_Inversion_Results_TEM.txt
17.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +1.346e+001 +1.518e+001 +1.574e+001 +1.582e+001 +1.567e+001
+1.539e+001 +1.519e+001 +1.511e+001 +1.512e+001 +1.529e+001 +1.556e+001
                                                                                        0.000/rms=119.00
+1.586e+001 +1.630e+001 +1.684e+001 +1.730e+001 +1.767e+001 +1.809e+001
+1.848e+001 +1.873e+001 +1.888e+001 +1.898e+001 +1.899e+001 +1.891e+001
+1.878e+001 +1.855e+001 +1.817e+001 +1.777e+001 +1.736e+001 +1.679e+001 +1.610e+001 +1.556e+001 +1.518e+001
Err[V/A]: +5.850e-001 +3.150e-001 +1.020e-001 -6.000e-003 -6.400e-002 -7.600e-002 -5.300e-002 -1.900e-002 +2.700e-002 +7.900e-002 +1.150e-001
+1.370e-001 +1.530e-001 +1.570e-001 +1.490e-001 +1.370e-001 +1.180e-001 +9.000e-002 +6.600e-002 +4.300e-002 +1.600e-002 -1.300e-002 -3.600e-002 -5.600e-002 -8.300e-002 -1.170e-001 -1.460e-001 -1.690e-001 -1.890e-001 -1.940e-001 -1.800e-001 -1.600e-001
  15.8911
                    4.49
   15.2368
                   11.31
   25.4133
                   32.71
   11.1063 10000000000.00
<Date: Thu May 22 11:17:57 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=</pre>
                                                                              3 Ampl=OFF
<Remark:
*****
#GEOSEC: PAN-006-A / 25.0/ 25.0/ 1. 15.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 562103.000/ 3917880.000/
                                                                 0.000 DH=
                                                                                        0.000/\text{rms}=195.00
S [V/A]: +2.116e+001 +2.136e+001 +2.132e+001 +2.120e+001 +2.095e+001
+2.064e+001 +2.043e+001 +2.032e+001 +2.033e+001 +2.053e+001 +2.084e+001
+2.119e+001 +2.168e+001 +2.225e+001 +2.271e+001 +2.308e+001 +2.350e+001 +2.397e+001 +2.433e+001 +2.458e+001 +2.480e+001 +2.488e+001 +2.481e+001
+2.467e+001 +2.445e+001 +2.414e+001 +2.382e+001 +2.346e+001 +2.277e+001
+2.148e+001 +1.991e+001 +1.824e+001
Err[V/A]: +6.400e-002 +1.300e-002 -2.300e-002 -4.700e-002 -6.500e-002 -6.100e-002 -4.400e-002 -1.800e-002 +2.200e-002 +6.900e-002 +1.010e-001 +1.180e-001 +1.250e-001 +1.210e-001 +1.130e-001 +1.060e-001 +1.000e-001
+9.100e-002 +7.800e-002 +6.100e-002 +3.400e-002 -2.000e-003 -2.800e-002 -4.400e-002 -5.600e-002 -7.100e-002 -9.300e-002 -1.320e-001 -2.120e-001
-3.280e-001 -4.120e-001 -4.580e-001
   30.9312
                    2.17
   18.2693
                   10.00
   27.2065 63.88
9.3408 10000000000.00
<Date: Thu May 22 11:25:08 2008
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=</pre>
                                                                              3 Ampl=OFF
<Remark:
/ 25.0/ 25.0/
#GEOSEC: PAN-007-A
                                                      1.0/ 562122.000/ 3917920.000/
14.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                  0.000 DH =
                                                                                        0.000/\text{rms}=283.00
S [V/A]:
              +2.521e+001 +2.426e+001 +2.342e+001 +2.285e+001 +2.241e+001
+2.222e+001 +2.218e+001 +2.211e+001 +2.182e+001 +2.119e+001 +2.053e+001
+2.001e+001 +1.957e+001 +1.940e+001 +1.956e+001 +1.985e+001 +2.031e+001
+2.087e+001 +2.131e+001 +2.170e+001 +2.227e+001 +2.315e+001 +2.408e+001
+2.496e+001 +2.595e+001 +2.656e+001 +2.633e+001 +2.555e+001 +2.402e+001 +2.189e+001 +2.014e+001 +1.880e+001
Err[V/A]: -1.450e-001 -1.660e-001 -1.600e-001 -1.260e-001 -7.000e-002 -2.200e-002 -1.600e-002 -4.400e-002 -1.010e-001 -1.580e-001 -1.710e-001
-1.480e-001 -8.500e-002 +7.000e-003 +7.500e-002 +1.120e-001 +1.290e-001
+1.260e-001 +1.230e-001 +1.330e-001 +1.650e-001 +2.110e-001 +2.370e-001 +2.300e-001 +1.680e-001 +2.200e-002 -1.330e-001 -2.520e-001 -3.430e-001 -3.860e-001 -3.910e-001 -3.840e-001
   28.2053
                     3.76
                   30.46
   18.8329
   39.3705
                   57.10
    3.3990 10000000000.00
<Date: Thu May 22 11:34:26 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=60 Deff=
                                                                              3 Ampl=OFF
<Remark:
```

```
*****
                                                              1.0/ 562135.000/ 3917934.000/
#GEOSEC: PAN-008-A
                                      25.0/ 25.0/
12.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                             0.000 DH =
                                                                                                       0.000/\text{rms}=253.00
S [V/A]: +3.436e+001 +3.568e+001 +3.599e+001 +3.575e+001 +3.507e+001 +3.403e+001 +3.315e+001 +3.243e+001 +3.163e+001 +3.083e+001 +3.028e+001
+2.991e+001 +2.959e+001 +2.944e+001 +2.946e+001 +2.955e+001 +2.969e+001 +2.977e+001 +2.964e+001 +2.933e+001 +2.867e+001 +2.760e+001 +2.655e+001
+2.557e+001 +2.428e+001 +2.259e+001 +2.097e+001 +1.941e+001 +1.737e+001 +1.505e+001 +1.332e+001 +1.204e+001
Err[V/A]: +2.140e-001 +9.300e-002 -2.000e-003 -6.700e-002 -1.150e-001 -1.380e-001 -1.410e-001 -1.370e-001 -1.260e-001 -1.100e-001 -9.100e-002
-7.100e-002 -4.300e-002 -1.000e-002 +1.300e-002 +2.400e-002 +2.000e-002 -8.000e-003 -5.100e-002 -9.600e-002 -1.510e-001 -2.010e-001 -2.320e-001 -2.540e-001 -2.900e-001 -3.450e-001 -3.940e-001 -4.290e-001 -4.550e-001
-4.660e-001 -4.660e-001 -4.620e-001
   44.9881
                        2.22
   31.9729
23.2369
                       12.06
                       51.47
     3.4734 10000000000.00
<Date: Thu May 22 11:42:04 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                            3 Ampl=OFF
<Remark:
<Place: PQNORMOS
#GEOSEC: PAN-009 / 25.0/ 25.0/ 1.0/ 562157.000/ 3917985.000/ 14.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +2.104e+001 +2.245e+001 +2.340e+001 +2.407e+001 +2.471e+001
                                                                                                       0.000/\text{rms}=269.00
+2.525e+001 +2.560e+001 +2.585e+001 +2.615e+001 +2.654e+001 +2.689e+001 +2.721e+001 +2.758e+001 +2.795e+001 +2.818e+001 +2.829e+001 +2.834e+001 +2.828e+001 +2.816e+001 +2.802e+001 +2.781e+001 +2.755e+001 +2.733e+001 +2.712e+001 +2.683e+001 +2.637e+001 +2.583e+001 +2.521e+001 +2.423e+001
+2.282e+001 +2.151e+001 +2.035e+001
                +2.890e-001 +2.330e-001 +1.890e-001 +1.540e-001 +1.170e-001
Err[V/A]:
+8.600e-002 +6.900e-002 +6.400e-002 +6.600e-002 +7.200e-002 +7.700e-002 +7.800e-002 +7.000e-002 +5.400e-002 +3.600e-002 +2.000e-002 +1.000e-003 -1.800e-002 -3.000e-002 -3.800e-002 -4.300e-002 -4.700e-002 -5.600e-002 -7.100e-002 -1.040e-001 -1.440e-001 -1.870e-001 -2.400e-001 -2.930e-001 -3.240e-001 -3.450e-001
   24.9824
                        2.00
   25.2060
                       10.00
   29.5267
                       57.54
   12.7918 10000000000.00
<Date: Thu May 22 11:52:45 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff= 3 Ampl=OFF</pre>
<Remark:
<Place: PQNORMOS
<****************************
*****
#GEOSEC: PAN-010-A / 25.0/ 25.0/ 1.0
14.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                              1.0/ 562181.000/ 3918017.000/
                                                                           0.000 DH =
                                                                                                       0.000/\text{rms}=253.00
S [V/A]: +2.214e+001 +2.283e+001 +2.294e+001 +2.280e+001 +2.248e+001 +2.209e+001 +2.184e+001 +2.174e+001 +2.176e+001 +2.201e+001 +2.236e+001 +2.272e+001 +2.321e+001 +2.375e+001 +2.412e+001 +2.437e+001 +2.457e+001
+2.467e+001 +2.462e+001 +2.450e+001 +2.425e+001 +2.385e+001 +2.348e+001
+2.315e+001 +2.270e+001 +2.200e+001 +2.117e+001 +2.023e+001 +1.883e+001
+1.708e+001 +1.570e+001 +1.468e+001
Err[V/A]: +1.810e-001 +7.000e-002 -9.000e-003 -5.300e-002 -7.500e-002 -7.000e-002 -4.500e-002 -1.400e-002 +2.700e-002 +7.300e-002 +1.000e-001
+1.130e-001 +1.140e-001 +9.900e-002 +7.900e-002 +5.900e-002 +3.300e-002 +3.000e-003 -2.300e-002 -4.500e-002 -6.800e-002 -8.600e-002 -9.500e-002 -1.040e-001 -1.290e-001 -1.870e-001 -2.550e-001 -3.150e-001 -3.670e-001 -3.930e-001 -3.890e-001 -3.740e-001
   28.9811
                        2.00
                       10.00
   20.6892
   24.9904
                       52.15
```

```
1D_Inversion_Results_TEM.txt
    6.7139 10000000000.00
<Date: Thu May 22 12:00:59 2008
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=60 Deff=</pre>
                                                                               3 Ampl=OFF
<Remark:
<Place: PQNORMOS
#GEOSEC: PAN-011 / 25.0/25.0/1.0 1.0 15.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 562210.000/ 3918021.000/
                                                                 0.000 DH =
                                                                                         0.000/\text{rms}=167.00
S [V/A]: +2.377e+001 +2.415e+001 +2.371e+001 +2.298e+001 +2.188e+001 +2.060e+001 +1.970e+001 +1.911e+001 +1.862e+001 +1.837e+001 +1.839e+001
+1.855e+001 +1.889e+001 +1.942e+001 +1.995e+001 +2.042e+001 +2.104e+001
+2.176e+001 +2.236e+001 +2.287e+001 +2.349e+001 +2.418e+001 +2.473e+001
+2.517e+001 +2.561e+001 +2.587e+001 +2.573e+001 +2.526e+001 +2.421e+001
+2.243e+001 +2.069e+001 +1.916e+001
Err[V/A]: +1.520e-001 -2.400e-002 -1.440e-001 -2.090e-001 -2.450e-001 -2.420e-001 -2.110e-001 -1.680e-001 -1.040e-001 -2.500e-002 +3.500e-002
+7.700e-002 +1.150e-001 +1.440e-001 +1.570e-001 +1.630e-001 +1.640e-001
+1.610e-001 +1.560e-001 +1.510e-001 +1.450e-001 +1.360e-001 +1.260e-001 +1.110e-001 +7.600e-002 +4.000e-003 -8.300e-002 -1.730e-001 -2.770e-001 -3.620e-001 -4.010e-001 -4.220e-001
   31.1274
                     4.62
   14.6906
                   11.53
75.36
   30.8376
    5.5824 10000000000.00
<Date: Thu May 22 12:07:18 2008
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=60 Deff=</pre>
                                                                               3 Ampl=OFF
<Remark:
<Place: PQNORMOS
*****
#GEOSEC: PAN-012 / 25.0/ 25.0/ 1.0/ 561967.000/ 3917733.000/ 28.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +1.277e+001 +1.580e+001 +1.795e+001 +1.959e+001 +2.133e+001
                                                                                         0.000/\text{rms}=166.00
+2.295e+001 +2.397e+001 +2.465e+001 +2.529e+001 +2.592e+001 +2.641e+001 +2.683e+001 +2.733e+001 +2.788e+001 +2.885e+001 +2.907e+001
+2.958e+001 +3.003e+001 +3.040e+001 +3.079e+001 +3.108e+001 +3.110e+001 +3.096e+001 +3.059e+001 +2.998e+001 +2.943e+001 +2.899e+001 +2.848e+001
+2.783e+001 +2.704e+001 +2.597e+001
Err[V/A]: +7.580e-001 +6.410e-001 +5.340e-001 +4.570e-001 +3.700e-001 +2.750e-001 +2.060e-001 +1.610e-001 +1.270e-001 +1.110e-001 +1.060e-001 +1.040e-001 +9.900e-002 +9.100e-002 +8.500e-002 +8.200e-002 +8.300e-002 +8.600e-002 +8.600e-002 +7.900e-002 +6.000e-002 +2.300e-002 -1.500e-002 -4.800e-002 -8.100e-002 -1.030e-001 -1.060e-001 -1.020e-001 -1.050e-001
-1.420e-001 -2.190e-001 -2.980e-001
                   2.00
57.74
   11.2356
   33.6509
   26.7248
                   31.00
   16.4703 10000000000.00
<Date: Thu May 22 12:50:21 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=60 Deff=
                                                                               3 Ampl=OFF
<Remark:
<Place: PQNORMOS
<
*****
                                                      1.0/ 561955.000/ 3917706.000/
```

#GEOSEC: PAN-013 / 25.0/ 25.0/ 1 29.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH =0.000/rms = 99.00S [V/A]: +9.643e+000 +1.261e+001 +1.456e+001 +1.602e+001 +1.764e+001 +1.943e+001 +2.093e+001 +2.226e+001 +2.393e+001 +2.592e+001 +2.753e+001 +2.882e+001 +3.018e+001 +3.135e+001 +3.196e+001 +3.222e+001 +3.225e+001 +3.193e+001 +3.138e+001 +3.068e+001 +2.955e+001 +2.797e+001 +2.656e+001 +2.537e+001 +2.399e+001 +2.251e+001 +2.139e+001 +2.044e+001 +1.925e+001 +1.781e+001 +1.656e+001 +1.546e+001 Err[V/A]: +8.440e-001 +7.180e-001 +5.780e-001 +4.970e-001 +4.380e-001 +4.010e-001 +3.860e-001 +3.790e-001 +3.670e-001 +3.460e-001 +3.150e-001 +2.770e-001 +2.190e-001 +1.430e-001 +8.100e-002 +3.300e-002 -1.900e-002 -7.800e-002 -1.290e-001 -1.750e-001 -2.250e-001 -2.660e-001 -2.840e-001 -2.880e-001 -2.840e-001 -2.800e-001 -2.830e-001 -2.940e-001 -3.170e-001

```
1D_Inversion_Results_TEM.txt
-3.490e-001 -3.750e-001 -3.940e-001
   10.2510
                      2.90
                     38.08
   45.1311
   11.9909
                     36.13
     6.6225 10000000000.00
<Date: Thu May 22 12:56:36 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=60 Deff=
                                                                                      3 Ampl=OFF
<Remark:
<Place: PQNORMOS
#GEOSEC: PAN-014-A / 25.0/ 25.0/ 1 33.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 561929.000/ 3917694.000/
                                                                        0.000 DH =
                                                                                                0.000/rms=188.00
               +1.466e+001 +1.773e+001 +2.069e+001 +2.360e+001 +2.760e+001
+3.267e+001 +3.686e+001 +3.997e+001 +4.272e+001 +4.418e+001 +4.419e+001 +4.359e+001 +4.241e+001 +4.075e+001 +3.921e+001 +3.779e+001 +3.589e+001
+3.345e+001 +3.125e+001 +2.930e+001 +2.688e+001 +2.412e+001 +2.191e+001
+2.012e+001 +1.806e+001 +1.589e+001 +1.429e+001 +1.303e+001 +1.164e+001
+1.017e+001 +9.051e+000 +8.135e+000
Err[V/A]: +6.530e-001 +6.600e-001 +6.670e-001 +6.690e-001 +6.570e-001 +6.130e-001 +5.340e-001 +4.260e-001 +2.600e-001 +7.200e-002 -5.000e-002 -1.170e-001 -1.660e-001 -2.010e-001 -2.260e-001 -2.500e-001 -2.850e-001 -3.270e-001 -3.580e-001 -3.790e-001 -4.010e-001 -4.190e-001 -4.300e-001 -4.360e-001 -4.420e-001 -4.460e-001 -4.470e-001 -4.490e-001 -4.510e-001 -4.580e-001 -4.670e-001 -4.750e-001
     9.5391
                      2.47
 164.0945
                     23.90
   10.2777
                     26.00
     2.0981 10000000000.00
<Date: Thu May 22 13:04:47 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                      3 Ampl=Off
<Remark:
<Place: PQNORMOS
******
#GEOSEC: PAN-015-A / 25.0/ 25.0/ 1.0/ 561912.000/ 3917672.000/ 37.0/32/4/0/2222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +4.996e+001 +6.136e+001 +7.238e+001 +8.237e+001 +9.337e+001 +1.011e+002 +1.018e+002 +9.895e+001 +9.333e+001 +8.643e+001 +8.139e+001
                                                                                                0.000/rms=222.00
+7.772e+001 +7.390e+001 +7.014e+001 +6.734e+001 +6.514e+001 +6.263e+001 +5.996e+001 +5.792e+001 +5.628e+001 +5.442e+001 +5.243e+001 +5.089e+001 +4.961e+001 +4.799e+001 +4.588e+001 +4.382e+001 +4.177e+001 +3.895e+001 +3.552e+001 +3.278e+001 +3.064e+001
Err[V/A]:
               +6.900e-001 +6.910e-001 +6.760e-001 +6.220e-001 -4.720e-001
-1.810e-001 +8.200e-001 -2.300e-001 -3.030e-001 -3.130e-001 -2.940e-001 -2.720e-001 -2.490e-001 -2.300e-001 -2.200e-001 -2.130e-001 -2.060e-001 -1.990e-001 -1.920e-001 -1.870e-001 -1.800e-001 -1.730e-001 -1.710e-001 -1.750e-001 -1.940e-001 -2.340e-001 -2.790e-001 -3.180e-001 -3.570e-001
-3.810e-001 -3.840e-001 -3.790e-001
                      2.00
   18.6733
 200.0000
                     26.56
   32.6044
                     88.14
   10.1654 10000000000.00
<Date: Thu May 22 13:16:03 2008</pre>
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                                      3 Ampl=OFF
<Remark:
<Place: PONORMOS
<
*****
#GEOSEC: PAN-016
                                    25.0/
                                               25.0/
                                                            1.0/ 561902.000/ 3917648.000/
38.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                        0.000 DH=
                                                                                                0.000/rms=282.00
               +5.709e+001 +6.508e+001 +7.319e+001 +8.085e+001 +8.976e+001
+9.665e+001 +9.762e+001 +9.517e+001 +8.976e+001 +8.268e+001 +7.725e+001 +7.310e+001 +6.856e+001 +6.383e+001 +6.014e+001 +5.718e+001 +5.374e+001 +5.004e+001 +4.718e+001 +4.487e+001 +4.219e+001 +3.926e+001 +3.691e+001 +3.493e+001 +3.249e+001 +2.962e+001 +2.721e+001 +2.509e+001 +2.246e+001
+1.943e+001 +1.699e+001 +1.499e+001
Err[V/A]: +4.670e-001 +5.220e-001 +5.450e-001 +5.220e-001 +4.170e-001
                                                     Σελίδα 103
```

```
1D_Inversion_Results_TEM.txt
+1.790e-001 -6.500e-002 -2.220e-001 -3.110e-001 -3.370e-001 -3.310e-001 -3.210e-001 -3.120e-001 -3.080e-001 -3.080e-001 -3.090e-001 -3.090e-001 -3.080e-001 -3.120e-001 -3.080e-001 -3.110e-001 -3.170e-001 -3.270e-001
-3.400e-001 -3.600e-001 -3.880e-001 -4.130e-001 -4.340e-001 -4.560e-001
-4.740e-001 -4.840e-001 -4.900e-001
  18.6240
                  2.00
                 28.15
 200.0000
  17.7899
                 48.07
    3.3993 10000000000.00
<Date: Thu May 22 13:23:01 2008
<Time Range=5 Currrent= 1.00 Stack= 5 Filter=50 Deff=
                                                                    3 Ampl=OFF
<Remark:
<Place: PQNORMOS
******
#GEOSEC: 0084
                             50.0/ 50.0/
                                              1.0/ 562877.000/ 3917044.000/
30.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                         0.000 DH=
                                                                            0.000/rms = 67.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.276e+001 +1.990e+001
+2.023e+001 +1.869e+001 +1.738e+001 +1.615e+001 +1.521e+001 +1.470e+001 +1.445e+001 +1.432e+001 +1.438e+001 +1.459e+001 +1.486e+001 +1.533e+001
+1.602e+001 +1.670e+001 +1.735e+001 +1.820e+001 +1.923e+001 +2.010e+001
+2.085e+001 +2.180e+001 +2.296e+001 +2.394e+001 +2.482e+001 +2.589e+001
+2.707e+001 +2.795e+001 +2.860e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +8.140e-001 -1.930e-001 -3.680e-001 -3.600e-001 -3.020e-001 -2.180e-001 -1.470e-001
-8.500e-002 -1.600e-002 +5.300e-002 +1.070e-001 +1.470e-001 +1.880e-001
+2.260e-001 +2.490e-001 +2.590e-001 +2.630e-001 +2.580e-001 +2.520e-001
+2.480e-001 +2.460e-001 +2.460e-001 +2.440e-001 +2.390e-001 +2.260e-001 +2.000e-001 +1.710e-001 +1.420e-001
 200.0000
                  1.44
                 24.38
  13.6033
 154.5246
                 12.32
  39.7449 10000000000.00
<Date: Tue Jul 22 11:38:44 2008</pre>
<Time Range=5 Currrent= 1.90 Stack= 5 Filter=50 Deff=
                                                                    6 Ampl=OFF
<Remark: NEXT TO BOREHOLE, NEAR RIVER</pre>
<Place: ROUMELI
*****
#GEOSEC: 0232 / 50.0/ 50.0/ 1.
59.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 564853.000/ 3919004.000/
                                                         0.000 DH=
                                                                            0.000/rms=222.00
    [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +5.805e+000 +1.879e+001
+2.913e+001 +3.616e+001 +4.196e+001 +4.902e+001 +5.672e+001 +6.190e+001
+6.490e+001 +6.656e+001 +6.605e+001 +6.414e+001 +6.181e+001 +5.831e+001
+5.378e+001 +4.988e+001 +4.657e+001 +4.262e+001 +3.835e+001 +3.511e+001
+3.262e+001 +2.999e+001 +2.761e+001 +2.620e+001 +2.533e+001 +2.453e+001 +2.349e+001 +2.199e+001 +2.000e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.700e-001 +7.720e-001 +7.090e-001 +6.380e-001 +5.210e-001 +3.780e-001
+2.310e-001 +5.600e-002 -1.070e-001 -2.050e-001 -2.630e-001 -3.150e-001 -3.550e-001 -3.770e-001 -3.890e-001 -4.000e-001 -4.060e-001 -4.040e-001 -3.940e-001 -3.670e-001 -3.120e-001 -2.510e-001 -2.010e-001 -1.890e-001
-2.820e-001 -4.120e-001 -4.780e-001
                2.94
  11.6389
 200.0000
  19.4282
                10.05
  12.0634
               150.00
  19.1460 10000000000.00
<Date: Tue Jul 22 07:13:40 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff= <Remark: NEXT TO NATIONAL ROAD
                                                                    6 Ampl=OFF
<Place: SKEPASTI
<****************
#GEOSEC: 0233 / 50.0/ 50.0/ 1.77.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 565614.000/ 3919097.000/
                                                         0.000 DH=
                                                                            0.000/rms=275.00
S [V/A]: +0.000e+000 +0.000e+000 +3.074e+001 +5.372e+001 +7.675e+001
+9.701e+001 +1.094e+002 +1.179e+002 +1.265e+002 +1.347e+002 +1.399e+002
                                          Σελίδα 104
```

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1D_Inversion_Results_TEM.txt
+1.431e+002 +1.452e+002 +1.450e+002 +1.429e+002 +1.398e+002 +1.346e+002 +1.271e+002 +1.201e+002 +1.137e+002 +1.054e+002 +9.560e+001 +8.748e+001 +8.068e+001 +7.268e+001 +6.401e+001 +5.750e+001 +5.229e+001 +4.634e+001
+3.996e+001 +3.494e+001 +3.083e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.580e-001 +6.700e-001 +5.020e-001 +4.030e-001 +3.220e-001 +2.440e-001 +1.770e-001 +1.170e-001 +4.000e-002 -4.900e-002 -1.190e-001 -1.710e-001 -2.270e-001 -2.800e-001 -3.170e-001 -3.430e-001 -3.710e-001 -3.980e-001 -4.160e-001 -4.270e-001 -4.370e-001 -4.460e-001 -4.510e-001 -4.560e-001 -4.640e-001 -4.750e-001 -4.840e-001 -4.900e-001 19.8073
      19.8073
                                          1.80
                                       47.50
   200.0000
      81.7778
                                        33.39
      14.1003
                                        38.53
         3.7541 10000000000.00
 <Date: Tue Jul 22 07:46:10 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=
                                                                                                                                                               6 Ampl=OFF
 <Remark: IN SKEPASTI VILLAGE</pre>
****
#GEOSEC: 0234 / 49.0/ 49.0/ 1.
50.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                1.0/ 564567.000/ 3918978.000/
                                                                                                                                      0.000 \text{ DH} = 
                                                                                                                                                                                   0.000/rms=293.00
S [V/A]: +0.000e+000 +0.000e+000 +1.497e+000 +2.187e+001 +4.258e+001 +6.255e+001 +7.718e+001 +8.842e+001 +1.000e+002 +1.090e+002 +1.120e+002
+1.117e+002 +1.087e+002 +1.035e+002 +9.888e+001 +9.496e+001 +9.021e+001 +8.469e+001 +7.998e+001 +7.583e+001 +7.063e+001 +6.463e+001 +5.979e+001
+5.584e+001 +5.130e+001 +4.645e+001 +4.282e+001 +3.989e+001 +3.651e+001 +3.280e+001 +2.981e+001 +2.726e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +9.000e-001 +8.540e-001 +7.500e-001 +6.460e-001 +4.880e-001 +2.590e-001 +6.000e-002 -7.800e-002 -1.810e-001 -2.350e-001 -2.520e-001 -2.590e-001 -2.710e-001 -2.910e-001 -3.120e-001 -3.320e-001 -3.530e-001 -3.710e-001 -3.810e-001 -3.850e-001 -3.880e-001 -3.900e-001 -3.920e-001 -3.950e-001 -4.030e-001
 -4.180e-001 -4.350e-001 -4.500e-001
      12.9158
                                          2.22
   400.0000
                                       43.72
                                       45.30
      22.8701
                                        39.63
         5.4682
         1.3795 10000000000.00
<Date: Tue Jul 22 08:24:51 2008
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
<Remark: NOT SQUARE, POWERLINES, FENCES</pre>
                                                                                                                                                               6 Ampl=OFF
<Place: SKEPASTI
 #GEOSEC: 0235 / 49.0/ 49.0/ 1.72.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                1.0/ 564172.000/ 3919071.000/
                                                                                                                                      0.000 \text{ DH} =
                                                                                                                                                                                   0.000/\text{rms}=335.00
                              +0.000e+000 +0.000e+000 +1.947e+000 +1.739e+001 +3.065e+001
+4.124e+001 +4.916e+001 +5.645e+001 +6.677e+001 +8.105e+001 +9.447e+001 +1.063e+002 +1.201e+002 +1.326e+002 +1.389e+002 +1.407e+002 +1.387e+002 +1.326e+002 +1.264e+002 +1.212e+002 +1.156e+002 +1.102e+002 +1.066e+002
+1.022e+002 +9.696e+001 +9.011e+001 +8.433e+001 +7.942e+001 +7.345e+001
+6.613e+001 +5.924e+001 +5.265e+001

Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.980e-001 +7.900e-001 +7.180e-001 +7.070e-001 +7.110e-001 +7.050e-001 +6.770e-001 +6.250e-001 +5.210e-001 +3.470e-001 +1.300e-001 -1.400e-001 +3.470e-001 +3.470e
-2.380e-001 -2.630e-001 -2.570e-001 -2.350e-001 -2.190e-001 -2.280e-001 -2.540e-001 -2.940e-001 -3.300e-001 -3.470e-001 -3.600e-001 -3.860e-001 -4.330e-001 -4.710e-001 -4.900e-001
      12.1710
                                         2.61
   400.0000
                                        74.31
      30.2976
                                       56.51
         9.4799
                                        38.37
         1.3347 10000000000.00
 <Date: Tue Jul 22 08:56:22 2008</pre>
 <Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                                                                                               6 Ampl=OFF
 <Remark: IN WATER-MELONS</pre>
```

## 1D\_Inversion\_Results\_TEM.txt

```
*****
#GEOSEC: 0236-A / 50.0/ 50.0/ 1.
59.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 563709.000/ 3919056.000/
                                                                        0.000 DH =
                                                                                                0.000/rms=241.00
S [V/A]: +0.000e+000 +0.000e+000 +1.668e+001 +3.849e+001 +5.935e+001 +7.779e+001 +8.969e+001 +9.800e+001 +1.062e+002 +1.128e+002 +1.156e+002
+1.163e+002 +1.152e+002 +1.116e+002 +1.068e+002 +1.015e+002 +9.357e+001 +8.349e+001 +7.526e+001 +6.881e+001 +6.192e+001 +5.543e+001 +5.111e+001
+4.805e+001 +4.491e+001 +4.186e+001 +3.966e+001 +3.788e+001 +3.575e+001 +3.330e+001 +3.124e+001 +2.942e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.850e-001 +7.350e-001 +5.750e-001 +4.630e-001 +3.420e-001 +2.000e-001 +8.500e-002
-3.000e-003 -9.700e-002 -1.980e-001 -2.780e-001 -3.410e-001 -3.970e-001 -4.310e-001 -4.400e-001 -4.380e-001 -4.260e-001 -4.000e-001 -3.730e-001 -3.470e-001 -3.200e-001 -2.980e-001 -2.900e-001 -2.910e-001 -3.020e-001 -3.210e-001 -3.420e-001 -3.620e-001
     8.3895
                      1.17
  308.8628
43.5443
                     39.23
                     20.47
   16.5785 10000000000.00
<Date: Tue Jul 22 09:46:26 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                     6 Ampl=OFF
<Remark: POWRLINES, NEAR NATIONAL ROAD</pre>
<Place: PANORMOS
#GEOSEC: 0237-A / 50.0/ 50.0/ 1. 49.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                            1.0/ 563201.000/ 3919146.000/
                                                                       0.000 \, \text{DH} =
                                                                                                0.000/\text{rms}=301.00
     [V/A]:
               +0.000e+000 +0.000e+000 +1.332e+001 +3.212e+001 +4.705e+001
+5.752e+001 +6.355e+001 +6.798e+001 +7.270e+001 +7.674e+001 +7.851e+001
+7.904e+001 +7.890e+001 +7.837e+001 +7.780e+001 +7.707e+001 +7.544e+001 +7.199e+001 +6.775e+001 +6.334e+001 +5.746e+001 +5.069e+001 +4.544e+001 +4.134e+001 +3.677e+001 +3.198e+001 +2.839e+001 +2.546e+001 +2.207e+001
+1.844e+001 +1.567e+001 +1.351e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.580e-001
+5.950e-001 +4.430e-001 +3.760e-001 +2.970e-001 +1.810e-001 +8.300e-002 +2.000e-002 -2.000e-002 -3.700e-002 -5.400e-002 -8.800e-002 -1.640e-001 -2.730e-001 -3.510e-001 -3.970e-001 -4.290e-001 -4.460e-001 -4.510e-001
-4.530e-001 -4.560e-001 -4.630e-001 -4.700e-001 -4.770e-001 -4.850e-001 -4.920e-001 -4.950e-001 -4.970e-001
 26.1484
112.9799
                      3.74
                     39.95
   17.0770
                     29.97
     2.2677 10000000000.00
<Date: Tue Jul 22 10:13:18 2008</pre>
<Time Range=5 Currrent= 3.40 Stack= 5 Filter=50 Deff=
                                                                                     6 Ampl=OFF
<Remark: POWRLINES, FENCES</pre>
<Place: PANORMOS
<**********************************
*****
                                                          1.0/ 562921.000/ 3919122.000/
#GEOSEC: 0238-B / 50.0/ 50.0/ 1.0
35.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                      0.000 DH =
S [V/A]: +3.526e+001 +4.891e+001 +5.638e+001 +6.035e+001 +6.250e+001 +6.240e+001 +6.132e+001 +6.031e+001 +5.944e+001 +5.890e+001 +5.857e+001 +5.804e+001 +5.679e+001 +5.434e+001 +5.160e+001 +4.898e+001 +4.558e+001
+4.152e+001 +3.802e+001 +3.493e+001 +3.104e+001 +2.661e+001 +2.318e+001
+2.057e+001 +1.785e+001 +1.537e+001 +1.386e+001 +1.288e+001 +1.201e+001
+1.137e+001 +1.103e+001 +1.078e+001 +1.038e+001 +9.558e+000 +8.518e+000
+7.450e+000
Err[V/A]: -8.740e-001 -7.230e-001 -4.790e-001 -2.820e-001 +8.700e-002 -5.400e-002 -9.800e-002 -9.100e-002 -6.000e-002 -3.600e-002 -4.700e-002
-8.600e-002 -1.580e-001 -2.420e-001 -2.960e-001 -3.280e-001 -3.580e-001 -3.910e-001 -4.190e-001 -4.420e-001 -4.640e-001 -4.780e-001 -4.830e-001 -4.820e-001 -4.750e-001 -4.550e-001 -4.220e-001 -3.770e-001 -3.010e-001 -2.090e-001 -1.640e-001 -1.780e-001 -2.780e-001 -4.210e-001 -4.820e-001
-4.970e-001
 200.0000
                       3.30
```

```
1D_Inversion_Results_TEM.txt
                 28.03
  45.3032
  17.1705
                 13.55
    3.9172 10000000000.00
<Date: Tue Jul 22 12:27:44 2008</pre>
<Time Range=6 Currrent= 2.40 Stack= 5 Filter=50 Deff=
                                                                    6 Ampl=OFF
<Remark: POWERLINES, NEXT TO ROAD</pre>
<Place: PANORMOS
*****
#GEOSEC: 0239-A / 50.0/ 50.0/ 1.
47.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 562717.000/ 3918971.000/
                                                        0.000 DH =
                                                                            0.000/\text{rms}=181.00
S [V/A]: +5.753e+001 +4.081e+001 +3.342e+001 +2.970e+001 +2.724e+001 +2.603e+001 +2.571e+001 +2.577e+001 +2.598e+001 +2.634e+001 +2.663e+001
+2.682e+001 +2.694e+001 +2.695e+001 +2.686e+001 +2.676e+001 +2.657e+001
+2.626e+001 +2.584e+001 +2.532e+001 +2.444e+001 +2.315e+001 +2.193e+001 +2.083e+001 +1.944e+001 +1.777e+001 +1.635e+001 +1.512e+001 +1.366e+001
+1.216e+001 +1.115e+001 +1.049e+001
            +5.000e-001 +4.980e-001 +4.800e-001 +4.220e-001 -2.860e-001
Err[V/A]:
-1.220e-001 -2.200e-002 +2.700e-002 +5.300e-002 +6.200e-002 +5.300e-002 +3.700e-002 +1.400e-002 -9.000e-003 -2.300e-002 -3.300e-002 -4.700e-002 -7.700e-002 -1.180e-001 -1.620e-001 -2.170e-001 -2.710e-001 -3.030e-001
-3.250e-001 -3.500e-001 -3.830e-001 -4.070e-001 -4.210e-001 -4.270e-001
-4.140e-001 -3.810e-001 -3.370e-001
                2.53
35.21
  28.4732
  24.9093
                23.86
   9.3147
    2.9346 10000000000.00
<Date: Tue Jul 22 13:03:45 2008
<Time Range=5 Currrent= 2.40 Stack= 5 Filter=50 Deff=</pre>
                                                                    6 Ampl=OFF
<Remark: POWERLINES, FENCES</pre>
<Place: PANORMOS
******
                            50.0/ 50.0/
                                              1.0/ 562334.000/ 3918875.000/
#GEOSEC: 0240-A
50.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                        0.000 DH =
                                                                            0.000/\text{rms} = 83.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.490e+000 +1.433e+001
+1.931e+001 +2.004e+001 +2.015e+001 +2.027e+001 +2.061e+001 +2.102e+001 +2.141e+001 +2.192e+001 +2.255e+001 +2.311e+001 +2.364e+001 +2.439e+001
+2.547e+001 +2.659e+001 +2.776e+001 +2.947e+001 +3.181e+001 +3.392e+001
+3.567e+001 +3.744e+001 +3.851e+001 +3.842e+001 +3.774e+001 +3.641e+001
+3.461e+001 +3.312e+001 +3.191e+001
+1.250e-001 +1.310e-001 +1.380e-001 +1.480e-001 +1.620e-001 +1.880e-001
+2.290e-001 +2.690e-001 +3.040e-001 +3.400e-001 +3.600e-001 +3.480e-001 +3.050e-001 +2.070e-001 +5.400e-002 -7.300e-002 -1.550e-001 -2.130e-001
-2.390e-001 -2.420e-001 -2.400e-001
  19.5353
                 7.37
                 31.34
  26.9223
 133.4679
                66.54
  11.4496 10000000000.00
<Date: Tue Jul 22 13:34:01 2008</pre>
<Time Range=5 Currrent= 2.40 Stack= 5 Filter=50 Deff=
                                                                    6 Ampl=OFF
<Remark: FENCES
<Place: PANORMOS
*****
#GEOSEC: 0241-A / 50.0/ 50.0/ 1 48.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 561725.000/ 3918946.000/
                                                         0.000 DH=
                                                                            0.000/rms = 97.00
   [V/A]: +2.878e+001 +1.856e+001 +1.468e+001 +1.310e+001 +1.236e+001
+1.222e+001 +1.226e+001 +1.226e+001 +1.216e+001 +1.191e+001 +1.163e+001
+1.138e+001 +1.112e+001 +1.092e+001 +1.087e+001 +1.092e+001 +1.113e+001
+1.158e+001 +1.212e+001 +1.272e+001 +1.363e+001 +1.490e+001 +1.610e+001 +1.721e+001 +1.855e+001 +1.990e+001 +2.063e+001 +2.089e+001 +2.066e+001
+1.970e+001 +1.844e+001 +1.710e+001
Err[V/A]: +5.000e-001 +5.000e-001 +4.870e-001 +3.900e-001 -1.690e-001 -1.100e-002 +8.000e-003 -2.000e-002 -6.700e-002 -1.150e-001 -1.350e-001 -1.330e-001 -1.080e-001 -5.400e-002 +7.000e-003 +6.600e-002 +1.430e-001
                                         Σελίδα 107
```

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1D_Inversion_Results_TEM.txt
+2.300e-001 +2.940e-001 +3.430e-001 +3.890e-001 +4.210e-001 +4.300e-001 +4.170e-001 +3.680e-001 +2.660e-001 +1.450e-001 +1.900e-002 -1.380e-001 -2.900e-001 -3.790e-001 -4.290e-001
   11.8250
                  30.43
 400.0000
                  12.87
44.74
 200.0000
    2.7459 10000000000.00
<Date: Tue Jul 22 14:07:54 2008</pre>
<Time Range=5 Currrent= 2.40 Stack= 5 Filter=50 Deff=
                                                                            6 Ampl=OFF
<Remark: FENCES, POWERLINES</pre>
<Place: PANORMOS
<
*****
#GEOSEC: 0242-A / 50.0/ 50.0/ 1.46.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 561948.000/ 3918970.000/
                                                               0.000 DH=
                                                                                     0.000/\text{rms}=352.00
    [V/A]: +6.460e-001 +5.030e+000 +8.416e+000 +1.048e+001 +1.185e+001
+1.216e+001 +1.186e+001 +1.147e+001 +1.104e+001 +1.083e+001 +1.091e+001
+1.119e+001 +1.176e+001 +1.273e+001 +1.385e+001 +1.501e+001 +1.673e+001
+1.917e+001 +2.151e+001 +2.368e+001 +2.637e+001 +2.920e+001 +3.115e+001 +3.258e+001 +3.426e+001 +3.646e+001 +3.853e+001 +4.027e+001 +4.171e+001
+4.118e+001 +3.849e+001 +3.493e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.920e-001 -7.400e-001 +3.530e-001 -2.300e-002 -1.720e-001 -1.990e-001 -1.450e-001 -1.800e-002 +1.080e-001
+2.110e-001 +3.130e-001 +4.120e-001 +4.770e-001 +5.200e-001 +5.590e-001 +5.850e-001 +5.850e-001 +5.630e-001 +5.050e-001 +4.090e-001 +3.310e-001
+2.900e-001 +2.850e-001 +3.070e-001 +3.070e-001 +2.530e-001 +7.700e-002
-2.330e-001 -4.170e-001 -4.800e-001
  9.5578
13.2412
                  0.25
17.39
 200.0000
                  86.73
   17.6383 10000000000.00
<Date: Tue Jul 22 14:34:34 2008</pre>
<Time Range=5 Currrent= 2.40 Stack= 5 Filter=50 Deff= <Remark: FENCES, POWERLINE
                                                                            6 Ampl=OFF
<Place: PANORMOS
1.0/ 562413.000/ 3917590.000/
H= 0.000 DH= 0.000/
#GEOSEC: 0276 / 50.0/ 50.0/ 1 23.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                     0.000/rms=176.00
              +0.000e+000 +0.000e+000 +1.164e+001 +2.096e+001 +2.421e+001
+2.330e+001 +2.188e+001 +2.092e+001 +2.017e+001 +1.977e+001 +1.970e+001
+1.979e+001 +2.001e+001 +2.039e+001 +2.078e+001 +2.114e+001 +2.160e+001 +2.216e+001 +2.263e+001 +2.306e+001 +2.360e+001 +2.421e+001 +2.464e+001
+2.486e+001 +2.483e+001 +2.426e+001 +2.338e+001 +2.240e+001 +2.108e+001
+1.961e+001 +1.859e+001 +1.793e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.980e-001 +2.840e-001 -2.430e-001 -2.800e-001 -2.280e-001 -1.430e-001 -5.200e-002 +6.000e-003 +4.300e-002 +7.400e-002 +1.000e-001 +1.130e-001 +1.190e-001 +1.210e-001
+1.230e-001 +1.250e-001 +1.280e-001 +1.270e-001 +1.130e-001 +8.000e-002 +3.100e-002 -5.500e-002 -1.670e-001 -2.440e-001 -2.880e-001 -3.110e-001 -2.990e-001 -2.590e-001 -2.090e-001
 200.0000
                   0.45
   20.2203
                   36.54
                   28.56
   99.8330
    8.4308 10000000000.00
<Date: Mon Sep 15 08:53:36 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=
                                                                            6 Ampl=OFF
<Remark: FENCES, POWER-LINES</pre>
*****
                                50.0/ 50.0/
                                                     1.0/
                                                             562294.000/ 3917437.000/
28.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.560e-001 +5.241e+000 +7.242e+000 +7.569e+000 +7.586e+000 +7.586e+000 +7.639e+000 +7.761e+000 +7.947e+000 +8.260e+000 +8.734e+000 +9.241e+000 +9.757e+000 +1.051e+001
                                                                                     0.000/rms = 92.00
+1.158e+001 +1.265e+001 +1.373e+001 +1.524e+001 +1.723e+001 +1.899e+001
+2.049e+001 +2.211e+001 +2.331e+001 +2.344e+001 +2.288e+001 +2.154e+001
```

```
1D_Inversion_Results_TEM.txt
+1.957e+001 +1.800e+001 +1.686e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +6.410e-001 +1.140e-001 +8.000e-003 +1.500e-002 +6.300e-002 +1.250e-001
+1.790e-001 +2.330e-001 +2.900e-001 +3.360e-001 +3.710e-001 +4.140e-001
+4.610e-001 +4.950e-001 +5.180e-001 +5.330e-001 +5.280e-001 +5.000e-001 +4.490e-001 +3.370e-001 +1.330e-001 -7.400e-002 -2.310e-001 -3.440e-001
-3.900e-001 -3.850e-001 -3.640e-001
    2.7033
                   0.28
   10.4962
                  19.60
 200.0000
                  62.44
    2.6731 10000000000.00
<Date: Mon Sep 15 09:16:02 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: POWER-LINE</pre>
<Place: ROUMELI
*****
#GEOSEC: 0278 / 50.0/ 50.0/ 1.0/ 562170.000/ 3917615.000/ 23.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +4.127e+001 +2.750e+001 +2.181e+001 +1.924e+001 +1.782e+001 +1.746e+001 +1.771e+001 +1.813e+001 +1.874e+001 +1.954e+001 +2.026e+001
                                                                                    0.000/rms = 98.00
+2.088e+001 +2.170e+001 +2.270e+001 +2.360e+001 +2.442e+001 +2.550e+001
+2.687e+001 +2.814e+001 +2.932e+001 +3.091e+001 +3.295e+001 +3.474e+001
+3.629e+001 +3.803e+001 +3.951e+001 +3.996e+001 +3.968e+001 +3.852e+001 +3.636e+001 +3.424e+001 +3.236e+001
             +5.000e-001 +5.000e-001 +4.900e-001 +4.230e-001 -2.260e-001
Err[V/A]:
+2.000e-003 +1.150e-001 +1.600e-001 +1.820e-001 +1.960e-001 +2.000e-001
+2.030e-001 +2.100e-001 +2.160e-001 +2.240e-001 +2.320e-001 +2.420e-001 +2.570e-001 +2.700e-001 +2.820e-001 +2.950e-001 +3.030e-001 +2.970e-001
+2.770e-001 +2.240e-001 +1.200e-001 +5.000e-003 -1.010e-001 -2.110e-001
-2.910e-001 -3.280e-001 -3.500e-001
    6.3546
                   0.29
  22.1479
52.5151
                  19.38
                 105.65
    6.5324 10000000000.00
<Date: Mon Sep 15 09:34:02 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: FENCE, POWER-LINE</pre>
<Place: ROUMELÍ
*****
#GEOSEC: 0279 / 50.0/ 50.0/ 1. 43.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 562019.000/ 3917469.000/
H= 0.000 DH= 0.000/
                                                                                    0.000/rms=175.00
S [V/A]: +0.000e+000 +0.000e+000 +1.680e+001 +3.150e+001 +4.479e+001
+5.720e+001 +6.701e+001 +7.576e+001 +8.728e+001 +1.011e+002 +1.116e+002 +1.188e+002 +1.245e+002 +1.270e+002 +1.268e+002 +1.256e+002 +1.235e+002 +1.209e+002 +1.186e+002 +1.167e+002 +1.141e+002 +1.108e+002 +1.079e+002 +1.055e+002 +1.026e+002 +9.952e+001 +9.714e+001 +9.503e+001 +9.199e+001
+8.716e+001 +8.148e+001 +7.523e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.600e-001 +7.330e-001 +6.690e-001 +6.450e-001 +6.150e-001 +5.470e-001 +4.480e-001
+3.320e-001 +1.800e-001 +3.700e-002 -4.100e-002 -7.700e-002 -9.700e-002 -1.060e-001 -1.110e-001 -1.190e-001 -1.310e-001 -1.450e-001 -1.530e-001 -1.530e-001 -1.450e-001 -1.620e-001 -2.110e-001 -3.030e-001 -3.890e-001 -4.440e-001
    3.4949
                   0.57
                  24.34
 388.8855
 200.0000
                  41.26
                 138.14
   61.4015
   17.2671 10000000000.00
<Date: Mon Sep 15 09:54:53 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: FENCES, POWER-LINE</pre>
<Place: ROUMELI
*****
                             / 50.0/ 50.0/ 1.0/ 562003.000/ 3917252.000/
#GEOSEC: 0280-A
42.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                  0.000/\text{rms}=228.00
                                              Σελίδα 109
```

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1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +0.000e+000 +1.149e+001 +2.164e+001 +2.662e+001 +2.772e+001 +2.753e+001 +2.724e+001 +2.698e+001 +2.684e+001 +2.691e+001 +2.714e+001 +2.764e+001 +2.851e+001 +2.949e+001 +3.047e+001 +3.183e+001
+3.356e+001 +3.510e+001 +3.645e+001 +3.818e+001 +4.035e+001 +4.236e+001
+4.428e+001 +4.689e+001 +5.010e+001 +5.253e+001 +5.417e+001 +5.525e+001
+5.498e+001 +5.363e+001 +5.183e+001 +4.896e+001 +4.466e+001 +4.013e+001
+3.557e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +5.490e-001 +5.900e-002 -5.300e-002 -6.000e-002 -3.800e-002 -3.000e-003 +3.800e-002
+7.600e-002 +1.220e-001 +1.720e-001 +2.070e-001 +2.280e-001 +2.440e-001 +2.530e-001 +2.550e-001 +2.550e-001 +2.550e-001 +2.720e-001 +2.890e-001 +3.050e-001 +3.130e-001 +2.920e-001 +2.400e-001 +1.660e-001 +4.800e-002 -9.100e-002 -1.880e-001 -2.560e-001 -3.330e-001 -4.190e-001 -4.720e-001
 -4.920e-001
     4.1727
49.3292
                                 0.51
                               10.00
     27.9183
                               21.37
     83.4259
                             142.72
       7.8487 10000000000.00
<Date: Mon Sep 15 10:15:26 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                                                6 Ampl=OFF
<Remark: FENCES</pre>
*****
                                                                                         1.0/ 561778.000/ 3917258.000/
#GEOSEC: 0281
                                                      50.0/ 50.0/
41.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                         0.000 DH =
                                                                                                                                               0.000/rms = 97.00
S [V/A]: +5.139e+000 +7.045e+000 +9.175e+000 +1.089e+001 +1.254e+001 +1.377e+001 +1.434e+001 +1.461e+001 +1.477e+001 +1.490e+001 +1.506e+001
+1.528e+001 +1.565e+001 +1.625e+001 +1.687e+001 +1.746e+001 +1.823e+001
+1.916e+001 +1.996e+001 +2.067e+001 +2.160e+001 +2.277e+001 +2.381e+001
+2.468e+001 +2.564e+001 +2.635e+001 +2.644e+001 +2.611e+001 +2.522e+001 +2.370e+001 +2.223e+001 +2.092e+001 =7.940e-001 -6.890e-001 +5.060e-001 +2.920e-001 +1.620e-001 +9.00e-002 +5.00e-002 +7.900e-002 +7.900e-
+1.120e-001 +1.530e-001 +1.950e-001 +2.210e-001 +2.330e-001 +2.370e-001
+2.360e-001 +2.360e-001 +2.390e-001 +2.470e-001 +2.540e-001 +2.500e-001 +2.300e-001 +1.750e-001 +7.200e-002 -3.700e-002 -1.340e-001 -2.330e-001
 -3.080e-001 -3.450e-001 -3.670e-001
       4.1217
                                 0.49
     20.4243
                                10.00
                               12.12
72.75
     16.4391
     38.3007
       5.6951 10000000000.00
<Date: Mon Sep 15 11:19:53 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                                                                6 Ampl=OFF
<Remark: IN GRAPES, FENCES</pre>
<Place: ROUMELI
 <
*****
#GEOSEC: 0282
                                                      49.0/ 49.0/
                                                                                         1.0/ 561538.000/ 3917285.000/
41.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
S [V/A]: +0.000e+000 +1.572e+000 +1.680e+001 +2.370e+001 +2.665e+001
                                                                                                                                               0.000/rms=187.00
+2.690e+001 +2.635e+001 +2.576e+001 +2.512e+001 +2.454e+001 +2.430e+001 +2.428e+001 +2.452e+001 +2.514e+001 +2.592e+001 +2.672e+001 +2.782e+001 +2.910e+001 +3.004e+001 +3.066e+001 +3.108e+001 +3.105e+001 +3.059e+001
+2.989e+001 +2.864e+001 +2.668e+001 +2.471e+001 +2.284e+001 +2.048e+001
+1.790e+001 +1.602e+001 +1.466e+001 +1.332e+001 +1.222e+001 +1.165e+001
+1.140e+001
                         -9.000e-001 -9.000e-001 -9.000e-001 -8.490e-001 +3.120e-001
Err[V/A]:
-4.300e-002 -1.260e-001 -1.360e-001 -1.200e-001 -7.800e-002 -2.900e-002
+2.000e-002 +8.500e-002 +1.480e-001 +1.900e-001 +2.120e-001 +2.180e-001
+1.980e-001 +1.590e-001 +1.100e-001 +3.900e-002 -5.000e-002 -1.250e-001 -1.880e-001 -2.660e-001 -3.480e-001 -3.990e-001 -4.290e-001 -4.480e-001 -4.540e-001 -4.470e-001 -4.310e-001 -3.910e-001 -3.080e-001 -2.020e-001
 -8.900e-002
     14.3404
                                 0.41
     28.3865
                               10.70
```

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1D_Inversion_Results_TEM.txt
   20.2267
                  10.00
   36.4419
                  49.99
    3.8501 10000000000.00
<Date: Mon Sep 15 12:21:11 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: NOT SQUARE</pre>
<Place: ROUMELI
<***************************
*****
#GEOSEC: 0283-A / 50.0/ 50.0/ 1.0/ 561765.000/ 3917668.000/ 24.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ S [V/A]: +0.000e+000 +2.125e+001 +3.827e+001 +4.478e+001 +4.664e+001
                                                                                   0.000/rms=124.00
+4.575e+001 +4.479e+001 +4.440e+001 +4.452e+001 +4.545e+001 +4.684e+001
+4.844e+001 +5.092e+001 +5.445e+001 +5.792e+001 +6.117e+001 +6.542e+001
+7.054e+001 +7.480e+001 +7.840e+001 +8.273e+001 +8.759e+001 +9.150e+001 +9.474e+001 +9.848e+001 +1.023e+002 +1.045e+002 +1.057e+002 +1.058e+002 +1.040e+002 +1.012e+002 +9.806e+001 +9.369e+001 +8.788e+001 +8.210e+001
+7.608e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.900e-001 -5.240e-001 +6.500e-002 -9.900e-002 -8.100e-002 -2.400e-002 +5.200e-002 +1.350e-001 +1.960e-001 +2.410e-001 +2.870e-001 +3.270e-001 +3.570e-001 +3.570e-001 +3.540e-001
+3.400e-001 +3.210e-001 +3.040e-001 +2.830e-001 +2.610e-001 +2.430e-001
+2.260e-001 +1.990e-001 +1.540e-001 +1.010e-001 +4.400e-002 -3.600e-002
-1.250e-001 -1.850e-001 -2.230e-001 -2.630e-001 -3.200e-001 -3.830e-001
-4.320e-001
 139.4967
   37.0237
                  19.55
                 87.06
142.28
 200.0000
   94.2233
   24.1395 10000000000.00
<Date: Mon Sep 15 12:56:48 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: ONLY OLIVE TREES
<Place: ROUMELI</pre>
*****
#GEOSEC: 0284-B / 50.0/ 50.0/ 1. 22.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 561285.000/ 3918218.000/
                                                              0.000 DH =
                                                                                   0.000/\text{rms}=383.00
             +6.220e-001 +2.050e+001 +3.045e+001 +3.472e+001 +3.669e+001
S [V/A]:
+3.691e+001 +3.663e+001 +3.647e+001 +3.640e+001 +3.640e+001 +3.626e+001
+3.588e+001 +3.510e+001 +3.397e+001 +3.305e+001 +3.244e+001 +3.200e+001 +3.190e+001 +3.210e+001 +3.240e+001 +3.287e+001 +3.352e+001 +3.415e+001 +3.480e+001 +3.581e+001 +3.735e+001 +3.891e+001 +4.035e+001 +4.194e+001
+4.289e+001 +4.253e+001 +4.143e+001 +3.951e+001 +3.731e+001 +3.603e+001
+3.553e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.350e-001 -4.880e-001 +1.530e-001 -1.100e-002 -3.300e-002 -1.900e-002 -6.000e-003 -1.200e-002 -4.800e-002 -9.200e-002 -1.340e-001 -1.530e-001 -1.380e-001 -1.020e-001 -4.800e-002
+1.300e-002 +5.100e-002 +7.200e-002 +8.700e-002 +1.020e-001 +1.200e-001
+1.430e-001 +1.800e-001 +2.230e-001 +2.430e-001 +2.330e-001 +1.660e-001 +2.300e-002 -1.190e-001 -2.110e-001 -2.550e-001 -2.270e-001 -1.440e-001
-4.600e-002
   34.2145
                  83.34
                 114.79
 110.6951
    1.7584
                  10.10
 200.0000
                 150.00
    9.6346 10000000000.00
<Date: Mon Sep 15 14:08:49 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: FENCES
#GEOSEC: 0285-B / 50.0 / 50.0 / 1.21.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/
                                                           561478.000/ 3918104.000/
                                                              0.000 DH =
                                                                                   0.000/rms=111.00
             +0.000e+000 +5.460e-001 +7.897e+000 +1.123e+001 +1.298e+001
+1.383e+001 +1.431e+001 +1.471e+001 +1.521e+001 +1.585e+001 +1.648e+001
+1.710e+001 +1.797e+001 +1.908e+001 +2.009e+001 +2.095e+001 +2.200e+001
                                             Σελίδα 111
```

```
1D_Inversion_Results_TEM.txt
+2.321e+001 +2.426e+001 +2.523e+001 +2.658e+001 +2.840e+001 +3.013e+001 +3.172e+001 +3.375e+001 +3.604e+001 +3.772e+001 +3.894e+001 +4.002e+001
+4.061e+001 +4.047e+001 +3.990e+001 +3.865e+001 +3.657e+001 +3.452e+001
+3.269e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.610e-001 +4.650e-001 +2.200e-001 +1.760e-001 +1.730e-001 +1.810e-001 +2.040e-001 +2.300e-001 +2.510e-001 +2.720e-001 +2.840e-001 +2.820e-001 +2.730e-001 +2.610e-001
+2.530e-001 +2.580e-001 +2.730e-001 +2.980e-001 +3.250e-001 +3.390e-001 +3.400e-001 +3.240e-001 +2.860e-001 +2.390e-001 +1.880e-001 +1.160e-001 +2.100e-002 -6.200e-002 -1.330e-001 -2.120e-001 -2.820e-001 -3.190e-001
-3.410e-001
   16.9534
                    16.33
   52.3237
                  135.08
    8.6117
                    37.61
    4.2988
                    50.87
    1.0000 10000000000.00
<Date: Mon Sep 15 14:34:23 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: FENCES
<Place: PANORMOS
*****
#GEOSEC: 0286-A / 50.0/ 50.0/ 1.
20.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 561649.000/ 3918105.000/
                                                                   0.000 DH=
                                                                                           0.000/\text{rms}=289.00
    [V/A]: +0.000e+000 +0.000e+000 +3.519e+000 +9.891e+000 +1.612e+001
+2.076e+001 +2.288e+001 +2.381e+001 +2.425e+001 +2.433e+001 +2.436e+001
+2.455e+001 +2.501e+001 +2.587e+001 +2.681e+001 +2.771e+001 +2.894e+001
+3.058e+001 +3.222e+001 +3.392e+001 +3.641e+001 +3.968e+001 +4.235e+001 +4.426e+001 +4.591e+001 +4.698e+001 +4.760e+001 +4.820e+001 +4.905e+001
+4.977e+001 +4.962e+001 +4.871e+001 +4.663e+001 +4.319e+001 +3.964e+001
+3.610e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.910e-001 +6.520e-001 +3.590e-001 +1.800e-001 +5.800e-002 +1.100e-002 +3.200e-002 +7.300e-002 +1.280e-001 +1.830e-001 +2.130e-001 +2.290e-001 +2.480e-001
+2.810e-001 +3.210e-001 +3.570e-001 +3.870e-001 +3.810e-001 +3.290e-001
+2.550e-001 +1.610e-001 +9.300e-002 +8.300e-002 +9.200e-002 +8.600e-002
+2.300e-002 -7.700e-002 -1.760e-001 -2.800e-001 -3.710e-001 -4.310e-001
-4.660e-001
   24.7469
                    24.01
   77.8949
                    99.89
                    75.76
   12.2748
    1.0000 10000000000.00
<Date: Mon Sep 15 14:58:57 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: FENCES, NEXT TO RIVER</pre>
<Place: PANORMOS
*****
#GEOSEC: 0287-B / 50.0 / 50.0 / 1.38.0 / 36/4 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 562346.000/ 3918269.000/
                                                                                           0.000/rms=201.00
                                                                    0.000 DH=
S [V/A]: +8.383e+001 +7.037e+001 +6.531e+001 +6.349e+001 +6.302e+001 +6.358e+001 +6.384e+001 +6.340e+001 +6.173e+001 +5.861e+001 +5.573e+001
+5.349e+001 +5.133e+001 +4.970e+001 +4.895e+001 +4.860e+001 +4.836e+001
+4.815e+001 +4.789e+001 +4.757e+001 +4.703e+001 +4.624e+001 +4.547e+001 +4.472e+001 +4.362e+001 +4.194e+001 +4.011e+001 +3.813e+001 +3.525e+001 +3.146e+001 +2.820e+001 +2.547e+001 +2.235e+001 +1.913e+001 +1.681e+001
+1.504e+001
Err[V/A]: +4.830e-001 +3.910e-001 +2.350e-001 +1.030e-001 -1.000e-003 +2.900e-002 -1.400e-002 -8.700e-002 -1.810e-001 -2.460e-001 -2.570e-001 -2.360e-001 -1.850e-001 -1.160e-001 -6.600e-002 -3.900e-002 -2.400e-002
-2.700e-002 -3.900e-002 -5.400e-002 -7.200e-002 -9.000e-002 -1.060e-001 -1.240e-001 -1.590e-001 -2.210e-001 -2.830e-001 -3.390e-001 -3.960e-001
-4.390e-001 -4.590e-001 -4.680e-001 -4.730e-001 -4.750e-001 -4.760e-001
-4.760e-001
   68.1007
                    17.71
   36.0858
                    45.03
   22.7077
                    48.34
    2.6186 10000000000.00
```

```
1D_Inversion_Results_TEM.txt
<Date: Tue Sep 16 08:17:57 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                         6 Ampl=OFF
<Remark: POWER LINES, NEXT TO ROAD</pre>
<Place: PANORMOS
*****
#GEOSEC: 0288-A / 50.0/ 50.0/ 1.
17.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                 1.0/ 561915.000/ 3918150.000/
                                                                                  0.000/rms=103.00
                                                            0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +8.189e+000 +1.447e+001 +1.808e+001
+1.996e+001 +2.104e+001 +2.190e+001 +2.299e+001 +2.438e+001 +2.564e+001 +2.682e+001 +2.843e+001 +3.042e+001 +3.215e+001 +3.355e+001 +3.510e+001
+3.650e+001 +3.731e+001 +3.775e+001 +3.801e+001 +3.799e+001 +3.774e+001
+3.740e+001 +3.686e+001 +3.616e+001 +3.558e+001 +3.507e+001 +3.441e+001
+3.345e+001 +3.236e+001 +3.113e+001 +2.923e+001 +2.666e+001 +2.446e+001
+2.267e+001
Err[V/A]:
             +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +6.510e-001
+3.350e-001 +2.600e-001 +2.500e-001 +2.580e-001 +2.720e-001 +2.850e-001
+2.980e-001 +3.110e-001 +3.100e-001 +2.940e-001 +2.670e-001 +2.190e-001
+1.550e-001 +1.020e-001 +6.200e-002 +1.900e-002 -2.200e-002 -5.100e-002 -7.100e-002 -8.600e-002 -9.500e-002 -9.700e-002 -1.020e-001 -1.200e-001 -1.650e-001 -2.230e-001 -2.810e-001 -3.440e-001 -3.900e-001 -4.060e-001
-4.120e-001
  22.7962
56.7504
                  12.89
                  50.34
90.78
  19.1996
    3.9042 10000000000.00
<Date: Tue Sep 16 09:01:25 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                         6 Ampl=OFF
<Remark: FENCES
<Place: PANORMOS
*****
#GEOSEC: 0289-A / 50.0/ 50.0/ 1.0/ 562052.000/ 3918309.000/ 22.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/S [V/A]: +0.000e+000 +6.048e+000 +1.680e+001 +2.074e+001 +2.208e+001
                                                                                  0.000/rms = 249.00
+2.206e+001 +2.187e+001 +2.181e+001 +2.190e+001 +2.224e+001 +2.274e+001
+2.330e+001 +2.417e+001 +2.536e+001 +2.642e+001 +2.728e+001 +2.817e+001 +2.885e+001 +2.910e+001 +2.912e+001 +2.899e+001 +2.880e+001 +2.874e+001
+2.885e+001 +2.926e+001 +3.017e+001 +3.128e+001 +3.244e+001 +3.396e+001
+3.542e+001 +3.595e+001 +3.570e+001 +3.458e+001 +3.260e+001 +3.087e+001
+2.958e+001
+1.770e-001 +2.120e-001 +2.290e-001 +2.230e-001 +1.980e-001 +1.480e-001 +7.900e-002 +2.500e-002 -8.000e-003 -2.800e-002 -2.100e-002 +9.000e-003 +5.000e-002 +1.110e-001 +1.840e-001 +2.310e-001 +2.500e-001 +2.300e-001 +1.400e-001 +1.500e-002 -1.060e-001 -2.190e-001 -2.810e-001 -2.810e-001
-2.610e-001
   23.1947
                  18.98
   51.0468
                  11.28
   32.5658
                150.00
    4.0000 10000000000.00
<Date: Tue Sep 16 09:22:59 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                         6 Ampl=OFF
*****
#GEOSEC: 0290-A / 50.0/ 50.0/ 1.
89.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 561535.000/ 3915121.000/
                                                            0.000 DH =
                                                                                  0.000/\text{rms}=155.00
S [V/A]: +0.000e+000 +0.000e+000 +5.456e+000 +1.161e+001 +1.670e+001
+2.018e+001 +2.184e+001 +2.272e+001 +2.333e+001 +2.369e+001 +2.385e+001
+2.395e+001 +2.407e+001 +2.423e+001 +2.436e+001 +2.447e+001 +2.461e+001 +2.481e+001 +2.505e+001 +2.533e+001 +2.583e+001 +2.662e+001 +2.748e+001 +2.836e+001 +2.964e+001 +3.135e+001 +3.289e+001 +3.425e+001 +3.581e+001 +3.713e+001 +3.749e+001 +3.708e+001 +3.567e+001 +3.303e+001 +3.044e+001
+2.820e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.460e-001
                                             Σελίδα 113
```

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1D_Inversion_Results_TEM.txt
+5.390e-001 +3.180e-001 +1.980e-001 +1.070e-001 +5.200e-002 +3.200e-002 +2.800e-002 +2.900e-002 +3.100e-002 +3.100e-002 +3.100e-002 +3.500e-002 +4.900e-002 +6.800e-002 +9.200e-002 +1.260e-001 +1.680e-001 +2.010e-001 +2.270e-001 +2.540e-001 +2.730e-001 +2.760e-001 +2.620e-001 +2.140e-001 +1.110e-001 -1.400e-002 -1.380e-001 -2.700e-001 -3.650e-001 -4.010e-001
-4.180e-001
   13.8250
                      1.69
   26.8906
                    53.29
                   109.44
   58.0233
     4.5379 10000000000.00
<Date: Tue Sep 16 10:11:23 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                   6 Ampl=OFF
<Remark: FENCES, POWERLINES, IN VILLAGE</pre>
*****
                                   50.0/ 50.0/
                                                        1.0/ 561668.000/ 3915426.000/
#GEOSEC: 0291-B
90.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                             0.000/\text{rms} = 83.00
                                                                   0.000 \, \text{DH} =
S [V/A]: +4.128e+001 +3.944e+001 +3.908e+001 +3.887e+001 +3.836e+001 +3.738e+001 +3.628e+001 +3.524e+001 +3.394e+001 +3.244e+001 +3.129e+001 +3.037e+001 +2.933e+001 +2.825e+001 +2.745e+001 +2.688e+001 +2.630e+001
+2.588e+001 +2.578e+001 +2.591e+001 +2.637e+001 +2.734e+001 +2.850e+001
+2.973e+001 +3.143e+001 +3.356e+001 +3.529e+001 +3.669e+001 +3.814e+001 +3.911e+001 +3.887e+001 +3.753e+001
Err[V/A]: +2.280e-001 +9.800e-002 +3.700e-002 +4.600e-002 -8.600e-002
-1.360e-001 -1.680e-001 -1.840e-001 -1.950e-001 -1.970e-001 -1.930e-001 -1.870e-001 -1.790e-001 -1.660e-001 -1.500e-001 -1.320e-001 -9.900e-002
-4.700e-002 +8.000e-003 +6.300e-002 +1.340e-001 +2.110e-001 +2.630e-001 +2.920e-001 +3.070e-001 +2.990e-001 +2.760e-001 +2.420e-001 +1.730e-001 +3.600e-002 -1.450e-001 -3.030e-001
   35.8783
                    12.65
   22.2982
                    40.80
  143.1713
                    95.52
     6.7816 1000000000000000000
<Date: Tue Sep 16 10:43:07 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                   6 Ampl=OFF
<Remark: POWERLINES, IN VILLAGE, PUMP</pre>
<Place: AGGELIANA
<
*****
#GEOSEC: 0292-B / 49.0/ 49.0/ 1.0
107.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
0.000/rms=205.00
                                                          1.0/ 561519.000/ 3915680.000/
                                                                       0.000 DH =
               +0.000e+000 +0.000e+000 +2.825e+001 +4.595e+001 +5.804e+001
+6.267e+001 +6.245e+001 +6.098e+001 +5.838e+001 +5.503e+001 +5.249e+001 +5.073e+001 +4.923e+001 +4.833e+001 +4.813e+001 +4.817e+001 +4.832e+001 +4.832e+001 +4.738e+001 +4.614e+001 +4.400e+001 +4.159e+001
+3.910e+001 +3.562e+001 +3.124e+001 +2.770e+001 +2.484e+001 +2.170e+001
+1.861e+001 +1.645e+001 +1.483e+001 +1.307e+001 +1.128e+001 +9.950e+000
+8.921e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -8.970e-001 +6.420e-001
+1.380e-001 -9.000e-002 -1.800e-001 -2.350e-001 -2.510e-001 -2.310e-001
-1.910e-001 -1.270e-001 -5.300e-002 -8.000e-003 +1.100e-002 +9.000e-003 -2.200e-002 -6.500e-002 -1.130e-001 -1.810e-001 -2.650e-001 -3.330e-001 -3.830e-001 -4.290e-001 -4.590e-001 -4.710e-001 -4.740e-001 -4.740e-001 -4.730e-001 -4.670e-001 -4.700e-001 -4.730e-001
-4.750e-001
   58.7773
                     21.09
   31.1070
                    21.91
   24.6041
                     33.03
    2.0389 10000000000.00
<Date: Tue Sep 16 11:19:05 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                   6 Ampl=OFF
<Remark: POWERLINES, NOT SQUARE, FENCES</pre>
*****
#GEOSEC: 0293-A
                                / 50.0/ 50.0/ 1.0/ 561094.000/ 3915749.000/
                                                   Σελίδα 114
```

```
1D_Inversion_Results_TEM.txt
85.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +0.000e+000 +2.661e+001 +5.572e+001 +7.406e+001 +8.892e+001
+9.875e+001 +1.042e+002 +1.083e+002 +1.131e+002 +1.183e+002 +1.219e+002
+1.245e+002 +1.265e+002 +1.273e+002 +1.263e+002 +1.241e+002 +1.195e+002
                                                                                                   0.000/\text{rms}=297.00
+1.118e+002 +1.039e+002 +9.655e+001 +8.726e+001 +7.688e+001 +6.895e+001 +6.280e+001 +5.609e+001 +4.939e+001 +4.467e+001 +4.107e+001 +3.711e+001 +3.303e+001 +2.992e+001 +2.742e+001 +2.449e+001 +2.126e+001 +1.871e+001
+1.662e+001
                 -9.000e-001 -9.000e-001 -9.000e-001 -8.410e-001 +5.960e-001
Err[V/A]:
+3.470e-001 +2.570e-001 +2.330e-001 +2.160e-001 +1.860e-001 +1.510e-001 +1.140e-001 +6.200e-002 -1.100e-002 -8.500e-002 -1.560e-001 -2.450e-001 -3.310e-001 -3.830e-001 -4.120e-001 -4.340e-001 -4.460e-001 -4.500e-001 -4.490e-001 -4.450e-001 -4.390e-001 -4.330e-001 -4.290e-001 -4.270e-001
-4.290e-001 -4.360e-001 -4.430e-001 -4.550e-001 -4.690e-001 -4.790e-001
-4.860e-001
 100.8773
  386.3859
                      30.71
   15.1154
                      36.47
     5.3400 10000000000.00
<Date: Tue Sep 16 11:45:15 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                        6 Ampl=OFF
<Remark: NEAR LITTLE RIVER</pre>
<Place: AGGELIANA
<
*****
#GEOSEC: 0294-B
                                     50.0/ 50.0/
                                                           1.0/ 560757.000/ 3915883.000/
65.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                        0.000 DH=
                                                                                                   0.000/rms = 92.00
S [V/A]: +0.000e+000 +4.920e-001 +2.357e+001 +3.547e+001 +4.123e+001 +4.172e+001 +4.044e+001 +3.918e+001 +3.779e+001 +3.646e+001 +3.570e+001
+3.526e+001 +3.501e+001 +3.509e+001 +3.541e+001 +3.581e+001 +3.641e+001
+3.714e+001 +3.768e+001 +3.804e+001 +3.831e+001 +3.834e+001 +3.816e+001
+3.789e+001 +3.748e+001 +3.698e+001 +3.661e+001 +3.634e+001 +3.607e+001
+3.583e+001 +3.566e+001 +3.550e+001 +3.523e+001 +3.472e+001 +3.401e+001 +3.308e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.810e-001 +3.900e-001 -6.800e-002 -1.790e-001 -1.890e-001 -1.730e-001 -1.370e-001 -9.800e-002
-6.200e-002 -1.600e-002 +3.300e-002 +6.500e-002 +8.300e-002 +9.400e-002 +9.000e-002 +7.500e-002 +5.400e-002 +2.300e-002 -1.300e-002 -3.900e-002 -5.400e-002 -6.300e-002 -6.200e-002 -5.500e-002 -4.700e-002 -3.700e-002 -3.000e-002 -3.000e-002 -3.700e-002 -5.600e-002 -9.800e-002 -1.560e-001
-2.140e-001
   39.4465
                      20.03
   21.1808
                      10.00
   78.4025
                      25.36
   30.4203 10000000000.00
<Date: Tue Sep 16 12:22:05 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                        6 Ampl=OFF
<Remark: NEAR G-12 DRILL</pre>
<Place: AGGELIANA
<
*****
                                                           1.0/ 561182.000/ 3915571.000/
#GEOSEC: 0295-B / 50.0/ 50.0/ 1.0
98.0/32/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                                        0.000 DH =
                                                                                                   0.000/\text{rms}=288.00
S [V/A]: +0.000e+000 +7.446e+000 +3.346e+001 +4.869e+001 +5.906e+001 +6.234e+001 +6.135e+001 +5.973e+001 +5.805e+001 +5.710e+001 +5.716e+001 +5.760e+001 +5.841e+001 +5.924e+001 +5.960e+001 +5.964e+001 +5.944e+001
+5.919e+001 +5.920e+001 +5.951e+001 +6.030e+001 +6.159e+001 +6.254e+001
+6.289e+001 +6.235e+001 +6.037e+001 +5.820e+001 +5.644e+001 +5.496e+001
+5.471e+001 +5.603e+001 +5.847e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.800e-001 +5.440e-001 +5.800e-002 -1.290e-001 -1.570e-001 -1.140e-001 -3.100e-002 +3.100e-002
+6.300e-002 +7.200e-002 +4.900e-002 +1.800e-002 -6.000e-003 -2.000e-002
-9.000e-003 +2.000e-002 +5.300e-002 +8.700e-002 +9.600e-002 +6.200e-002 -1.000e-003 -9.800e-002 -1.840e-001 -2.060e-001 -1.790e-001 -9.000e-002
+6.700e-002 +2.210e-001 +3.510e-001
58.9127 57.65
   66.1541
                      58.46
   35.5053 10000000000.00
```

```
1D_Inversion_Results_TEM.txt
<Date: Tue Sep 16 13:28:16 2008</pre>
<Time Range=5 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: POWER-LINES, FENCES</pre>
<Place: AGGELIANA
*****
#GEOSEC: 0296-B / 50.0/ 50.0/ 1.
93.0/35/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                          1.0/ 560978.000/ 3915555.000/
                                                                      0.000 DH=
                                                                                               0.000/\text{rms}=135.00
S [V/A]: +0.000e+000 +0.000e+000 +2.758e+000 +1.241e+001 +1.986e+001
+2.473e+001 +2.745e+001 +2.939e+001 +3.156e+001 +3.402e+001 +3.604e+001 +3.774e+001 +3.977e+001 +4.195e+001 +4.358e+001 +4.480e+001 +4.610e+001
+4.736e+001 +4.826e+001 +4.894e+001 +4.964e+001 +5.024e+001 +5.047e+001
+5.046e+001 +5.018e+001 +4.967e+001 +4.931e+001 +4.919e+001 +4.936e+001
+4.996e+001 +5.054e+001 +5.084e+001 +5.057e+001 +4.904e+001 +4.677e+001 

Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.850e-001 

+6.260e-001 +4.550e-001 +3.870e-001 +3.480e-001 +3.230e-001 +3.050e-001
+2.890e-001 +2.660e-001 +2.310e-001 +1.990e-001 +1.730e-001 +1.450e-001
+1.190e-001 +1.020e-001 +8.900e-002 +7.000e-002 +4.100e-002 +1.100e-002 -1.500e-002 -4.000e-002 -4.600e-002 -2.900e-002 -1.000e-003 +3.800e-002 +6.400e-002 +5.300e-002 +9.000e-003 -8.500e-002 -2.110e-001 -3.030e-001
     1.9123
                      0.25
                     24.43
   50.8254
   75.7182
                     25.28
   48.4566 10000000000.00
<Date: Tue Sep 16 13:57:05 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                    6 Ampl=OFF
<Remark: ON THE HILL
*****
#GEOSEC: 0297-A / 50.0/ 50.0/ 1.76.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                           1.0/ 560304.000/ 3917574.000/
                                                                       0.000 DH=
                                                                                               0.000/rms=148.00
S [V/A]: +0.000e+000 +0.000e+000 +1.193e+001 +3.330e+001 +5.154e+001 +6.574e+001 +7.497e+001 +8.233e+001 +9.123e+001 +1.012e+002 +1.086e+002
+1.142e+002 +1.202e+002 +1.264e+002 +1.314e+002 +1.355e+002 +1.402e+002
+1.142e+002 +1.202e+002 +1.204e+002 +1.314e+002 +1.333e+002 +1.402e+002 +1.444e+002 +1.461e+002 +1.455e+002 +1.417e+002 +1.328e+002 +1.223e+002 +1.120e+002 +9.867e+001 +8.341e+001 +7.189e+001 +6.291e+001 +5.322e+001 +4.381e+001 +3.732e+001 +3.260e+001 +2.771e+001 +2.305e+001 +1.984e+001
+1.747e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 +8.820e-001 +6.950e-001 +5.680e-001 +5.170e-001 +4.720e-001 +4.100e-001 +3.490e-001
+3.000e-001 +2.560e-001 +2.260e-001 +2.120e-001 +1.980e-001 +1.670e-001 +1.020e-001 +1.700e-002 -8.200e-002 -2.170e-001 -3.480e-001 -4.190e-001 -4.530e-001 -4.750e-001 -4.860e-001 -4.910e-001 -4.920e-001 -4.930e-001
-4.930e-001 -4.930e-001 -4.920e-001 -4.910e-001 -4.900e-001 -4.890e-001
-4.890e-001
   11.0195
                      1.51
  208.3373
                     70.48
                     45.55
   35.0161
    1.7631 10000000000.00
<Date: Thu Sep 18 08:53:01 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                    6 Ampl=OFF
<Remark: FENCES</pre>
*****
                                   50.0/ 50.0/
#GEOSEC: 0298-A
                                                         1.0/ 560574.000/ 3917639.000/
80.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                       0.000 DH=
                                                                                               0.000/\text{rms}=219.00
S [V/A]: +0.000e+000 +1.029e+001 +5.140e+001 +8.391e+001 +1.193e+002 +1.478e+002 +1.608e+002 +1.673e+002 +1.721e+002 +1.753e+002 +1.762e+002 +1.760e+002 +1.743e+002 +1.703e+002 +1.652e+002 +1.599e+002 +1.528e+002 +1.454e+002 +1.407e+002 +1.381e+002 +1.381e+002 +1.371e+002 +1.371e+002 +1.370e+002
+1.372e+002 +1.341e+002 +1.259e+002 +1.158e+002 +1.059e+002 +9.338e+001
+8.000e+001 +7.018e+001 +6.269e+001 +5.442e+001 +4.573e+001 +3.906e+001
+3.370e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +8.500e-001 +5.840e-001 +3.300e-001 +2.020e-001 +1.180e-001 +5.400e-002 +9.000e-003 -2.900e-002 -8.000e-002 -1.430e-001 -1.930e-001 -2.220e-001 -2.320e-001
                                                    Σελίδα 116
```

```
1D_Inversion_Results_TEM.txt
-2.050e-001 -1.530e-001 -9.300e-002 -2.400e-002 +1.800e-002 +1.000e-015 -6.900e-002 -2.030e-001 -3.510e-001 -4.240e-001 -4.540e-001 -4.700e-001 -4.760e-001 -4.770e-001 -4.790e-001 -4.830e-001 -4.900e-001 -4.950e-001
-4.970e-001
 16.2598
278.9301
64.2664
                      1.19
                     58.12
                   110.26
     3.5615 10000000000.00
<Date: Thu Sep 18 09:29:33 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                     6 Ampl=OFF
<Remark: FENCES
*****
#GEOSEC: 0299-A / 50.0/ 50.0/ 1. 68.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                           1.0/ 560715.000/ 3917843.000/
                                                                      0.000 DH=
                                                                                               0.000/\text{rms}=291.00
S [V/A]: +0.000e+000 +0.000e+000 +1.928e+001 +4.209e+001 +6.402e+001
+8.396e+001 +9.810e+001 +1.096e+002 +1.235e+002 +1.391e+002 +1.502e+002
+1.575e+002 +1.629e+002 +1.646e+002 +1.637e+002 +1.531e+002 +1.599e+002 +1.569e+002 +1.535e+002 +1.4495e+002 +1.431e+002 +1.340e+002 +1.257e+002 +1.185e+002 +1.099e+002 +1.004e+002 +9.303e+001 +8.702e+001 +8.004e+001 +7.253e+001 +6.678e+001 +6.222e+001 +5.702e+001 +5.129e+001 +4.651e+001
+4.224e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.830e-001 +7.510e-001 +6.420e-001 +5.860e-001 +5.330e-001 +4.530e-001 +3.550e-001
+2.500e-001 +1.210e-001 +6.000e-003 -5.000e-002 -7.000e-002 -8.400e-002 -1.100e-001 -1.520e-001 -2.000e-001 -2.600e-001 -3.120e-001 -3.400e-001 -3.530e-001 -3.630e-001 -3.710e-001 -3.760e-001 -3.810e-001 -3.870e-001 -3.910e-001 -3.920e-001 -3.940e-001 -4.000e-001 -4.200e-001 -4.450e-001
-4.650e-001
   14.5401
                      1.80
  300.0000
                     70.69
   60.4188
                     75.79
   17.0491 10000000000.00
<Date: Thu Sep 18 09:50:09 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                     6 Ampl=OFF
<Remark: FENCES
<Place: AGGELIANA
<
*****
#GEOSEC: 0300-A / 50.0/ 50.0/ 1.
46.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                           1.0/ 560849.000/ 3918027.000/
                                                                      0.000 DH =
                                                                                               0.000/rms=104.00
S [V/A]: +1.825e+002 +1.667e+002 +1.616e+002 +1.611e+002 +1.634e+002 +1.677e+002 +1.706e+002 +1.709e+002 +1.678e+002 +1.598e+002 +1.515e+002
+1.077e+002 +1.70de+002 +1.70de+002 +1.078e+002 +1.33de+002 +1.313e+002 +1.444e+002 +1.366e+002 +1.291e+002 +1.235e+002 +1.189e+002 +1.129e+002 +1.053e+002 +9.854e+001 +9.261e+001 +8.533e+001 +7.715e+001 +7.068e+001 +6.544e+001 +5.942e+001 +5.294e+001 +4.799e+001 +4.394e+001 +3.918e+001
+3.396e+001 +2.990e+001 +2.663e+001 +2.296e+001 +1.918e+001 +1.642e+001
+1.431e+001
Err[V/A]: +3.690e-001 +2.190e-001 +7.700e-002 -2.100e-002 +9.000e-002 +1.000e-001 +4.800e-002 -3.700e-002 -1.530e-001 -2.490e-001 -2.830e-001
-2.830e-001 -2.650e-001 -2.450e-001 -2.420e-001 -2.540e-001 -2.830e-001
-3.210e-001 -3.480e-001 -3.680e-001 -3.850e-001 -4.000e-001 -4.080e-001 -4.140e-001 -4.200e-001 -4.280e-001 -4.360e-001 -4.450e-001 -4.570e-001 -4.690e-001 -4.770e-001 -4.830e-001 -4.870e-001 -4.900e-001 -4.930e-001
-4.940e-001
 153.8239
                     48.26
   29.5561
                     39.10
    4.6059
                     30.11
     1.0000 10000000000.00
<Date: Thu Sep 18 10:10:03 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                     6 Ampl=OFF
<Remark: FENCES</pre>
<Place: PANORMOS
*****
                                 / 50.0/ 50.0/ 1.0/ 561174.000/ 3918116.000/
#GEOSEC: 0301-A
16.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                       0.000 DH =
                                                                                             0.000/\text{rms}=356.00
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +0.000e+000 +1.511e+001 +2.660e+001 +3.164e+001 +3.171e+001 +3.051e+001 +2.946e+001 +2.838e+001 +2.746e+001 +2.687e+001 +2.649e+001 +2.614e+001 +2.579e+001 +2.551e+001 +2.527e+001 +2.497e+001
+2.466e+001 +2.450e+001 +2.444e+001 +2.450e+001 +2.476e+001 +2.512e+001
+2.550e+001 +2.607e+001 +2.684e+001 +2.756e+001 +2.823e+001 +2.910e+001 +3.008e+001 +3.076e+001 +3.116e+001 +3.130e+001 +3.088e+001 +3.009e+001
+2.921e+001
Err[V/A]:
                   +5.000e-001 -9.000e-001 -9.000e-001 -8.980e-001 +4.240e-001
-1.080e-001 -2.050e-001 -2.020e-001 -1.710e-001 -1.330e-001 -1.050e-001 -8.400e-002 -6.900e-002 -6.300e-002 -6.400e-002 -6.500e-002 -6.300e-002 -4.900e-002 -2.700e-002 -2.000e-003 +3.200e-002 +6.900e-002 +9.500e-002 +1.130e-001 +1.310e-001 +1.490e-001 +1.610e-001 +1.670e-001 +1.650e-001 +1.460e-001 +1.090e-001 +6.000e-002 -1.700e-002 -1.120e-001 -1.760e-001
-2.200e-001
    25.9772
                          90.62
  117.9494
                        102.33
     2.3366
                         10.00
    49.9983
                          18.77
    50.0000 10000000000.00
<Date: Thu Sep 18 11:06:30 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                                       6 Ampl=OFF
<Remark: FENCES</pre>
<Place: PANORMOS
 <
*****
#GEOSEC: 0302-A / 50.0/ 50.0/ 1. 19.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                     1.0/ 561234.000/ 3917965.000/
                                                                                     0.000 DH =
                                                                                                                   0.000/rms=149.00
S [V/A]: +0.000e+000 +0.000e+000 +1.083e+001 +2.105e+001 +2.476e+001 +2.412e+001 +2.294e+001 +2.219e+001 +2.168e+001 +2.155e+001 +2.172e+001
+2.206e+001 +2.262e+001 +2.347e+001 +2.426e+001 +2.498e+001 +2.585e+001
+2.680e+001 +2.751e+001 +2.805e+001 +2.863e+001 +2.918e+001 +2.955e+001 +2.980e+001 +2.999e+001 +2.997e+001 +2.969e+001 +2.922e+001 +2.830e+001 +2.680e+001 +2.527e+001 +2.383e+001 +2.199e+001 +1.989e+001 +1.820e+001
+1.680e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +3.500e-001 -1.900e-001 -2.250e-001 -1.670e-001 -7.700e-002 +1.200e-002 +7.500e-002
Err[V/A]:
+1.180e-001 +1.540e-001 +1.820e-001 +1.930e-001 +1.930e-001 +1.820e-001 +1.620e-001 +1.410e-001 +1.240e-001 +1.040e-001 +8.300e-002 +6.500e-002 +4.700e-002 +1.700e-002 -3.100e-002 -8.400e-002 -1.390e-001 -2.100e-001 -2.840e-001 -3.310e-001 -3.600e-001 -3.840e-001 -4.030e-001 -4.150e-001
-4.250e-001
    23.0563
39.9014
                         23.30
55.29
      6.1206
                          10.00
    31.2429
                          30.70
      3.8764 10000000000.00
 <Date: Thu Sep 18 11:34:59 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                       6 Ampl=OFF
<Remark: FENCES
<Place: PANORMOS
 *****
#GEOSEC: 0303-B / 50.0/ 50.0/ 1.0/ 561176.000/ 3917718.000/ 25.0/36/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rr S [V/A]: +0.000e+000 +0.000e+000 +1.310e+001 +2.400e+001 +3.047e+001 +3.365e+001 +3.527e+001 +3.662e+001 +3.841e+001 +4.075e+001 +4.291e+001 +4.486e+001 +4.772e+001 +4.990e+001 +5.304e+001 +5.304e+001 +5.472e+001
                                                                                                                   0.000/rms=183.00
+5.458e+001 +5.455e+001 +5.422e+001 +5.344e+001 +5.187e+001 +4.984e+001 +4.755e+001 +4.414e+001 +3.971e+001 +3.611e+001 +3.325e+001 +3.020e+001
+2.747e+001 +2.586e+001 +2.497e+001 +2.447e+001 +2.468e+001 +2.543e+001
+2.634e+001
                   +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +6.730e-001
+3.200e-001 +2.400e-001 +2.400e-001 +2.560e-001 +2.760e-001 +2.860e-001 +2.840e-001 +2.670e-001 +2.300e-001 +1.840e-001 +1.370e-001 +7.900e-002 +1.900e-002 -2.400e-002 -5.900e-002 -1.100e-001 -1.870e-001 -2.620e-001 -3.230e-001 -3.790e-001 -4.160e-001 -4.260e-001 -4.220e-001 -4.010e-001
-3.470e-001 -2.720e-001 -1.790e-001 -4.100e-002 +1.160e-001 +2.100e-001
+2.660e-001
```

```
1D_Inversion_Results_TEM.txt
                              8.87
55.59
     30.8992
     67.0570
    21.3386
                               30.05
       9.7913
                              49.01
  200.0000 10000000000.00
<Date: Thu Sep 18 11:57:52 2008
<Time Range=6 Current= 3.70 Stack= 5 Filter=50 Deff=
<Remark: NEXT TO MARGARITIANOS RIVER</pre>
                                                                                                                           6 Ampl=OFF
<Place: PANORMOS
#GEOSEC: 0304-A / 50.0/ 50.0/ 1
53.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      1.0/ 560851.000/ 3917696.000/
                                                                                                        0.000 DH =
                                                                                                                                          0.000/rms=253.00
                       +0.000e+000 +0.000e+000 +5.202e+000 +2.535e+001 +4.425e+001
       [V/A]:
+6.089e+001 +7.194e+001 +7.991e+001 +8.812e+001 +9.569e+001 +1.003e+002 +1.030e+002 +1.048e+002 +1.049e+002 +1.035e+002 +1.013e+002 +9.758e+001
+9.195e+001 +8.651e+001 +8.163e+001 +7.584e+001 +7.000e+001 +6.614e+001 +6.363e+001 +6.147e+001 +5.996e+001 +5.913e+001 +5.829e+001 +5.660e+001
+5.317e+001 +4.915e+001 +4.522e+001 +4.037e+001 +3.526e+001 +3.166e+001 +2.902e+001
Err[V/A]:
                       +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.980e-001
+7.950e-001 +6.470e-001 +5.380e-001 +4.250e-001 +3.080e-001 +2.150e-001
+1.390e-001 +5.100e-002 -4.200e-002 -1.120e-001 -1.670e-001 -2.310e-001 -2.940e-001 -3.310e-001 -3.470e-001 -3.450e-001 -3.180e-001 -2.730e-001 -2.220e-001 -1.560e-001 -9.900e-002 -9.100e-002 -1.270e-001 -2.200e-001
 -3.400e-001 -4.090e-001 -4.390e-001 -4.520e-001 -4.510e-001 -4.430e-001
-4.330e-001
  14.5098
191.3100
                                2.13
                              54.67
     26.9229
                            108.70
       3.2568 10000000000.00
<Date: Thu Sep 18 13:36:02 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: SW TO G-50
                                                                                                                           6 Ampl=OFF
<Place: PANORMOS
#GEOSEC: 0305-A / 50.0/ 50.0/ 186.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      1.0/ 560303.000/ 3917103.000/
                                                                                                                                          0.000/rms=186.00
                                                                                                        0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +3.779e+001 +6.860e+001 +1.023e+002 +1.327e+002 +1.506e+002 +1.621e+002 +1.722e+002 +1.784e+002 +1.794e+002 +1.785e+002 +1.768e+002 +1.755e+002 +1.752e+002 +1.751e+002 +1.747e+002 +1.728e+002 +1.650e+002 +1.650e+002 +1.7570e+002 +1.602e+002 +1.602e+
+1.178e+002 +1.022e+002 +8.530e+001 +7.319e+001 +6.408e+001 +5.451e+001
+4.543e+001 +3.924e+001 +3.474e+001 +3.003e+001 +2.542e+001 +2.208e+001
+1.945e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.770e-001 +7.050e-001 +5.110e-001 +3.800e-001 +2.410e-001 +9.100e-002 -4.000e-003
-4.300e-002 -4.500e-002 -2.200e-002 -6.000e-003 -8.000e-003 -3.200e-002 -8.500e-002 -1.470e-001 -2.150e-001 -3.080e-001 -4.020e-001 -4.510e-001 -4.730e-001 -4.850e-001 -4.900e-001 -4.910e-001 -4.910e-001 -4.900e-001 -4.890e-001 -4.860e-001 -4.840e-001 -4.830e-001 -4.840e-001 -4.870e-001
 -4.900e-001
    29.6411
                              3.39
50.13
   500.0001
     59.3348
                              65.80
       2.7847 10000000000.00
 <Date: Thu Sep 18 14:16:48 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                           6 Ampl=OFF
<Remark: NORTH TO G-17</pre>
*****
#GEOSEC: 0306-A / 50.0 / 50.0 1. 86.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      1.0/
                                                                                                   560518.000/ 3917272.000/
                                                                                                       0.000 DH =
                                                                                                                                          0.000/rms = 86.00
                       +0.000e+000 +0.000e+000 +2.649e+001 +4.583e+001 +6.255e+001
+7.557e+001 +8.376e+001 +9.005e+001 +9.751e+001 +1.060e+002 +1.129e+002
+1.185e+002 +1.251e+002 +1.321e+002 +1.368e+002 +1.397e+002 +1.411e+002
                                                                            Σελίδα 119
```

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1D_Inversion_Results_TEM.txt
+1.388e+002 +1.336e+002 +1.270e+002 +1.167e+002 +1.033e+002 +9.178e+001 +8.233e+001 +7.158e+001 +6.054e+001 +5.272e+001 +4.680e+001 +4.051e+001
+3.445e+001 +3.030e+001 +2.729e+001 +2.419e+001 +2.124e+001 +1.916e+001
+1.753e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.170e-001 +5.870e-001 +4.630e-001 +4.160e-001 +3.840e-001 +3.530e-001 +3.260e-001
+3.020e-001 +2.720e-001 +2.250e-001 +1.690e-001 +1.010e-001 -8.000e-003
-1.540e-001 -2.690e-001 -3.470e-001 -4.110e-001 -4.520e-001 -4.680e-001 -4.70e-001 -4.830e-001 -4.830e-001 -4.830e-001 -4.830e-001 -4.830e-001
-4.770e-001 -4.710e-001 -4.650e-001 -4.550e-001 -4.440e-001 -4.410e-001
-4.420e-001
   12.6463
  180.1776
                     69.78
                     30.85
   29.3674
     3.9886 10000000000.00
<Date: Thu Sep 18 14:38:00 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
<Remark: NORTH TO G-17</pre>
*****
#GEOSEC: 0307-A / 50.0/ 50.0/ 1. 70.0/33/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                             1.0/ 560553.000/ 3916602.000/
                                                                         0.000 DH=
                                                                                                 0.000/rms=634.00
S [V/A]: +0.000e+000 +1.910e+001 +4.053e+001 +5.184e+001 +5.893e+001 +6.158e+001 +6.186e+001 +6.163e+001 +6.121e+001 +6.065e+001 +6.018e+001
+5.985e+001 +5.961e+001 +5.967e+001 +6.002e+001 +6.055e+001 +6.142e+001
+6.271e+001 +6.399e+001 +6.526e+001 +6.715e+001 +6.997e+001 +7.308e+001
+7.649e+001 +8.193e+001 +9.058e+001 +1.001e+002 +1.105e+002 +1.266e+002 +1.506e+002 +1.752e+002 +1.999e+002 +2.346e+002 
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -7.760e-001 +3.970e-001
+9.800e-002 -2.000e-003 -2.900e-002 -3.900e-002 -4.300e-002 -4.000e-002 -3.000e-002 -9.000e-003 +2.100e-002 +4.800e-002 +6.800e-002 +8.900e-002 +1.100e-001 +1.270e-001 +1.460e-001 +1.770e-001 +2.270e-001 +2.810e-001 +3.350e-001 +4.100e-001 +4.990e-001 +5.690e-001 +6.200e-001 +6.690e-001
+7.040e-001 +7.180e-001 +7.200e-001 +7.190e-001
   34.1942
                      0.96
                     70.63
   63.6837
1000.0001 10000000000.00
<Date: Fri Sep 19 08:27:53 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
<Remark: ĔAST TO G-17
<Place: AGGELIANA
******
#GEOSEC: 0308 / 50.0/ 50.0/ 1.0/ 560931.000/ 3916889.000/ 75.0/32/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                                 0.000/\text{rms}=472.00
75.0/32/4/0/2222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/rf S [V/A]: +0.000e+000 +0.000e+000 +1.288e+001 +3.034e+001 +4.819e+001 +6.714e+001 +8.288e+001 +9.657e+001 +1.134e+002 +1.315e+002 +1.441e+002 +1.523e+002 +1.591e+002 +1.633e+002 +1.647e+002 +1.649e+002 +1.637e+002 +1.606e+002 +1.567e+002 +1.527e+002 +1.473e+002 +1.406e+002 +1.349e+002 +1.300e+002 +1.238e+002 +1.168e+002 +1.112e+002 +1.065e+002 +1.008e+002 +9.383e+001 +8.737e+001 +8.133e+001
               +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.940e-001
Err[V/A]:
+8.350e-001 +7.720e-001 +7.210e-001 +6.490e-001 +5.340e-001 +4.100e-001 +2.990e-001 +1.830e-001 +8.500e-002 +2.600e-002 -1.500e-002 -6.400e-002 -1.190e-001 -1.570e-001 -1.820e-001 -2.040e-001 -2.230e-001 -2.370e-001 -2.480e-001 -2.580e-001 -2.660e-001 -2.770e-001 -2.980e-001
-3.380e-001 -3.790e-001 -4.110e-001
   36.5338
                       6.59
  500.0001
                     64.48
   73.4195
                    105.59
   33.5466 10000000000.00
<Date: Fri Sep 19 08:58:04 2008</pre>
<Time Range=5 Currrent= 2.10 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
<Remark: SOUTH TO MARGARITIANOS</pre>
<Place: AGGELIANA
*****
```

```
1D_Inversion_Results_TEM.txt
#GEOSEC: 0309-A / 50.0/ 50.0/ 1.0/ 561066.000/ 3916973.000/ 49.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                                 0.000/\text{rms} = 684.00
S [V/A]: +1.720e-001 +5.649e+001 +1.047e+002 +1.503e+002 +2.073e+002 +2.601e+002 +2.868e+002 +2.994e+002 +3.059e+002 +3.047e+002 +2.993e+002
+2.934e+002 +2.866e+002 +2.803e+002 +2.763e+002 +2.731e+002 +2.686e+002 +2.616e+002 +2.542e+002 +2.471e+002 +2.375e+002 +2.256e+002 +2.148e+002 +2.045e+002 +1.900e+002 +1.706e+002 +1.535e+002 +1.389e+002 +1.220e+002 +1.051e+002 +9.329e+001 +8.464e+001 +7.547e+001 +6.611e+001 +5.878e+001
+5.254e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.930e-001 +8.400e-001 +6.230e-001 +3.680e-001 +1.980e-001 +5.200e-002 -6.400e-002 -1.160e-001
-1.280e-001 -1.160e-001 -9.200e-002 -8.000e-002 -8.500e-002 -1.080e-001 -1.460e-001 -1.770e-001 -1.990e-001 -2.230e-001 -2.530e-001 -2.870e-001
-3.270e-001 -3.800e-001 -4.300e-001 -4.550e-001 -4.660e-001 -4.700e-001 -4.670e-001 -4.610e-001 -4.550e-001 -4.510e-001 -4.580e-001 -4.710e-001
-4.820e-001
 278.7476
                     98.22
   91.9230
                     71.82
   25.6268
                     32.29
9.1381 10000000000.00
<Date: Fri Sep 19 09:27:10 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                       6 Ampl=OFF
<Remark: POWER-LINES</pre>
<Place: AGGELIANA
*****
0.000/rms=381.00
+3.816e+001 +4.158e+001 +4.342e+001 +4.460e+001 +4.498e+001 +4.488e+001
+4.468e+001 +4.442e+001 +4.412e+001 +4.378e+001 +4.335e+001 +4.256e+001
+4.133e+001 +4.010e+001 +3.898e+001 +3.757e+001 +3.592e+001 +3.449e+001 +3.315e+001 +3.127e+001 +2.866e+001 +2.617e+001 +2.386e+001 +2.098e+001 +1.782e+001 +1.549e+001 +1.375e+001 +1.196e+001 +1.031e+001 +9.259e+000
+8.552e+000
                -9.000e-001 -9.000e-001 -9.000e-001 -8.930e-001 +7.780e-001
Err[V/A]:
+5.360e-001 +3.430e-001 +2.110e-001 +9.300e-002 +1.100e-002 -2.200e-002 -3.100e-002 -3.200e-002 -3.900e-002 -5.700e-002 -8.300e-002 -1.190e-001 -1.570e-001 -1.800e-001 -1.920e-001 -2.030e-001 -2.180e-001 -2.410e-001
-4.020e-001
   19.4935
                       1.38
   46.6329
                     38.59
   12.2629
                     38.29
     1.3076 10000000000.00
<Date: Fri Sep 19 10:40:30 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                      6 Ampl=OFF
<Remark: POWER-LINES IN LOOP, FENCES</pre>
<Place: PANORMOS
*****
                                 / 50.0/ 50.0/ 1.0/ 561565.000/ 3919088.000/
35.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                       0.000 DH=
                                                                                                 0.000/rms=232.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +1.004e+001 +1.606e+001 +1.886e+001 +2.085e+001 +2.330e+001 +2.643e+001 +2.935e+001
+3.206e+001 +3.557e+001 +3.954e+001 +4.244e+001 +4.430e+001 +4.554e+001
+4.549e+001 +4.445e+001 +4.310e+001 +4.118e+001 +3.885e+001 +3.690e+001 +3.519e+001 +3.299e+001 +3.015e+001 +2.760e+001 +2.529e+001 +2.247e+001 +1.942e+001 +1.720e+001 +1.556e+001 +1.386e+001 +1.225e+001 +1.112e+001
+1.024e+001
Err[V/A]: -1.000e-015 -1.000e-015 -1.000e-015 -9.000e-001 +9.000e-001 +8.570e-001 +6.280e-001 +5.480e-001 +5.280e-001 +5.290e-001 +5.310e-001 +5.230e-001 +4.940e-001 +4.250e-001 +3.320e-001 +2.260e-001 +8.000e-002 -7.600e-002 -1.710e-001 -2.190e-001 -2.510e-001 -2.710e-001 -2.860e-001 -3.070e-001 -3.430e-001 -3.910e-001 -4.670e-001 -4.670e-001 -4.670e-001
-4.670e-001 -4.650e-001 -4.590e-001 -4.470e-001 -4.320e-001 -4.270e-001
-4.260e-001
```

```
1D_Inversion_Results_TEM.txt
 17.9103
100.0000
                  8.27
23.05
 107.9211
                  18.85
    8.9092
                  36.66
    2.0554 10000000000.00
<Date: Fri Sep 19 11:26:20 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                           6 Ampl=OFF
<Remark: POWER-LINES, FENCES, NAT.ROAD</pre>
<Place: PANORMOS
#GEOSEC: 0312-A / 50.0/ 50.0/ 1
39.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 561007.000/ 3919229.000/
                                                               0.000 DH =
                                                                                    0.000/rms=640.00
S [V/A]: +0.000e+000 +4.186e+000 +1.377e+001 +2.158e+001 +2.991e+001 +3.821e+001 +4.428e+001 +4.881e+001 +5.344e+001 +5.747e+001 +6.021e+001 +6.251e+001 +6.572e+001 +7.001e+001 +7.348e+001 +7.538e+001 +7.522e+001
+7.122e+001 +6.590e+001 +6.103e+001 +5.550e+001 +5.022e+001 +4.666e+001 +4.397e+001 +4.076e+001 +3.665e+001 +3.283e+001 +2.930e+001 +2.498e+001
+2.047e+001 +1.733e+001 +1.510e+001 +1.293e+001 +1.107e+001 +9.962e+000
+9.285e+000
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.980e-001 +8.490e-001 +7.200e-001 +6.030e-001 +5.050e-001 +3.910e-001 +2.870e-001 +2.500e-001
+2.550e-001 +2.800e-001 +2.820e-001 +2.180e-001 +9.000e-002 -1.270e-001
-3.230e-001 -3.950e-001 -4.110e-001 -4.030e-001 -3.770e-001 -3.560e-001 -3.550e-001 -3.820e-001 -4.350e-001 -4.690e-001 -4.850e-001 -4.920e-001
-4.950e-001 -4.940e-001 -4.910e-001 -4.830e-001 -4.610e-001 -4.190e-001
-3.590e-001
  27.2612
99.2604
                    5.85
                  35.80
   38.1822
                  21.04
    4.6540
                  24.70
    1.0000 10000000000.00
<Date: Fri Sep 19 11:57:29 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                           6 Ampl=OFF
<Remark: NATIONAL ROAD</pre>
<Place: PANORMOS
#GEOSEC: 0313-B
                             / 50.0/ 50.0/
                                                    1.0/ 563183.000/ 3918618.000/
37.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                    0.000/\text{rms}=156.00
S [V/A]: +0.000e+000 +3.545e+000 +2.689e+001 +4.070e+001 +5.118e+001 +5.772e+001 +6.065e+001 +6.219e+001 +6.344e+001 +6.445e+001 +6.525e+001 +6.604e+001 +6.727e+001 +6.893e+001 +7.028e+001 +7.111e+001 +7.149e+001 +6.604e+001 +6.727e+001 +6.893e+001 +7.028e+001 +7.028e+001 +7.79e+001
+7.074e+001 +6.920e+001 +6.735e+001 +6.460e+001 +6.099e+001 +5.779e+001
+5.494e+001 +5.136e+001 +4.712e+001 +4.365e+001 +4.069e+001 +3.717e+001
+3.334e+001 +3.039e+001 +2.807e+001 +2.547e+001 +2.281e+001 +2.083e+001
+1.928e+001
              -9.000e-001 -9.000e-001 -9.000e-001 -8.920e-001 +6.830e-001
Err[V/A]:
+3.630e-001 +2.040e-001 +1.340e-001 +9.000e-002 +7.100e-002 +7.500e-002
+8.900e-002 +1.080e-001 +1.130e-001 +9.400e-002 +5.700e-002 -8.000e-003 -9.300e-002 -1.560e-001 -1.990e-001 -2.400e-001 -2.750e-001 -3.000e-001 -3.200e-001 -3.430e-001 -3.670e-001 -3.840e-001 -3.960e-001 -4.070e-001
-4.150e-001 -4.190e-001 -4.190e-001 -4.170e-001 -4.140e-001 -4.130e-001
-4.140e-001
  47.2826
72.1353
                  65.17
   15.4362
                  45.68
    5.6257 10000000000.00
<Date: Fri Sep 19 12:35:56 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                           6 Ampl=OFF
<Remark: SOUTH TO NATIONAL ROAD</pre>
<Place: ROUMELI
<***************
#GEOSEC: 0314-A / 50.0/ 50.0/ 1.
30.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 563442.000/ 3918718.000/
                                                               0.000 DH =
                                                                                    0.000/rms=107.00
S [V/A]: +0.000e+000 +0.000e+000 +4.996e+000 +1.650e+001 +2.324e+001
+2.582e+001 +2.646e+001 +2.668e+001 +2.683e+001 +2.689e+001 +2.691e+001
                                              Σελίδα 122
```

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1D_Inversion_Results_TEM.txt
+2.697e+001 +2.711e+001 +2.745e+001 +2.790e+001 +2.839e+001 +2.915e+001 +3.019e+001 +3.116e+001 +3.202e+001 +3.315e+001 +3.456e+001 +3.589e+001 +3.718e+001 +3.892e+001 +4.100e+001 +4.250e+001 +4.343e+001 +4.393e+001
+4.358e+001 +4.269e+001 +4.162e+001 +3.999e+001 +3.752e+001 +3.474e+001
+3.170e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +7.910e-001 +2.700e-001 +8.800e-002 +4.200e-002 +2.000e-002 +7.000e-003 +1.000e-002 +2.200e-002 +4.300e-002 +7.700e-002 +1.070e-001 +1.310e-001 +1.570e-001
+1.760e-001 +1.840e-001 +1.890e-001 +1.960e-001 +2.110e-001 +2.300e-001
+2.450e-001 +2.510e-001 +2.280e-001 +1.780e-001 +1.110e-001 +1.600e-002 -8.400e-002 -1.480e-001 -1.910e-001 -2.490e-001 -3.380e-001 -4.190e-001
-4.670e-001
  11.9971
                   0.61
   29.4570
                  33.69
   57.9055
                 126.95
    9.0518 10000000000.00
<Date: Fri Sep 19 12:59:03 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: SOUTH TO NATIONAL ROAD</pre>
<Place: ROUMELI
<***************
*****
#GEOSEC: 0315-B / 50.0/ 50.0/ 1.
33.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 563688.000/ 3918750.000/
                                                              0.000 DH=
                                                                                    0.000/\text{rms}=147.00
    [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +1.368e+000
+1.040e+001 +1.575e+001 +1.940e+001 +2.328e+001 +2.732e+001 +3.043e+001
+3.298e+001 +3.590e+001 +3.889e+001 +4.099e+001 +4.242e+001 +4.372e+001
+4.472e+001 +4.526e+001 +4.560e+001 +4.587e+001 +4.592e+001 +4.555e+001 +4.482e+001 +4.332e+001 +4.083e+001 +3.842e+001 +3.628e+001 +3.379e+001
+3.130e+001 +2.961e+001 +2.840e+001 +2.712e+001 +2.569e+001 +2.427e+001
+2.272e+001
Err[V/A]: -1.000e-015 -1.000e-015 -1.000e-015 -9.000e-001 +9.000e-001 +9.000e-001 +9.000e-001 +5.150e-001 +6.950e-001 +5.850e-001 +5.150e-001 +4.050e-001 +4.030e-001 +3.270e-001 +2.590e-001 +2.020e-001 +1.400e-001
+8.800e-002 +5.900e-002 +4.300e-002 +2.000e-002 -2.400e-002 -8.100e-002 -1.440e-001 -2.240e-001 -2.960e-001 -3.310e-001 -3.430e-001 -3.370e-001
-3.110e-001 -2.810e-001 -2.570e-001 -2.460e-001 -2.780e-001 -3.440e-001
-4.040e-001
    4.7214
                  27.27
 119.7299
   39.2906
                  63.07
12.0282 10000000000.00
<Date: Fri Sep 19 14:07:12 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: FENCES, POWERLINES</pre>
<place: ROUMELI</pre>
*****
#GEOSEC: 0316-A / 50.0 / 50.0 / 1.44.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 563889.000/ 3918795.000/
                                                              0.000 DH=
                                                                                    0.000/rms=218.00
   [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.264e+000 +1.429e+001
+2.400e+001 +2.947e+001 +3.315e+001 +3.679e+001 +4.004e+001 +4.214e+001
+4.368e+001 +4.549e+001 +4.781e+001 +5.016e+001 +5.247e+001 +5.571e+001
+5.972e+001 +6.290e+001 +6.516e+001 +6.703e+001 +6.771e+001 +6.721e+001 +6.619e+001 +6.442e+001 +6.181e+001 +5.935e+001 +5.709e+001 +5.425e+001
+5.106e+001 +4.858e+001 +4.658e+001 +4.419e+001 +4.122e+001 +3.832e+001
+3.537e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 +9.000e-001 +8.810e-001 +7.170e-001 +5.780e-001 +4.440e-001 +3.230e-001 +2.560e-001
+2.270e-001 +2.250e-001 +2.530e-001 +2.850e-001 +3.090e-001 +3.230e-001
+3.080e-001 +2.650e-001 +2.020e-001 +1.070e-001 -1.000e-003 -7.700e-002
-1.250e-001 -1.700e-001 -2.130e-001 -2.400e-001 -2.580e-001 -2.690e-001
-2.710e-001 -2.690e-001 -2.710e-001 -2.890e-001 -3.380e-001 -3.970e-001
-4.410e-001
    8.3327
                    1.67
                  52.15
   75.7730
  97.6866
                  54.41
  16.4812
                 107.67
```

```
1D_Inversion_Results_TEM.txt
4.1657 10000000000.00

<Date: Fri Sep 19 14:29:00 2008

<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                              6 Ampl=OFF
<Remark: SOUTH TO NATIONAL ROAD</pre>
<Place: ROUMELI
******
#GEOSEC: 0317-A / 50.0/ 50.0/ 1.0
61.0/36/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 564065.000/ 3917742.000/
                                                               0.000 DH =
                                                                                       0.000/\text{rms}=924.00
S [V/A]: +1.326e+001 +1.022e+001 +1.023e+001 +1.100e+001 +1.209e+001 +1.296e+001 +1.306e+001 +1.275e+001 +1.198e+001 +1.084e+001 +9.894e+000
+9.186e+000 +8.490e+000 +7.928e+000 +7.641e+000 +7.514e+000 +7.483e+000
+7.620e+000 +7.876e+000 +8.204e+000 +8.777e+000 +9.727e+000 +1.083e+001
+1.207e+001 +1.405e+001 +1.708e+001 +2.009e+001 +2.278e+001 +2.555e+001
+2.715e+001 +2.705e+001 +2.619e+001 +2.445e+001 +2.178e+001 +1.927e+001
+1.710e+001
Err[V/A]: +5.000e-001 +3.570e-001 -2.260e-001 -4.120e-001 +3.680e-001 +1.560e-001 -6.500e-002 -2.210e-001 -3.380e-001 -3.930e-001 -3.990e-001 -3.800e-001 -3.330e-001 -2.470e-001 -1.550e-001 -7.300e-002 +2.900e-002 +1.450e-001 +2.360e-001 +3.140e-001 +4.110e-001 +5.200e-001 +6.020e-001 +6.620e-001 +7.160e-001 +7.420e-001 +7.220e-001 +6.480e-001 +4.520e-001 +1.230e-001 -1.290e-001 -2.740e-001 -3.840e-001 -4.520e-001 -4.780e-001
-4.880e-001
    8.9412
                    8.12
                   19.21
    9.8586
                   97.51
 200.0000
    1.0000 10000000000.00
<Date: Fri Sep 19 15:03:44 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
<Remark: SOUTH TO NATIONAL ROAD</pre>
<Place: ROUMELI
******
#GEOSEC: 0318-A / 50.0/ 50.0/ 1.0
47.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 564412.000/ 3917700.000/
                                                                0.000 DH=
                                                                                       0.000/\text{rms}=116.00
S [V/A]: +0.000e+000 +0.000e+000 +5.520e-001 +9.128e+000 +1.517e+001
+1.869e+001 +2.067e+001 +2.220e+001 +2.403e+001 +2.611e+001 +2.785e+001 +2.931e+001 +3.101e+001 +3.280e+001 +3.410e+001 +3.507e+001 +3.611e+001
+3.712e+001 +3.784e+001 +3.839e+001 +3.897e+001 +3.945e+001 +3.964e+001
+3.958e+001 +3.921e+001 +3.828e+001 +3.707e+001 +3.566e+001 +3.346e+001
+3.032e+001 +2.739e+001 +2.481e+001 +2.171e+001 +1.836e+001 +1.585e+001
+1.389e+001
Err[V/A]:
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.890e-001
+6.070e-001 +4.560e-001 +4.120e-001 +3.830e-001 +3.570e-001 +3.360e-001
+3.140e-001 +2.820e-001 +2.400e-001 +2.040e-001 +1.760e-001 +1.470e-001 +1.210e-001 +1.050e-001 +9.200e-002 +7.300e-002 +4.200e-002 +8.000e-003 -2.900e-002 -8.200e-002 -1.540e-001 -2.200e-001 -2.820e-001 -3.540e-001 -4.180e-001 -4.510e-001 -4.670e-001 -4.790e-001 -4.860e-001 -4.900e-001
-4.920e-001
  18.9891
48.1872
                   6.83
47.44
   27.2906
                   16.80
   12.0019
                   42.06
    1.2373 10000000000.00
<Date: Fri Sep 19 15:26:47 2008
<Time Range=6 Currrent= 1.90 Stack= 5 Filter=50 Deff=</pre>
                                                                              6 Ampl=OFF
<Remark: SOUTH TO NATIONAL ROAD</pre>
<Place: ROUMELI
******
#GEOSEC: 0319-A / 50.0/ 50.0/ 1.0
46.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 564859.000/ 3917633.000/
                                                               0.000 DH =
```

0.000/rms = 93.005 [V/A]: +0.000e+000 +0.000e+000 +6.800e-002 +4.252e+000 +6.827e+000 +7.696e+000 +7.719e+000 +7.526e+000 +7.207e+000 +6.873e+000 +6.667e+000 +6.568e+000 +6.537e+000 +6.585e+000 +6.678e+000 +6.800e+000 +6.980e+000 +7.248e+000 +7.517e+000 +7.792e+000 +8.195e+000 +8.769e+000 +9.357e+000 +9.956e+000 +1.083e+001 +1.208e+001 +1.329e+001 +1.447e+001 +1.604e+001 +1.791e+001 +1.936e+001 +2.040e+001 +2.130e+001 +2.184e+001 +2.197e+001

```
1D_Inversion_Results_TEM.txt
+2.198e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.670e-001 +2.370e-001 -8.000e-002 -1.840e-001 -2.130e-001 -1.860e-001 -1.300e-001
-6.600e-002 +3.000e-003 +6.000e-002 +1.040e-001 +1.320e-001 +1.610e-001
+1.970e-001 +2.280e-001 +2.570e-001 +2.960e-001 +3.450e-001 +3.870e-001 +4.230e-001 +4.640e-001 +5.030e-001 +5.240e-001 +5.280e-001 +5.130e-001 +4.610e-001 +3.870e-001 +1.870e-001 +7.400e-002 +1.700e-002
-1.300e-002
    7.3543
                    6.98
   7.5207
23.1418
                   14.60
                   13.15
 200.0000
                 102.10
    8.4715 10000000000.00
<Date: Fri Sep 19 15:49:25 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: SOUTH TO NATIONAL ROAD
                                                                            6 Ampl=OFF
<Place: ROUMELI</pre>
*****
#GEOSEC: 0329-A / 50.0/ 50.0/ 1.53.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                     1.0/ 565210.000/ 3918636.000/
                                                                0.000 DH =
                                                                                      0.000/rms=187.00
              +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +6.471e+000
+1.137e+001 +1.357e+001 +1.523e+001 +1.743e+001 +2.034e+001 +2.314e+001
+2.582e+001 +2.946e+001 +3.402e+001 +3.797e+001 +4.132e+001 +4.537e+001 +4.997e+001 +5.377e+001 +5.696e+001 +6.067e+001 +6.428e+001 +6.639e+001
+6.737e+001 +6.746e+001 +6.616e+001 +6.423e+001 +6.211e+001 +5.904e+001
+5.490e+001 +5.087e+001 +4.691e+001
+6.210e-001 +6.100e-001 +5.780e-001 +5.400e-001 +5.030e-001 +4.600e-001
+4.200e-001 +3.900e-001 +3.610e-001 +3.110e-001 +2.280e-001 +1.410e-001 +5.900e-002 -4.000e-002 -1.370e-001 -1.980e-001 -2.410e-001 -2.890e-001 -3.490e-001 -4.020e-001 -4.410e-001
   15.8972
                    9.18
 200,0000
                   18.96
 200.0000
                   46.28
   38.8033
                   76.92
9.1050 10000000000.00
<Date: Fri Oct 10 13:08:59 2008
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                            6 Ampl=OFF
<Remark: NEAR NATIONAL ROAD</pre>
******
#GEOSEC: 0330-B / 50.0/ 50.0/ 1.
39.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                   1.0/ 564905.000/ 3918653.000/
                                                                0.000 DH=
                                                                                      0.000/\text{rms}=216.00
S [V/A]: +0.000e+000 +0.000e+000 +6.610e-001 +1.424e+001 +2.658e+001 +3.606e+001 +4.197e+001 +4.631e+001 +5.103e+001 +5.569e+001 +5.878e+001
+6.077e+001 +6.242e+001 +6.343e+001 +6.372e+001 +6.368e+001 +6.337e+001 +6.268e+001 +6.186e+001 +6.096e+001 +5.964e+001 +5.791e+001 +5.640e+001 +5.512e+001 +5.358e+001 +5.173e+001 +5.005e+001 +4.841e+001 +4.618e+001
+4.347e+001 +4.134e+001 +3.979e+001
              +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.990e-001
Err[V/A]:
+7.720e-001 +6.120e-001 +5.200e-001 +4.320e-001 +3.360e-001 +2.530e-001 +1.860e-001 +1.130e-001 +4.900e-002 +1.000e-002 -1.500e-002 -3.900e-002 -6.600e-002 -8.900e-002 -1.090e-001 -1.300e-001 -1.470e-001 -1.530e-001
-1.550e-001 -1.610e-001 -1.790e-001 -2.050e-001 -2.320e-001 -2.600e-001
-2.720e-001 -2.590e-001 -2.360e-001
                  6.11
17.60
   23.4822
 200.0000
   73.2239
                   23.00
   38.2835
                   65.63
   22.1913 10000000000.00
<Date: Fri Oct 10 13:28:35 2008
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=</pre>
                                                                            6 Ampl=OFF
<Remark: NEAR NATIONAL ROAD</pre>
<Place: SKEPASTI
```

## 1D\_Inversion\_Results\_TEM.txt

```
******
                                    50.0/ 50.0/
                                                         1.0/
                                                                  563412.000/ 3917599.000/
#GEOSEC: 0326-A
84.0/32/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                     0.000 DH =
0.000/\text{rms}=1121.00
S [V/A]: +3.110e-001 +4.878e+001 +8.809e+001 +1.240e+002 +1.697e+002 +2.149e+002 +2.366e+002 +2.423e+002 +2.391e+002 +2.294e+002 +2.201e+002 +2.114e+002 +1.991e+002 +1.819e+002 +1.656e+002 +1.517e+002 +1.354e+002 +1.192e+002 +1.082e+002 +1.003e+002 +9.224e+001 +8.428e+001 +7.813e+001
+7.288e+001 +6.636e+001 +5.886e+001 +5.316e+001 +4.875e+001 +4.410e+001
+3.974e+001 +3.677e+001 +3.448e+001

Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.900e-001 +8.400e-001

+6.310e-001 +3.060e-001 +5.100e-002 -1.250e-001 -2.040e-001 -2.360e-001

-2.710e-001 -3.290e-001 -3.930e-001 -4.270e-001 -4.410e-001 -4.440e-001
-4.340e-001 -4.160e-001 -3.960e-001 -3.760e-001 -3.690e-001 -3.800e-001 -3.980e-001 -4.200e-001 -4.350e-001 -4.380e-001 -4.320e-001 -4.150e-001 -3.890e-001 -3.730e-001 -3.660e-001
 200.0000
                     1.05
 200.0000
                    21.22
                    44.67
 200.0000
   19.0843
                    58.68
    7.8809 10000000000.00
<Date: Fri Oct 10 11:36:15 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark: FENCES, POWER-LINES
<Place: ROUMELI</pre>
#GEOSEC: 0327-B / 50.0 / 50.0 / 1.82.0 / 32/5 / 0/22222 SPM=0 K= 0.000e+000 H=
                                                         1.0/ 563247.000/ 3917493.000/
                                                                   0.000 \, \text{DH} =
                                                                                            0.000/\text{rms}=222.00
    [V/A]:
              +0.000e+000 +4.395e+000 +2.809e+001 +4.368e+001 +5.831e+001
+7.220e+001 +8.319e+001 +9.309e+001 +1.064e+002 +1.233e+002 +1.377e+002
+1.491e+002 +1.606e+002 +1.692e+002 +1.724e+002 +1.728e+002 +1.712e+002 +1.670e+002 +1.620e+002 +1.563e+002 +1.477e+002 +1.356e+002 +1.245e+002 +1.148e+002 +1.034e+002 +9.121e+001 +8.236e+001 +7.548e+001 +6.786e+001
+5.986e+001 +5.361e+001 +4.842e+001
               -9.000e-001 -9.000e-001 -9.000e-001 -8.970e-001 +8.150e-001
Err[V/A]:
+6.810e-001 +6.260e-001 +6.120e-001 +6.020e-001 +5.730e-001 +5.180e-001 +4.430e-001 +3.220e-001 +1.700e-001 +5.800e-002 -1.500e-002 -8.300e-002
-1.490e-001 -2.050e-001 -2.570e-001 -3.210e-001 -3.800e-001 -4.120e-001
-4.280e-001 -4.370e-001 -4.390e-001 -4.380e-001 -4.370e-001 -4.390e-001 -4.480e-001 -4.590e-001 -4.690e-001
 5.0037
111.7470
                     0.53
                     5.10
 300.0000
                    79.69
                    51.31
   38.6949
   10.6027 10000000000.00
<Date: Fri Oct 10 12:01:36 2008</p>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                  6 Ampl=OFF
<Remark: FENCES, POWER-LINES</pre>
*****
#GEOSEC: 0325-A / 50.0/ 50.0/ 1.0/ 562913.000/ 3917726.000/ 82.0/32/5/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/
                                                                                            0.000/rms=577.00
S [V/A]: +0.000e+000 +0.000e+000 +6.890e-001 +1.163e+001 +2.449e+001 +3.767e+001 +4.846e+001 +5.811e+001 +7.084e+001 +8.688e+001 +1.005e+002
+1.112e+002 +1.212e+002 +1.263e+002 +1.250e+002 +1.206e+002 +1.129e+002
+1.030e+002 +9.512e+001 +8.894e+001 +8.201e+001 +7.447e+001 +6.824e+001
+6.283e+001 +5.619e+001 +4.892e+001 +4.368e+001 +3.983e+001 +3.601e+001 +3.277e+001 +3.093e+001 +2.987e+001
              +5.000e-001 -9.000e-001 -9.000e-001 +9.000e-001
+8.790e-001 +8.290e-001 +7.930e-001 +7.570e-001 +7.040e-001 +6.300e-001
+5.250e-001 +3.320e-001 +5.700e-002 -1.560e-001 -2.740e-001 -3.460e-001 -3.760e-001 -3.790e-001 -3.770e-001 -3.790e-001 -3.950e-001 -4.170e-001 -4.360e-001 -4.580e-001 -4.530e-001 -4.390e-001 -4.060e-001
-3.410e-001 -2.660e-001 -1.900e-001
    5.0388
                     0.86
   71.9999
                      1.91
```

```
1D_Inversion_Results_TEM.txt
                  62.52
35.28
 300.0000
   15.9957
    8.6874 10000000000.00
<Date: Fri Oct 10 11:11:27 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                           6 Ampl=OFF
<Remark: FENCES, POWER-LINES</pre>
<Place: ROUMELI
*****
#GEOSEC: 0324-B / 50.0/ 50.0/ 1.
23.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 562801.000/ 3917433.000/
                                                              0.000 DH =
                                                                                    0.000/\text{rms}=320.00
             +0.000e+000 +0.000e+000 +1.794e+001 +3.302e+001 +3.937e+001
    [V/A]:
+3.749e+001 +3.394e+001 +3.109e+001 +2.830e+001 +2.589e+001 +2.436e+001
+2.330e+001 +2.225e+001 +2.129e+001 +2.064e+001 +2.018e+001 +1.969e+001
+1.917e+001 +1.874e+001 +1.832e+001 +1.774e+001 +1.694e+001 +1.618e+001 +1.548e+001 +1.457e+001 +1.345e+001 +1.252e+001 +1.175e+001 +1.084e+001
+9.904e+000 +9.207e+000 +8.635e+000
             +5.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +3.390e-001
Err[V/A]:
-3.350e-001 -4.160e-001 -4.100e-001 -3.760e-001 -3.270e-001 -2.870e-001 -2.560e-001 -2.210e-001 -1.860e-001 -1.600e-001 -1.420e-001 -1.300e-001 -1.420e-001 -1.620e-001 -1.940e-001 -2.340e-001 -2.660e-001 -2.920e-001 -3.210e-001 -3.480e-001 -3.640e-001 -3.720e-001 -3.720e-001
-3.660e-001 -3.660e-001 -3.720e-001
   33.3778
                   2.95
   38.3607
                   6.54
                  34.00
  13.2566
    5.0000 10000000000.00
<Date: Fri Oct 10 10:26:48 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                          6 Ampl=OFF
<Remark: NEAR STANI</pre>
<Place: ROUMELI
******
                               50.0/ 50.0/
                                                  1.0/ 563382.000/ 3916638.000/
#GEOSEC: 0320-B
0.0/36/4/0/22222 SPM=0 K= 0.000e+000 H= 0.000 DH= 0.000/ri
S [V/A]: +1.712e+001 +2.630e+001 +3.298e+001 +3.755e+001 +4.145e+001
+4.326e+001 +4.260e+001 +4.066e+001 +3.730e+001 +3.315e+001 +3.015e+001 +2.812e+001 +2.635e+001 +2.521e+001 +2.488e+001 +2.494e+001 +2.528e+001
+2.571e+001 +2.578e+001 +2.547e+001 +2.459e+001 +2.308e+001 +2.162e+001
+2.031e+001 +1.867e+001 +1.670e+001 +1.509e+001 +1.376e+001 +1.229e+001 +1.088e+001 +9.949e+000 +9.316e+000 +8.700e+000 +8.115e+000 +7.633e+000
+7.148e+000
Err[V/A]:
              -8.950e-001 -8.440e-001 -7.140e-001 -5.560e-001 +3.290e-001
+3.700e-002 -1.900e-001 -3.230e-001 -3.960e-001 -4.150e-001 -3.950e-001
-3.520e-001 -2.660e-001 -1.340e-001 -2.500e-002 +4.300e-002 +7.800e-002 +4.500e-002 -3.800e-002 -1.320e-001 -2.350e-001 -3.120e-001 -3.490e-001 -3.730e-001 -4.000e-001 -4.280e-001 -4.430e-001 -4.480e-001 -4.430e-001 -4.230e-001 -3.920e-001 -3.590e-001 -3.220e-001 -3.130e-001 -3.510e-001
-3.970e-001
   35.2381
                  19.27
7.34
    7.6176
                  23.63
   50.0000
    2.9452 10000000000.00
<Date: Fri Oct 10 08:33:10 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 6 Filter=50 Deff= <Remark: NEXT TO ROAD
                                                                          6 Ampl=OFF
<Place: SOLOCHIANA
*****
#GEOSEC: 0328-A / 50.0/ 50.0/ 1. 26.0/32/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                    1.0/ 562919.000/ 3916940.000/
                                                              0.000 DH=
                                                                                    0.000/rms=179.00
             +0.000e+000 +0.000e+000 +1.448e+001 +2.740e+001 +3.269e+001
+3.153e+001 +2.913e+001 +2.726e+001 +2.550e+001 +2.411e+001 +2.334e+001 +2.290e+001 +2.257e+001 +2.237e+001 +2.232e+001 +2.229e+001 +2.227e+001 +2.220e+001 +2.211e+001 +2.202e+001 +2.191e+001 +2.182e+001 +2.181e+001
+2.184e+001 +2.190e+001 +2.192e+001 +2.179e+001 +2.152e+001 +2.098e+001
+2.017e+001 +1.953e+001 +1.911e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +3.640e-001
                                              Σελίδα 127
```

```
1D_Inversion_Results_TEM.txt
-2.770e-001 -3.560e-001 -3.370e-001 -2.810e-001 -2.070e-001 -1.490e-001 -1.050e-001 -6.200e-002 -2.700e-002 -1.100e-002 -7.000e-003 -1.000e-002 -1.900e-002 -2.700e-002 -2.900e-002 -2.400e-002 -1.100e-002 +3.000e-003 +1.200e-002 +1.100e-002 -1.700e-002 -6.300e-002 -1.110e-001 -1.610e-001
-1.850e-001 -1.640e-001 -1.270e-001
 200.0000 33.9825
                    1.67
                    1.48
   20.0876
                   96.08
    7.6701 10000000000.00
<Date: Fri Oct 10 12:32:12 2008</pre>
<Time Range=5 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NEAR RIVER</pre>
<Place: ROUMELI
*****
#GEOSEC: 0321-B
                                50.0/ 50.0/
                                                    1.0/ 563217.000/ 3916479.000/
37.0/35/4/0/22222 SPM=0 K= 0.000e+000 H=
                                                               0.000 DH =
                                                                                      0.000/rms=458.00
S [V/A]: +0.000e+000 +4.169e+001 +7.657e+001 +1.036e+002 +1.305e+002
+1.497e+002 +1.562e+002 +1.568e+002 +1.527e+002 +1.432e+002 +1.331e+002 +1.240e+002 +1.133e+002 +1.024e+002 +9.455e+001 +8.881e+001 +8.272e+001 +7.680e+001 +7.262e+001 +6.949e+001 +6.612e+001 +6.281e+001 +6.046e+001
+5.868e+001 +5.671e+001 +5.454e+001 +5.269e+001 +5.094e+001 +4.850e+001
+4.528e+001 +4.241e+001 +3.995e+001 +3.713e+001 +3.435e+001 +3.258e+001
Err[V/A]: -9.000e-001 -9.000e-001 -8.990e-001 -8.660e-001 +7.030e-001 +3.740e-001 +1.150e-001 -5.200e-002 -2.030e-001 -3.170e-001 -3.680e-001
-3.880e-001 -3.930e-001 -3.830e-001 -3.670e-001 -3.510e-001 -3.300e-001
-3.060e-001 -2.850e-001 -2.690e-001 -2.480e-001 -2.240e-001 -2.050e-001 -1.920e-001 -1.840e-001 -1.910e-001 -2.110e-001 -2.380e-001 -2.790e-001 -3.210e-001 -3.450e-001 -3.520e-001 -3.440e-001 -3.070e-001 -2.610e-001
 134.3537
                   49.79
   11.2452
                    5.09
                   85.31
   36.3089
12.9827 10000000000.00
<Date: Fri Oct 10 09:03:53 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NEXT TO ROAD
<Place: SOLOCHIANA
*****
#GEOSEC: 0322-A / 50.0/ 50.0/ 1.
68.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                      1.0/ 563021.000/ 3916564.000/
                                                                                      0.000/rms=597.00
                                                                0.000 DH=
S [V/A]: +0.000e+000 +0.000e+000 +2.374e+001 +5.076e+001 +8.270e+001 +1.199e+002 +1.481e+002 +1.668e+002 +1.805e+002 +1.847e+002 +1.813e+002
+1.750e+002 +1.648e+002 +1.513e+002 +1.397e+002 +1.304e+002 +1.197e+002
+1.088e+002 +1.006e+002 +9.424e+001 +8.697e+001 +7.918e+001 +7.309e+001 +6.814e+001 +6.232e+001 +5.580e+001 +5.055e+001 +4.600e+001 +4.038e+001
+3.399e+001 +2.900e+001 +2.510e+001 +2.094e+001 +1.700e+001 +1.440e+001
+1.260e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 +8.970e-001 +8.500e-001 +7.260e-001 +5.400e-001 +2.660e-001 -1.000e-002 -1.690e-001 -2.560e-001 -3.220e-001 -3.640e-001 -3.800e-001 -3.840e-001 -3.830e-001 -3.750e-001 -3.750e-001 -3.750e-001 -3.750e-001 -3.750e-001 -3.750e-001 -3.750e-001 -3.750e-001
-3.940e-001 -4.060e-001 -4.250e-001 -4.440e-001 -4.610e-001 -4.780e-001
-4.900e-001 -4.940e-001 -4.960e-001 -4.960e-001 -4.950e-001 -4.930e-001
-4.900e-001
   50.2311
                    5.58
                   51.02
  300,0000
   20.6251
                   11.67
   11.9231
                   37.57
    1.0295 10000000000.00
<Date: Fri Oct 10 09:28:06 2008</pre>
<Time Range=6 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                             6 Ampl=OFF
<Remark: NEAR STANI</pre>
<Place: ROUMELI
*****
                              / 50.0/ 50.0/ 1.0/ 562863.000/ 3916526.000/
#GEOSEC: 0323-A
69.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                0.000 DH =
                                                                                     0.000/\text{rms}=321.00
```

```
1D_Inversion_Results_TEM.txt
S [V/A]: +0.000e+000 +2.862e+001 +7.319e+001 +1.134e+002 +1.642e+002 +2.130e+002 +2.374e+002 +2.471e+002 +2.491e+002 +2.426e+002 +2.326e+002 +2.221e+002 +2.079e+002 +1.905e+002 +1.754e+002 +1.625e+002 +1.473e+002 +1.312e+002 +1.194e+002 +1.105e+002 +1.010e+002 +9.183e+001 +8.539e+001
+8.060e+001 +7.549e+001 +7.031e+001 +6.641e+001 +6.308e+001 +5.884e+001
+5.363e+001 +4.919e+001 +4.549e+001 +4.133e+001 +3.724e+001 +3.451e+001
+3.262e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.990e-001 +8.700e-001 +6.780e-001 +3.820e-001 +1.570e-001 -3.500e-002 -1.790e-001 -2.550e-001 -2.970e-001 -3.360e-001 -3.720e-001 -3.960e-001 -4.110e-001 -4.200e-001 -4.210e-001 -4.150e-001 -4.060e-001 -3.910e-001 -3.700e-001 -3.510e-001 -3.350e-001 -3.170e-001 -3.060e-001 -3.100e-001 -3.260e-001 -3.570e-001 -3.910e-001 -4.100e-001 -4.100e-001 -4.100e-001 -3.870e-001 -3.550e-001
-3.190e-001
   67.9591
                          3.71
  300.0000
                         59.19
    31.3752
                         33.04
    23.3282
                         71.25
     7.5400 10000000000.00
<Date: Fri Oct 10 09:51:00 2008</pre>
<Time Range=6 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                                   6 Ampl=OFF
<Remark: NEAR STANI</pre>
*****
#GEOSEC: 0332 / 50.0/ 50.0/ 1. 41.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                     1.0/ 558599.000/ 3918271.000/
                                                                                  0.000 DH =
                                                                                                                0.000/rms=121.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.134e+001 +2.174e+001 +2.744e+001 +2.999e+001 +3.148e+001 +3.293e+001 +3.438e+001 +3.559e+001
+3.678e+001 +3.858e+001 +4.119e+001 +4.376e+001 +4.603e+001 +4.860e+001
+5.057e+001 +5.088e+001 +5.009e+001 +4.802e+001 +4.478e+001 +4.192e+001 +3.957e+001 +3.694e+001 +3.427e+001 +3.237e+001 +3.089e+001 +2.924e+001 +2.748e+001 +2.604e+001 +2.478e+001 +2.317e+001 +2.126e+001 +1.974e+001
+1.858e+001
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 -8.980e-001 +6.150e-001 +3.670e-001 +2.690e-001 +2.160e-001 +1.950e-001 +2.050e-001
+2.330e-001 +2.780e-001 +3.200e-001 +3.330e-001 +3.160e-001 +2.470e-001 +1.060e-001 -4.200e-002 -1.610e-001 -2.630e-001 -3.230e-001 -3.400e-001 -3.390e-001 -3.290e-001 -3.120e-001 -2.880e-001 -2.880e-001 -2.800e-001
-2.840e-001 -2.980e-001 -3.180e-001 -3.440e-001 -3.620e-001 -3.610e-001
-3.510e-001
   25.7049
50.1184
                        27.72
  100.0000
                         30.95
     9.9546
                         86.68
     2.5396 10000000000.00
<Date: Tue Nov 25 08:45:20 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                   6 Ampl=OFF
<Remark: PHYLLITES</pre>
*****
                                          50.0/ 50.0/
                                                                     1.0/
                                                                                559158.000/ 3919367.000/
14.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                                                0.000/rms=136.00
                                                                                   0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +8.476e+000 +2.675e+001 +3.915e+001 +4.536e+001 +4.809e+001 +5.025e+001 +5.346e+001 +5.809e+001 +6.257e+001 +6.644e+001 +7.039e+001 +7.224e+001 +7.056e+001 +6.687e+001 +6.039e+001
+5.189e+001 +4.502e+001 +3.962e+001 +3.372e+001 +2.788e+001 +2.375e+001 +2.070e+001 +1.749e+001 +1.440e+001 +1.232e+001 +1.080e+001 +9.238e+000 +7.772e+000 +6.785e+000 +6.079e+000 +5.361e+000 +4.696e+000 +4.258e+000
+3.951e+000
                  +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -8.380e-001
+4.300e-001 +2.860e-001 +2.920e-001 +3.400e-001 +3.830e-001 +3.880e-001 +3.470e-001 +2.230e-001 -1.700e-002 -2.440e-001 -3.760e-001 -4.500e-001 -4.790e-001 -4.860e-001 -4.890e-001 -4.910e-001 -4.920e-001 -4.930e-001 -4.930e-001 -4.930e-001 -4.930e-001 -4.930e-001 -4.930e-001 -4.870e-001
-4.830e-001 -4.780e-001 -4.710e-001 -4.600e-001 -4.400e-001 -4.180e-001
-3.930e-001
```

```
1D_Inversion_Results_TEM.txt
  34.1371
                 7.15
                 24.60
  71.8947
  18.1943
                12.65
                10.00
   1.0000
    1.0000 10000000000.00
<Date: Tue Nov 25 09:11:32 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                   6 Ampl=OFF
<Remark: NEAR COAST</pre>
<Place: AFTER RIVER
#GEOSEC: 0334 / 50.0/ 50.0/ 1
13.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                               1.0/ 559349.000/ 3919354.000/
                                                         0.000 DH =
                                                                            0.000/rms = 41.00
S [V/A]:
            +0.000e+000 +0.000e+000 +2.965e+000 +1.779e+001 +2.856e+001
+3.457e+001 +3.727e+001 +3.885e+001 +4.033e+001 +4.162e+001 +4.239e+001 +4.283e+001 +4.301e+001 +4.264e+001 +4.173e+001 +4.051e+001 +3.848e+001
+3.562e+001 +3.303e+001 +3.078e+001 +2.809e+001 +2.518e+001 +2.295e+001
+2.120e+001 +1.924e+001 +1.719e+001 +1.568e+001 +1.449e+001 +1.314e+001
+1.174e+001 +1.068e+001 +9.855e+000 +8.941e+000 +8.016e+000 +7.352e+000
+6.857e+000
Err[V/A]:
            +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -8.810e-001
+5.330e-001 +3.150e-001 +2.290e-001 +1.720e-001 +1.220e-001 +8.400e-002
+4.800e-002 -7.000e-003 -8.600e-002 -1.620e-001 -2.260e-001 -2.940e-001 -3.510e-001 -3.800e-001 -3.960e-001 -4.080e-001 -4.150e-001 -4.170e-001 -4.180e-001 -4.180e-001 -4.180e-001 -4.180e-001 -4.200e-001
-4.210e-001 -4.220e-001 -4.210e-001 -4.170e-001 -4.080e-001 -3.960e-001
-3.830e-001
  29.1644
48.5281
                  6.29
                 23.31
  13.8544
                16.99
    3.8036
                 26.32
    2.0372 10000000000.00
<Date: Tue Nov 25 09:35:49 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                   6 Ampl=OFF
<Remark: NEAR COAST
<Place: AFTER RIVER
<*****************************
#GEOSEC: 0335-A
                          / 50.0/ 50.0/
                                               1.0/ 559450.000/ 3919384.000/
14.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                         0.000 DH =
                                                                            0.000/\text{rms} = 39.00
S [V/A]: +0.000e+000 +0.000e+000 +1.010e+001 +3.223e+001 +4.871e+001 +5.731e+001 +5.980e+001 +6.038e+001 +5.999e+001 +5.822e+001 +5.594e+001
+5.362e+001 +5.061e+001 +4.722e+001 +4.456e+001 +4.247e+001 +4.004e+001
+3.733e+001 +3.506e+001 +3.303e+001 +3.040e+001 +2.723e+001 +2.459e+001
+2.242e+001 +1.995e+001 +1.741e+001 +1.560e+001 +1.422e+001 +1.273e+001 +1.126e+001 +1.020e+001 +9.396e+000 +8.535e+000 +7.674e+000 +7.050e+000
+6.565e+000
            +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -8.580e-001
Err[V/A]:
+4.160e-001 +1.360e-001 +1.800e-002 -8.200e-002 -1.800e-001 -2.400e-001
-2.720e-001 -2.920e-001 -2.990e-001 -2.970e-001 -2.950e-001 -2.990e-001 -3.140e-001 -3.380e-001 -3.640e-001 -3.970e-001 -4.270e-001 -4.430e-001 -4.510e-001 -4.540e-001 -4.530e-001 -4.500e-001 -4.470e-001 -4.410e-001
-4.350e-001 -4.280e-001 -4.210e-001 -4.120e-001 -4.020e-001 -3.960e-001
-3.930e-001
  44.4496
56.7744
                  4.53
                 24.00
  11.3481
                 23.77
    2.9676
                 10.00
    2.2959 10000000000.00
<Date: Tue Nov 25 09:52:06 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                   6 Ampl=OFF
<Remark: NEAR COAST</pre>
******
#GEOSEC: 0336-A
                            50.0/ 50.0/ 1.0/ 559917.000/ 3919419.000/
14.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        0.000 \, DH =
                                                                            0.000/\text{rms}=185.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.690e+000 +9.434e+000
                                         Σελίδα 130
```

```
1D_Inversion_Results_TEM.txt
+1.775e+001 +2.357e+001 +2.783e+001 +3.227e+001 +3.627e+001 +3.865e+001 +4.008e+001 +4.116e+001 +4.153e+001 +4.110e+001 +4.018e+001 +3.836e+001 +3.552e+001 +3.283e+001 +3.045e+001 +2.758e+001 +2.446e+001 +2.207e+001
+2.019e+001 +1.807e+001 +1.585e+001 +1.423e+001 +1.295e+001 +1.153e+001
+1.010e+001 +9.060e+000 +8.283e+000 +7.460e+000 +6.664e+000 +6.115e+000
+5.711e+000
Err[V/A]:
                -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 -9.000e-001
+8.980e-001 +8.350e-001 +7.290e-001 +5.850e-001 +4.150e-001 +2.870e-001 +1.950e-001 +9.700e-002 -1.300e-002 -1.100e-001 -1.930e-001 -2.830e-001 -3.560e-001 -3.930e-001 -4.120e-001 -4.260e-001 -4.350e-001 -4.400e-001 -4.430e-001 -4.460e-001 -4.490e-001 -4.510e-001 -4.520e-001 -4.530e-001 -4.500e-001 -4.460e-001 -4.400e-001 -4.280e-001 -4.100e-001 -3.930e-001
-3.760e-001
   20.1859
                      8.04
                    24.19
 100.0000
    7.6970
                    13.95
    3.3318
                    13.25
    1.7661 10000000000.00
<Date: Tue Nov 25 10:12:31 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                   6 Ampl=OFF
<Remark: NEAR COAST
<Place: AFTER RIVER
<*****************************
*****
                                                        1.0/ 560099.000/ 3919448.000/
                                   50.0/ 50.0/
#GEOSEC: 0337
15.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                    0.000 DH=
                                                                                             0.000/rms = 97.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +1.362e+000 +5.563e+000
+9.326e+000 +1.192e+001 +1.386e+001 +1.603e+001 +1.842e+001 +2.044e+001 +2.224e+001 +2.454e+001 +2.714e+001 +2.889e+001 +2.973e+001 +2.964e+001
+2.807e+001 +2.603e+001 +2.410e+001 +2.178e+001 +1.934e+001 +1.757e+001
+1.622e+001 +1.479e+001 +1.337e+001 +1.239e+001 +1.163e+001 +1.077e+001 +9.830e+000 +9.077e+000 +8.448e+000 +7.701e+000 +6.888e+000 +6.270e+000
+5.788e+000
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 -9.000e-001 +8.880e-001 +7.970e-001 +7.010e-001 +6.110e-001 +5.480e-001 +5.190e-001
+5.020e-001 +4.720e-001 +3.940e-001 +2.640e-001 +9.900e-002 -1.290e-001
-3.190e-001 -3.920e-001 -4.170e-001 -4.280e-001 -4.270e-001 -4.220e-001 -4.140e-001 -4.010e-001 -3.830e-001 -3.710e-001 -3.650e-001 -3.670e-001 -3.780e-001 -3.910e-001 -4.020e-001 -4.130e-001 -4.200e-001 -4.210e-001
-4.200e-001
   13.7735
74.3127
                    8.31
23.24
    7.4730
                    10.00
    2.9419
                    37.00
    1.0000 10000000000.00
<Date: Tue Nov 25 10:29:42 2008
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                   6 Ampl=OFF
<Remark: NEAR COAST
<Place: AFTER RIVER
<****
*****
#GEOSEC: 0338-A / 50.0/ 50.0/ 1.0
12.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 560320.000/ 3919434.000/
                                                                    0.000 DH =
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +0.000e+000 +5.337e+000 +1.145e+001 +1.574e+001 +1.903e+001 +2.288e+001 +2.748e+001 +3.161e+001 +3.545e+001 +4.047e+001 +4.616e+001 +5.006e+001 +5.203e+001 +5.227e+001
+4.966e+001 +4.595e+001 +4.230e+001 +3.772e+001 +3.271e+001 +2.889e+001
+2.589e+001 +2.256e+001 +1.917e+001 +1.675e+001 +1.492e+001 +1.297e+001
+1.106e+001 +9.744e+000 +8.775e+000 +7.765e+000 +6.797e+000 +6.127e+000
+5.630e+000
               -1.000e-015 -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001
Err[V/A]:
+9.000e-001 +8.630e-001 +7.920e-001 +7.210e-001 +6.730e-001 +6.510e-001
+6.340e-001 +5.930e-001 +4.940e-001 +3.420e-001 +1.550e-001 -1.010e-001 -3.190e-001 -4.050e-001 -4.370e-001 -4.560e-001 -4.670e-001 -4.720e-001 -4.750e-001 -4.780e-001 -4.800e-001 -4.800e-001 -4.780e-001
-4.750e-001 -4.710e-001 -4.660e-001 -4.580e-001 -4.460e-001 -4.370e-001
-4.280e-001
   15.1879
                      6.38
```

```
1D_Inversion_Results_TEM.txt
                              28.27
  100.0000
  100.0000
                               13.30
       2.3430
                              15.32
       1.2501 10000000000.00
 <Date: Tue Nov 25 10:49:36 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                                                           6 Ampl=OFF
<Remark: NEAR COAST
<Place: AFTER RIVER
 ******
#GEOSEC: 0340 / 50.0/ 50.0/ 1.55.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      1.0/ 560700.000/ 3918704.000/
                                                                                                        0.000 DH=
                                                                                                                                          0.000/rms=178.00
                       +0.000e+000 +1.035e+001 +4.269e+001 +6.357e+001 +8.076e+001
       [V/A]:
+9.085e+001 +9.420e+001 +9.517e+001 +9.506e+001 +9.357e+001 +9.148e+001 +8.915e+001 +8.559e+001 +8.044e+001 +7.513e+001 +7.003e+001 +6.329e+001 +5.547e+001 +4.946e+001 +4.486e+001 +4.001e+001 +3.548e+001 +3.252e+001
+3.050e+001 +2.858e+001 +2.699e+001 +2.610e+001 +2.555e+001 +2.506e+001 +2.458e+001 +2.416e+001 +2.375e+001 +2.318e+001 +2.249e+001 +2.197e+001
+2.162e+001
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.910e-001 -6.940e-001 +3.230e-001 +1.230e-001 +3.300e-002 -3.700e-002 -1.020e-001 -1.480e-001
-1.870e-001 -2.410e-001 -3.100e-001 -3.670e-001 -4.050e-001 -4.360e-001
-4.530e-001 -4.570e-001 -4.530e-001 -4.420e-001 -4.170e-001 -3.850e-001 -3.490e-001 -2.940e-001 -2.220e-001 -1.670e-001 -1.290e-001 -1.020e-001 -9.700e-002 -1.100e-001 -1.260e-001 -1.400e-001 -1.400e-001 -1.210e-001
 -9.500e-002
    49.1226
                                1.99
    94.5733
23.0942
                               34.20
                               21.76
       5.5623
                               10.00
     23.0175 10000000000.00
<Date: Tue Nov 25 12:03:08 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff= <Remark: PHYLLITES
                                                                                                                           6 Ampl=OFF
<Place: KATAPATIMENA
#GEOSEC: 0344-A / 50.0/ 50.0/ 1
40.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      1.0/ 560534.000/ 3919257.000/
                                                                                                                                          0.000/\text{rms}=101.00
                                                                                                        0.000 DH =
                       +0.000e+000 +3.037e+000 +2.238e+001 +3.489e+001 +4.615e+001
+5.651e+001 +6.459e+001 +7.181e+001 +8.152e+001 +9.440e+001 +1.064e+002 +1.169e+002 +1.289e+002 +1.383e+002 +1.400e+002 +1.363e+002 +1.266e+002 +1.110e+002 +9.704e+001 +8.564e+001 +7.310e+001 +6.092e+001 +5.254e+001
+4.644e+001 +4.001e+001 +3.369e+001 +2.925e+001 +2.586e+001 +2.219e+001
+1.858e+001 +1.605e+001 +1.420e+001 +1.228e+001 +1.047e+001 +9.230e+000
+8.332e+000
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.970e-001 -8.020e-001 +6.570e-001 +6.000e-001 +5.870e-001 +5.890e-001 +5.900e-001 +5.730e-001
+5.300e-001 +4.160e-001 +1.880e-001 -6.500e-002 -2.630e-001 -4.050e-001
-4.670e-001 -4.830e-001 -4.880e-001 -4.890e-001 -4.890e-001 -4.870e-001 -4.870
 -4.620e-001
  24.3030
192.8514
99.8110
                              4.18
48.93
12.52
                              19.04
       2.3477
       1.1687 10000000000.00
<Date: Tue Nov 25 13:47:00 2008</pre>
 <Time Range=6 Currrent= 2.00 Stack= 5 Filter=50 Deff=
                                                                                                                           6 Ampl=OFF
<Remark: PHYLLITES</pre>
<Place: KATAPATIMENA-COAST
<
#GEOSEC: 0339-A / 50.0/ 50.0/ 1.1.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                                                      1.0/ 560510.000/ 3919427.000/
                                                                                                       0.000 DH=
                                                                                                                                          0.000/rms=168.00
S [V/A]: +0.000e+000 +0.000e+000 +0.000e+000 +5.710e-001 +6.037e+000
+1.297e+001 +1.842e+001 +2.298e+001 +2.870e+001 +3.606e+001 +4.286e+001
                                                                            Σελίδα 132
```

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1D_Inversion_Results_TEM.txt
+4.888e+001 +5.536e+001 +5.923e+001 +5.823e+001 +5.486e+001 +4.904e+001 +4.180e+001 +3.618e+001 +3.187e+001 +2.724e+001 +2.280e+001 +1.975e+001 +1.755e+001 +1.527e+001 +1.310e+001 +1.163e+001 +1.053e+001 +9.349e+000
+8.173e+000 +7.320e+000 +6.665e+000 +5.946e+000 +5.216e+000 +4.680e+000
+4.266e+000
Err[V/A]: -1.000e-015 -1.000e-015 -9.000e-001 -9.000e-001 -9.000e-001 +9.000e-001 +8.820e-001 +8.420e-001 +7.980e-001 +7.610e-001 +7.240e-001
+6.570e-001 +4.740e-001 +9.300e-002 -2.470e-001 -3.990e-001 -4.620e-001 -4.820e-001 -4.870e-001 -4.880e-001 -4.880e-001 -4.860e-001 -4.860e-001 -4.500e-001 -4.500e-001
-4.500e-001
   12.8490
                     5.15
 250.0000
                    34.26
    1.4867
                    10.00
    1.9017
                    12.08
    1.0000 10000000000.00
<Date: Tue Nov 25 11:13:54 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                 6 Ampl=OFF
<Remark: NEAR COAST
*****
#GEOSEC: 0343-A / 50.0 / 50.0 / 1.40.0 / 36 / 5 / 0 / 22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 560724.000/ 3919235.000/
                                                                    0.000 DH=
                                                                                           0.000/\text{rms}=208.00
               +0.000e+000 +3.964e+000 +1.321e+001 +2.033e+001 +2.749e+001
S [V/A]:
+3.429e+001 +3.934e+001 +4.353e+001 +4.880e+001 +5.539e+001 +6.135e+001
+6.668e+001 +7.312e+001 +7.934e+001 +8.259e+001 +8.337e+001 +8.165e+001 +7.640e+001 +7.024e+001 +6.431e+001 +5.684e+001 +4.857e+001 +4.227e+001
+3.735e+001 +3.193e+001 +2.643e+001 +2.257e+001 +1.966e+001 +1.662e+001
+1.376e+001 +1.187e+001 +1.056e+001 +9.280e+000 +8.180e+000 +7.528e+000
+7.131e+000
Err[V/A]: -9.000e-001 -9.000e-001 -9.000e-001 -8.970e-001 -8.270e-001 +6.830e-001 +5.950e-001 +5.560e-001 +5.350e-001 +5.240e-001 +5.120e-001
+4.880e-001 +4.240e-001 +2.950e-001 +1.390e-001 -1.700e-002 -2.020e-001
-3.530e-001 -4.200e-001 -4.500e-001 -4.690e-001 -4.800e-001 -4.850e-001
-4.870e-001 -4.900e-001 -4.920e-001 -4.930e-001 -4.930e-001 -4.930e-001 -4.900e-001 -4.850e-001 -4.770e-001 -4.590e-001 -4.190e-001 -3.610e-001
-2.910e-001
   20.6955
                     4.74
 115.5725
22.2610
                    42.77
                    10.00
    3.0611
                    10.00
    1.2572 10000000000.00
<Date: Tue Nov 25 13:27:36 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                                 6 Ampl=OFF
<Remark: PHYLLITES</pre>
<Place: KATAPATIMENA-COAST
*****
#GEOSEC: 0341-A / 50.0/ 50.0/ 1.
50.0/36/5/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 561089.000/ 3918832.000/
                                                                                           0.000/rms=120.00
                                                                   0.000 DH =
               +0.000e+000 +0.000e+000 +8.056e+000 +2.353e+001 +3.337e+001
+3.769e+001 +3.900e+001 +3.954e+001 +3.992e+001 +4.012e+001 +4.018e+001 +4.019e+001 +4.023e+001 +4.034e+001 +4.051e+001 +4.069e+001 +4.094e+001 +4.122e+001 +4.141e+001 +4.153e+001 +4.161e+001 +4.158e+001 +4.147e+001
+4.137e+001 +4.129e+001 +4.138e+001 +4.166e+001 +4.205e+001 +4.264e+001
+4.327e+001 +4.350e+001 +4.336e+001 +4.269e+001 +4.137e+001 +4.003e+001
+3.891e+001
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -8.060e-001 +3.250e-001 +1.300e-001 +7.100e-002 +3.700e-002 +1.500e-002 +5.000e-003
+3.000e-003 +9.000e-003 +1.900e-002 +2.700e-002 +3.200e-002 +3.300e-002
+3.000e-002 +2.400e-002 +1.600e-002 +4.000e-003 -1.000e-002 -1.600e-002 -1.400e-002 -1.000e-003 +2.700e-002 +5.300e-002 +7.100e-002 +7.500e-002 +5.000e-002 +2.000e-003 -5.200e-002 -1.170e-001 -1.710e-001 -1.880e-001
-1.910e-001
   23.7020
                     1.03
   42.0853
                  131.71
```

```
1D_Inversion_Results_TEM.txt
  49.0102
                  134.41
    3.0896
                   11.15
 100.0000 10000000000.00
<Date: Tue Nov 25 12:28:35 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=
                                                                                6 Ampl=OFF
<Remark: PHYLLITES</pre>
<Place: KATAPATIMENA
<**************************
*****
#GEOSEC: 0342 / 50.0/ 50.0/ 1. 67.0/36/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                        1.0/ 561459.000/ 3918999.000/
                                                                  0.000 DH =
                                                                                         0.000/\text{rms}=304.00
               +0.000e+000 +0.000e+000 +1.396e+001 +2.802e+001 +3.634e+001
+3.931e+001 +3.957e+001 +3.917e+001 +3.833e+001 +3.704e+001 +3.590e+001
+3.488e+001 +3.360e+001 +3.194e+001 +3.022e+001 +2.843e+001 +2.578e+001
+2.225e+001 +1.920e+001 +1.668e+001 +1.388e+001 +1.112e+001 +9.230e+000 +7.870e+000 +6.480e+000 +5.184e+000 +4.331e+000 +3.717e+000 +3.093e+000
+2.515e+000 +2.129e+000 +1.855e+000 +1.576e+000 +1.316e+000 +1.141e+000
+1.015e+000
Err[V/A]: +5.000e-001 -9.000e-001 -9.000e-001 -9.000e-001 -6.800e-001 +1.700e-001 -1.800e-002 -8.600e-002 -1.330e-001 -1.640e-001 -1.780e-001 -1.890e-001 -2.120e-001 -2.620e-001 -3.250e-001 -3.850e-001 -4.440e-001
-4.800e-001 -4.910e-001 -4.950e-001 -4.970e-001 -4.980e-001 -4.980e-001 -4.980e-001 -4.980e-001 -4.980e-001 -4.960e-001 -4.950e-001 -4.940e-001 -4.930e-001 -4.910e-001 -4.870e-001 -4.830e-001 -4.790e-001
   28.9401
                    13.61
    4.8509
                   10.00
    0.2000 10000000000.00
<Date: Tue Nov 25 12:52:14 2008</pre>
<Time Range=6 Currrent= 3.70 Stack= 5 Filter=50 Deff=</pre>
                                                                               6 Ampl=OFF
<Remark: PHYLLITES</pre>
*****
                                                        1.0/ 565350.000/ 3914318.000/
#GEOSEC: 0331-A
                                  50.0/ 50.0/
131.0/28/3/0/22222 SPM=0 K= 0.000e+000 H=
                                                                    0.000 DH =
0.000/\text{rms}=499.00
S [V/A]: +1.060e+002 +1.768e+002 +2.643e+002 +3.784e+002 +5.915e+002 +8.981e+002 +1.003e+003 +9.310e+002 +7.795e+002 +6.272e+002 +5.318e+002 +4.685e+002 +4.085e+002 +3.573e+002 +3.251e+002 +3.033e+002 +2.809e+002 +2.578e+002 +2.383e+002 +2.199e+002 +1.950e+002 +1.646e+002 +1.403e+002 +1.216e+002 +1.022e+002 +8.446e+001 +7.343e+001 +6.601e+001 Err[V/A]: -8.950e-001 -8.950e-001 -8.970e-001 -8.970e-001
+8.030e-001 +1.100e-002 -4.600e-001 -4.940e-001 -4.940e-001 -4.890e-001
-4.800e-001 -4.630e-001 -4.320e-001 -4.000e-001 -3.740e-001 -3.560e-001 -3.670e-001 -4.020e-001 -4.390e-001 -4.720e-001 -4.890e-001 -4.940e-001 -4.950e-001 -4.930e-001 -4.880e-001 -4.780e-001 -4.620e-001
 863.6017
                   77.13
                    39.27
   23.6960
    1.6462 10000000000.00
<Date: Thu Nov 13 11:03:52 2008</pre>
<Time Range=4 Currrent= 1.00 Stack= 5 Filter=50 Deff=</pre>
                                                                                5 Ampl=OFF
<Remark: TEST IONIAN DOLOM</pre>
*****
```